

C.W.

Theory important

Yasin Sir L-1

Date: 13/04/19

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References

1. Principles of foundation engg - BM Dash
2. Physical and Geotechnical Properties of soil - Bowels
3. Coduto
4. Peck and Hanson

- Soil investigation techniques
- Planning and reporting
- Rafts and piles
- Slope stability analysis

Site exploration and characterization
 properties of subsoil. unique in geotechnical engg. In other cases, specified properties are available or decided by engineers.

Soil strength parameters, c, ϕ, q_u (Direct shear, Unconfined Compression)
 Settlement, C_c, C_r, OCR

BD, alluvial soil, heterogenous, recent deposit.
 Soil cannot be specified, we must what we have.

* Purpose / Significance

No place for imagination. Should be tested / explored

* Explanation of each point reqd.

1. Nature \rightarrow type: boulder-gravel-clay / cohesion / thickness, depth, organic mat \uparrow $q_u < 10 \sim 15$ kPa
 consistency: stiff, soft (clay)
 loose, dense (sand)

\downarrow
 SPT 40-50

2. Assess the suitability:

CE \rightarrow 4th upto 200m for high rise / bridge.

Geologist \rightarrow deeper

Agriculture: few meters. before construction

Type and height of structure determines depth of exploration.

3. Topsoil → weathered zone
Solid crust → bedrock.

slope north to south in BD
Fault movement, tectonic activity for important structure (Padma bridge, nuclear power plant)

Bearing level/stratum

Scouring depth with high velocity, washes away bed material (Padma - 60m)

Position of soft clay layers

4. GWT: Fluctuation. Permanent level
Depth increases → settlement, liquefaction.

- Variation harms wooden foundation.

5. foundation problems:

Soil may lose shear strength & pore pressure buildup.
↓
Collapse

Expansion.

6. Type of foundation:

Pile, raft, mat.

7. Ground improvement.

When forced to use bad soil.

8. Soil sample, tests. → design parameters

Canal, leachate pond (impermeable layer), embankment

↓
permeability

↓
c, φ.

9. Construction method:
Basements. increase depth to cut
Dewatering if GWL intercepts.
Shore protection for structures nearby.

Soil movement, factors, activities important
structures (Radar bridge, nuclear power plant)
Bearing level/shaft
Soil movement, factors, activities important
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Soil movement, factors, activities important
structures (Radar bridge, nuclear power plant)
Bearing level/shaft

1. Foundation problems
Soil may lose shear strength. presence of
collapse
Expansion
2. Type of foundation:
Pile, raft, mat
3. Ground improvement
When forced to use bad soil.
4. Soil sample, tests - design parameters
5. Soil test results (impermeable layer) important

3. Reconnaissance:

সংক্রান্ত

general topography - canal, marsh
 shrinkage crack in dry season
 embankment failure as rainwater enters through cracks.
 stratification through previous excavation
 high water mark (flood level)
 vegetation.
 info of adjacent building (foundation)

Site Geology

filled up channel
 Satellite image for shift in channel for 10-20 years
 (SPAARSO) - Padma bridge.

Seismic potential

Difference in plain, hilly, marshy areas.

Earthquake: nearby faults, return period

Great Brahmaputra earthquake - 100 years return period

Gravity slope followed by rivers, break in that indicates fault. Sylhet, Tongi

for 100 story building in Purbachal.

2. Field work

Boring de

Boring depth. Minimum influence zone depending on type and load of structure.

Bed rock can be found $\frac{1}{2}$ - 1 km down

Stress due to imposed load decreases with depth (Newmark chart)

Thumb rule: 1:2 dispersion.

$$D_2 = \frac{\Delta\sigma}{\sigma_z} = 0.05 \quad \left(\Delta\sigma = \frac{1}{20} \text{th} \right)$$

Depth determined from experience or empirical equation.

Steel can take higher differential settlement.

$$D_1 = 0.1q \geq 30 \text{ ft}$$

Boring spacing:

Close spacing for dam.

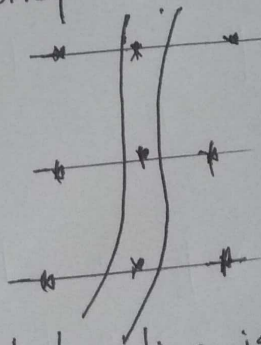
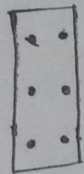
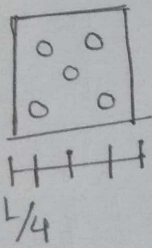
Airport runway: 10km

Sparse in case of road

For large projects, at first sparse, grid pattern boring for preliminary design producing general picture.

Boring location:

depends on plot shape.



(Boring may be done crosswise)

If structure exact location is known, boring should be done there.

Borehole location for bridge depends on scour depth.

আগে কিছু জায়গায় deep boring, uniform layer দান্ত্রা গেলে cost বাঁচে কারণ অন্য জায়গায় shallow boring.

* Soil investigation is very important for safe structure.

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Exploratory Borings Techniques and Equipments

Boring methods

- * Process
- * Applicability
- * Limitation
- * Advantages

Auger method:

Hand auger: not for sandy soil highly disturbed.

Machine operated: helix এর সাথে soil লাগে থাকবে,
Solid stem / Hollow stem

↓
Undisturbed soil

(Auger remains, removing the front bit and pushing a sampler through the hollow pipe)

70-100 mm hole enough to collect samples for consolidation, unconfined compression, direct shear.

Wash boring:

Sharp cutters in front. Fall from a height. Then torque applied. Water pumped into the loose soil which is forced upward with the soil. Water circulation.

Suitable for soft alluvial deposit (BD). manpower তার 4500/- for 30m

Easy to carry.

Drill হলে SPT or undisturbed sample

↓
(disturbed sample)

Rotary drilling

Relatively hard soil As wash boring.

Percussion drilling:

machine operated. unlike wash boring. only disturbed sample due to pounding.

Bore-log

D1, 2, Disturbed samples

Description - symbol - D1 - SPT.

* Mentioned if layers changes in the middle.

SPT: 140 pound hammer from 2.5' on drill. 6"

penetrate করতে কত blow?

প্রথম column ignore. কারণ top 6" is disturbed due to boring.

Existing G.L. elevation বসানে homogeneity, discontinuity

যাওয়া যাবে

Staggered boring

Geological profile. for det foundation design.

Individual footing - relative settlement due to relative density.

footing depth.

Ground improvement, if reqd.

Grasfield layout.

Observation of Water Table

High hydraulic conductivity - after borehole stabilization, then
(Highly permeable)

Impermeable - waters will not stabilize
rain/heat may affect open waters

Piezometers.

ডিয়েটরে ৫০৮ dia standpipe. দ্রুত stabilize
Impermeable layer to prevent water entering
into borehole.

Electric transducer = auto record water level.

Silty soil: Vorstev method

3 # equal time interval

* 3 টি point পাওয়া যাবে. Average line draw করতে
হবে।

Also piezometer may be used.

Soil sampling:

Disturbed = Boring, SPT-N

Undisturbed

Wash boring করলে পানি mix করলে constituent change
হয়ে যায়। Sample হয়না।

SPT থেকে disturbed sample.

6" penetrate করতে যত blow লাগে - SPT-N

Test ~ attachment বার বার change করতে হয়।

SPT তে pipe এর নিচে Split Spoon Sampler. Hollow pipe এ
sample উঠে আসে. Ingredient same, but compressed.

* Undisturbed allowed for all tests.

Split Spoon Samplers

Driving shoe জুড়ুর দিকে dia কক্ষ, পরে dia বোঝা হওয়ার থাকলে friction length বাড়ায় অনেক বোঝা resistance আসত। ওয়ার কক্ষ dia 'র resistance continue করবে।

Ball joint Other end solid থাকলে আগে পানি ঢুকবে জায়গা দখল করে soil ঢুকতে পারবে না।

Other end open হলে উপরে পানির কলাম soil কে নিচে ফেলে দিবে। Ball works as a lock.
Suction

Shelby tube.

Soft to moderate stiff ~ BD

Ball joint - 7-8m depth sampling. Vacuum.

Parameters:

Annular area ratio $< 10\%$.

For large A_r , soil will be compressed.

Cramping ratio. $C_r < 1$ (Variable internal dia)

*Advantages and disadvantages.

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Sampling of Cohesionless soil

Spraying core catcher tube and cap.

Sand cannot drop as springs close.

Very fine sand / pebble may not be recovered.

Piston sampler:

For very soft soil. 2 tubes. Piston is connected. After boring,

Inside piston is pushed down, Fixed piston stays in place.

Because of fixed piston, no water or air cannot remain

inside. Sample cannot drop due to suction.

Fixed piston prevents swelling of soft soil

Hand carved sample:

Tube then plate. Undisturbed sample at shallow depth.

Lecture-5

Field Tests:

- DPL: Dynamic penetration
- light
- medium
- heavy
- super heavy

SPT is the most common. Others are conducted depending on project.

Standard Penetration Test

Too many error sources.

Hammer height is important for energy transmission.

Manually controlled means height varies.

Rope এর পিঠ friction control করে। (2 1/2 turns)

Connection

Ideally, hammer energy should be transmitted completely.

$$\left(\frac{E_A}{E_{in}}\right)_{max} = 1$$

Convert accordingly. Different for different countries.

Empirical relationship of SPT and soil properties.

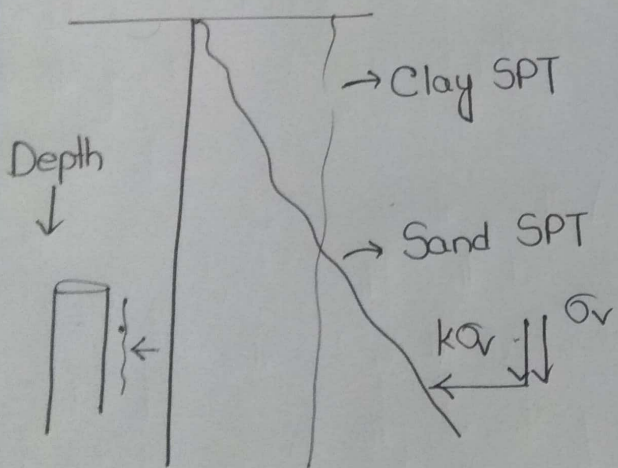
Interpretation depends on type of soil, not only on N.

SPT ~ OCR

Straight line in semilog papers.

OCR from consolidation test.

Cohesionless soil



Sand SPT increases due to friction → normal stress → overburden pressure.

Clay SPT remains same.

SPT ~ Relative Density:

N_f - field SPT is accompanied with σ_v'

SPT is done on silty soil under GWT. Water level lowers due to fast pulling out of drill rod. Bailing occurs due to hydraulic head.

Compressibility → check moisture content along with SPT.

Disadvantages:

- Automated operation is not 100% accurate.
- Human judgment reqd.
- Pore pressure cannot be zero (minm σ_h)
- Wheel mounted so difficult to move.

CPT correlations:

- Relative density Semilog \curvearrowright straight line.
- Angle of internal friction.
- Friction ratio (Soil type) $N_f = \text{SPT-field value}$.
- $C_u = \frac{q_u}{2}$ = undrained cohesion.

Preconsolidation pressure, OCR
 * কীভাবে related, Graph type, কোন factor এর উপর কোন parameters dependent ~ স্নেহে রাখতে হবে

Pressuremeter test

- We want soil to expand laterally.
- Guard cell prevents vertical expansion.
- Supplied liquid/gas indicates the increased volume.
- Points of inflection - two.
- P_L = limit pressure. Volume will continue to increase.

Soil yields.

$$V_m = \frac{V_o + V_f}{2}$$

Pressuremeter modulus E_p (Slope of volumetric strain vs pressure)

Crosscheck with CPT & SPT correlations

Vane shear Test

Hand vane: on sample soft soil only. sand & vane shear test

λ = correction factor.

$C_u \uparrow$ stiffer $\uparrow \lambda \downarrow$

Geophysical Exploration

1. Seismic refraction survey
2. Cross hole seismic "
3. Resistivity survey.

Relatively new technology

Applicability: Large area, Megaprojects (10 acre and +)

Rapid

Precision scale

Validation reqd. (Casualty) different.

* There is small scale applicability.

* Image interpretation can be flawed 1 in 100 or 1 in 1000.

Seismic Refraction Survey

S-wave - Shear wave

P-wave - Compression and Expansion.

Velocity of P wave depends on soil stiffness.

Mechanism

Transducers: mili/nano second recorder.

যতগুলো layer within 5-10 m range ততগুলো straight line

$$\text{Slope} = \frac{1}{\text{Velocity}} = \frac{\text{Time}}{\text{Distance}}$$

পূর্ণ অভ্রবুর্তীণ প্রতিফলন

যিও stiff medium তত $E \uparrow$ $v \uparrow$

Water এর নিচে থাকলে incorrect velocity. | Limitation.

Cross-hole seismic survey:

Old buildings cannot be removed for exploration.

যেই depth এ measure করাছি সেই S-wave সেই layer এর info.

Related to shear modulus.

Layers can be identified by time profiling (change in time)

Electrical Resistivity Survey

Mechanism:

Wenner method

৩টি line করে 1 m electrode, same gap.

Voltage drop

d is adjusted for multiple values.

Multiple layers হলে segmented straightline.

Old utility lines can be located. (Map নাই থাকলে)

Soft pocket within mat foundation may cause building to tilt. To save boring cost, survey.

Subsoil exploration report

Arbitration if it is neglected.

Preview: Slope stability.

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SLOPE STABILITY

Slope:

Not horizontal. 'Unrestrained'. Fortified - not.

Natural: Mountain, Bank

Manmade: Road embankment.

How do they fail?

Large magnitude.

Macro stability of slope

Micro stability also possible (দাশড় থেকে আট কটা)

Natural failure. Inclined component of gravity.

Liquid will flow but soil has shear strength.

Causes:

৩৭. পানি ঢুকলে, W level বড়বে.

Particle to particle stress field changes.

Phenomena Governing Stability of Slope:

Water lowers stability

Pore water pressure \uparrow effective stress/strength

Horizontal seepage imposes additional force.

Lubrication between two layers - sliding.

Liquefaction: Earthquake. behaves as liquid.

Factor of Safety:

Shear stress \leq Shear strength.

Shear strength এর অধীন হলেই factor failure

১৯২

Type of soil can predict potential surfaces.
Trial and error matching stress-strength of each surface.

$$FS = \frac{\text{Strength}}{\text{Developed stress}}$$

Mohr-Coulomb Failure Criteria.

Cohesion = glue effect

ϕ = depends on normal stress how much resistance will develop.

$FS > 1$ must

For permanent slope $FS \geq 1.5$

$$F_c \text{ and } F_\phi \quad F_c = F_\phi \text{ (always)}$$

$$\frac{c}{c_d} = \frac{\tan \phi}{\tan \phi_d} \text{ (Not precise, but within reasonable range)}$$

- 1. Limit equilibrium method
- 2. Stress analysis method (मातृसूत्र)

Impending failure:

Plane ~

Shear stress = Shear Strength

Curved ~

Moment

(Rotational failure about a point)

Infinite slope and semi-infinite soil mass.

AB potentially failure surface, abcd parallelepiped

Force imbalance by freebody diagram.

Stability of infinite slope without seepage

Assumption. Side forces are equal and colinear
(No need to consider this)

Assume, homogenous soil,

$$\tau = \frac{T_a}{A} = \frac{\gamma L H \sin \beta}{L / \cos \beta} = \gamma H \sin \beta \cos \beta$$

$$\sigma = \gamma H \cos^2 \beta$$

$$\tau_d = c_d + \sigma \tan \phi_d$$

$$c_d = \frac{c}{FS}$$

$$\tan \phi_d = \frac{\tan \phi}{FS}$$

How does c, ϕ, β affect FS?

Apparent cohesion if sand is wet, but mostly $c=0$

For sand,

$$F_s = \frac{\tan \phi}{\tan \beta}$$

[H has no effect on FS]

$\beta < \phi$ β যত ছোট steep angle এ যাত্রা যাবেন,

$\phi = 0$, saturated clay / undrained situation.

$$F_s = \frac{c}{\gamma H \cos^2 \beta \tan \beta}$$

[H is important here]

That is why mountains are made of rock / granular material

At critical condition,

$$F_s = 1 \Rightarrow H_{cr} = \frac{c}{\gamma \cos^2 \beta \tan \beta}$$

Stability of Infinite Slope with Seepage,

$\gamma = \gamma_{sat}$
 $\sigma = \sigma' + u$

$$F_s = \frac{c}{\gamma_{sat} H \cos^2 \beta \tan \beta} + \frac{\gamma'}{\gamma_{sat}} \frac{\tan \phi}{\tan \beta}$$

since, $\gamma_{sat} > \gamma'$ $\left[\frac{\gamma'}{\gamma_{sat}} \approx 0.5 \right]$
 F_s decreases.

Slope fails in rainy season
 Disturbed slope causes high seepage as base
 Lower surface runoff.

Examples:

Not only slope but also excavation.

Finite Slopes

In real life, slopes are finite with limited height.

Shallow failure: Top surface.

Toe failure

Base failure

Single/Curved/Multistep

Plain.

Analysis

ABC block, Weight, Friction resistance, Normal force, reaction

At impending condition, Weight component = Resistance.

Resistance development due to cohesion and normal force (friction)

$$\tau = \tau_d \text{ (developed)}$$

যে plane এ τ_d minimum হৈছে সেখানে fail করবে।

$$\frac{\partial \tau_d}{\partial \theta} = 0 \quad (\theta = \theta_{\text{critical}})$$

$$\frac{\beta + \phi_d}{2} = \theta_{\text{critical}} < \beta \text{ (slope angle)}$$

To determine Factor of Safety, start with ϕ , FS_ϕ then FS_c .

$$FS_\phi = FS_c \text{ (or else revised)}$$

Maximum height of slope/depth of cut for a particular factor of safety. Design problem, Here

Steeper slope may fail, then decrease β (milder)

Example 13.3

$c = 600 \text{ lb/ft}^2, \phi = 15^\circ$

$c_d = 200 \text{ lb/ft}^2, \phi = 5.1^\circ \text{ (FS = 3)}$

Here $= 23', \beta = 45^\circ$

Slopes with water in the crack (tensile)

Soil variation. Insufficient soil investigation warrants

higher slope FS = 3

Temporary slope, FS = 1.5

Dry season: Shrinkage crack.

Rainy season: Water infiltrates crack.

FS decreases. Extra pressure affects failure block.

Disturbing force ↑

Buoyancy decreases normal force ↓

Crack depth is important

Crack vertical, Water pressure works perpendicular to crack.

X can be determined from graph/design pad.

Disturbing force W, U

Resisting force, $R = cX + (W \cos \theta - U_1 \sin \theta - U_2) \tan \phi$

Area

Considerations:

Q. Find point C for protection against excess loading.

1. BC may have load on them. as trucks loading (shoulder) rest on shoulder. Should assume distributed load on BC.

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Finite slope: Circular Failure Surface

Homogenous clay, $\phi = 0$ (Undrained condition)

$$\tau_f = c_u$$

Drained condition ϕ $c-\phi$ হয়ে যাবে,Fast loading - direct shear - c_u W_0 moment রাখায় দিবে,

* Use design pad.

Limiting condition এর আগ পর্যন্ত $c_d = c_u$ develop করার
gradually.

$$M_R = c_d (AED)(1/r) = cr^2\theta$$

$$F_c = \frac{c_u}{c_d} = [\text{Change } \beta \text{ accordingly}]$$

For a single centre, all options need not be analyzed.

Critical circles - minm of minm.

 $B > 53^\circ$ Toe circle $B < 53^\circ$ Toe/Midpoint/Slope (Depends on D = Depth of
hard layer from top) $D \geq 1.2H$ হলে Midpoint circle, $D = 1.2H$ toe, $D \leq 1H$ slope

$$m = \frac{c_d}{\gamma H} = \text{stability numbers}$$

$$m = \frac{\gamma H}{c_d} = \text{stability factor}$$

Q Maximum depth with $FS = 3$

$$FS \rightarrow c_u \rightarrow c_d \rightarrow m \rightarrow \beta \rightarrow H$$

* বড় load পর্যন্ত safe আ বের করতে হবে,

Rana plaza crash due to overloading

To locate the centre, use graphs.

$$n = \frac{\text{Horizontal distance}}{\text{Vertical distance}}$$

Top horizontal distance reqd to impose restriction.

Examples 13.4

Example 13.5

$$\beta = 75^\circ$$

Maxm depth - limiting condition - $c_u = c_d - FS = 1$.

Example 13.6

Mass procedure

$$\phi > 0^\circ$$

Normal force is ignored.

N and R - combined indeed.

Resultant

W. Design chart.

$$F_c \neq F_\phi \text{ (Revise } \phi)$$

Example 13.8

Critical height $\Rightarrow FS = 1, c_u = c_d$.

For any other height, c_d, ϕ_d haven't reached c_u, ϕ .

Trial and error. $\phi \leq 20^\circ$

Ordinary Method of Slices

পাহাড় ঝাঁস : Manmade disaster. Sand-hill, will get saturated and fail.

আগের method গুলো ছিল mass procedure considering blocks.

Assumption: 1. Pore water pressure zero
Water table way below.

Freebody diagram.

ΣF_x , ΣM এর কোন effect ফেলবে না, Resistance remains. W , T_r , N_r . Resultant vertically upward

হবে হবে। ΔL

$A = \text{Factored}$.

σ = Normal stress on normal surface area,

(Homogeneous soil, else, plastic...)
1. Point makes modelling to holders, depends.

Effective Stress Analysis-

Summation
Summation

FS কমবে overall. Void space এর দানি' থেকে উঠবে

Example 13.9

Design sheet এর ছবি, Arbitrary centre.

সময়সময় 5 slice.

Width (দক্ষাঙ্কিতের পর দরকার নাই)

Height (Avg height)

Centre থেকে line টেনে radial line connect করতে

হবে। α . Vertically clockwise negative. Resisting

and disturbing moment.

We are considering segmental straight line.

অথবা inclined length scale দিয়ে যে করা যায়

$$W = b \times h \times \gamma$$

This is for one centre. এককর আধা centre (dome) নিয়ে critical FS and critical surface দেব করতে হবে।

Normal stress on normal surface
 Point method
 Effective stress analysis
 Overall void space
 Example 13.9
 Design sheet of soil
 (Arbitrary centre)
 (Arbitrary centre)
 (Arbitrary centre)

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Bishop's Simplified Method of Slices

Ordinary method of slices is too conservative.

If calculated FS < field FS (conservative)

calculated FS (say 1.25) > field FS (say 0.9) (may fail)

→ Implication of conservative

Design becomes uneconomic to some extent.

We must not use method that overestimates FS.

Gone are the days of thumb rule. Analysis should estimate field FS closely.

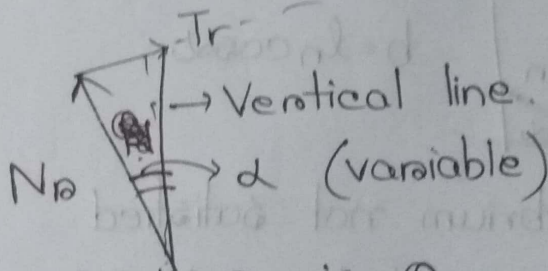
Ordinary method assumption. Side forces are equal in magnitude and colinear. Completely balances.

But Bishop considers them to some extent.

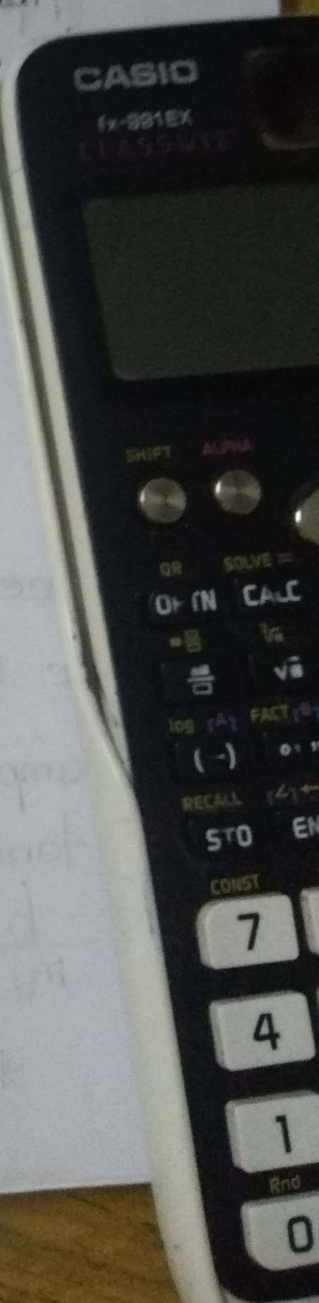
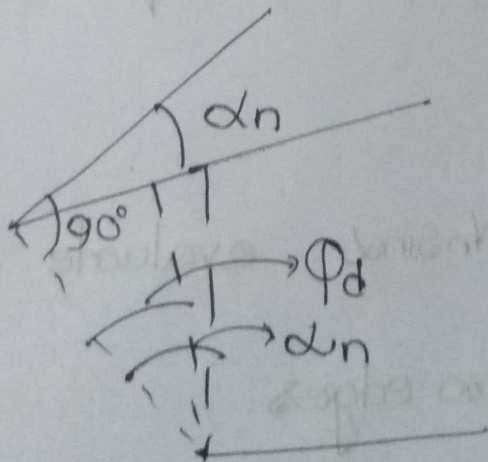
Developed friction factor. $\tan \phi_d$

T_r inclined. ΔP horizontal, $\Delta T, W$ - vertical

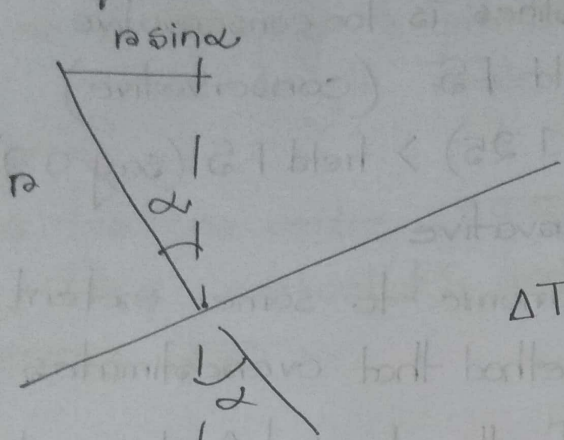
$N_r \perp T_r$ 90°



Angle b/w N_r and $N_r \tan \phi_d$ is ϕ_d .



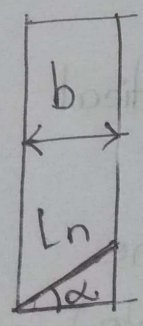
Moment Equilibrium:



ΔT also ignored.

$\Delta P, \Delta T$ ignored.

Equation of F_s becomes implicit equation. Use
Transcendental
 Numerical methods. Trial and Error



Slice

$b = L_n \cos \alpha$

Force equilibrium not satisfied.

Slide width doesnot have to be equal.

Example 13.9

$c, \tan \phi$ constant

$\frac{b}{m_2}, \frac{W_n}{m_2}, W_n \sin \alpha$ evaluate $\frac{b}{m_2}$ & $\frac{W_n}{m_2}$

* Avg ht of two edges.

চাঁদ না থাকলে α বের করতে trigonometry use.

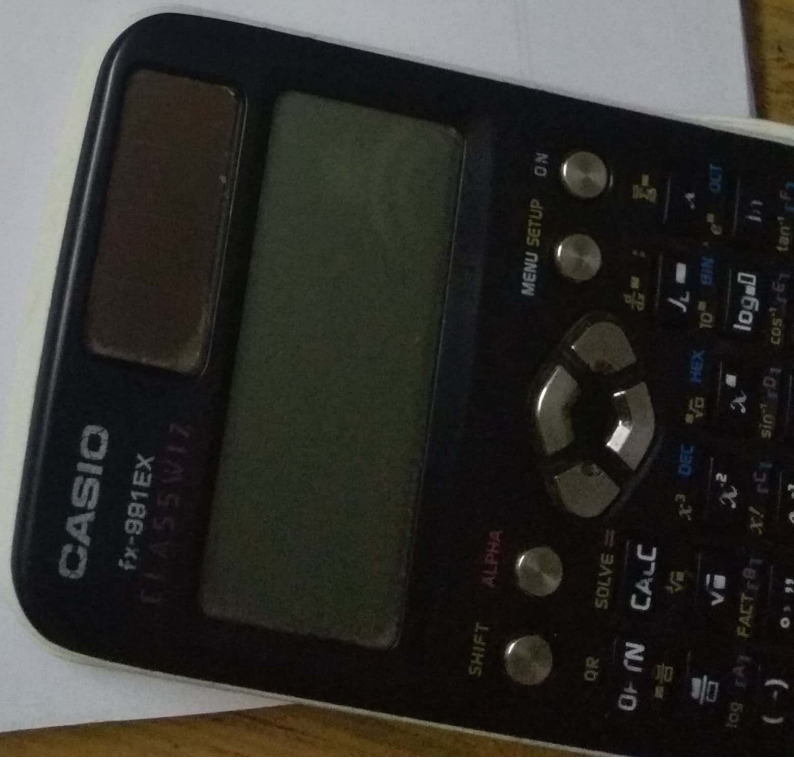
Math এ $\frac{bn}{m\alpha}$ column নাই। Add করতে হবে।

*Comment: Analysis have to revised ~~us~~ considering lower FS. [যদি FS=2 বিয়ে finally 1.60 আছে, কিন্তু revise করে দেখানোর দরকার নাই]

Computer ব্যবহার করলেও limit equilibrium দিখে check.

Layered soil: Affect W calculation. Ordinary method applicable.

c, ϕ avg করা যেতে পারে অথবা layer এর area বের করে করা যায়।

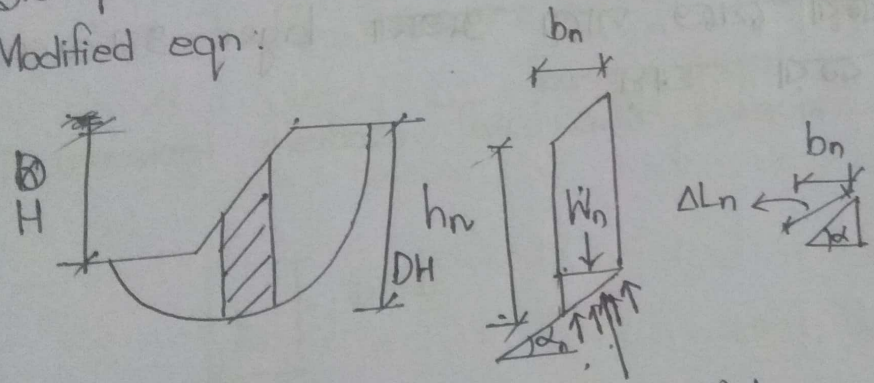


Ordinary method of slices

- Considering wt at great depth
- Considering pore pressure.
- Weight component reduced due to buoyancy force.

For Bangladesh, rain should be considered as a big factor
Bracing system: Horizontal I-joist and Shore pile.
Contractors delay may cause damage to road and utilities lines. ~ if slope fails.

Bishop's method of slices doesnot consider wt
Modified eqn:



$$u = \gamma_w h_n$$

u perpendicular to surface area (inclined)
To develop charat, non-dimension equation.

a = non dimension parameters
= avg ht of slice.

$$F_s = \frac{1}{a} \times \sum (b - c r_u)$$

$m - n r_u$

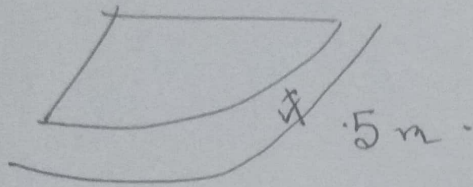
r_u differs from slice to slices For, different slices c.s. (Exam)

Re assume to be 1.

Top of seepage water,

BD river bank = 0.7

Toe surface:



Example.

Critical β_s \neq β_s = विद्युत -

Interporation = उदाहरण इकाय विद्युतक.

C.W

* ~~Multiple~~ ~~Beam~~

দেখানো হবে।

Morgenstern method of slices for rapid drawdown curve
যাগুলোকে যুক্তি না হলেও catchment India তে আকার
নদীতে সানি বেড়ে যায়। কয়েকদিনের মধ্যে Rapid
drawdown.

- Low permeability - Seepage pressure - Critical.
- Large fluctuation in water level - flash flood -
- Flood protection embankment.

Polder = প্রলাকার চারপাশে খাঁড় দেয়া যেন ভিতরে
dry থাকে।

$\gamma_{sat} = 2 \gamma_{water}$

Graphs :

Example :

$$\left. \begin{array}{l} c/\gamma H \\ \tan \beta \\ L/H \end{array} \right\} = \text{Stability number}$$

$\rightarrow F_s$

* interpolate করা যাবে। $(\frac{c}{\gamma H}$ or $\beta)$

Spencer's solution for stability of simple slope with seepage Bishop's method only takes into account moment equilibrium. Spencer considered all inter-slice forces. Trial and Error / Graph method F_s ବେଶ୍ କରା ଯାଏ ।
 r_u = non-dimensional pore pressure parameter.

Example 13.11.

Fluctuation of F_s of slopes in clay embankment on saturated clay

Shear stress becomes constant

Pore pressure dissipates.

At final height \sim min $F_s \sim$ at the time of construction.

To prevent this, stage loading or ground improvement.

Question pattern will change.

L-15

Date: 23/07/19

Deep Foundation on Sand

General discussion on pile foundation.

Classification according to depth

1. Shallow:

Strip: Wall
Individual
Combined
Mat / Raft

2. Deep:

Pile, Caisson, Well foundation

1. $D_f/B \leq 2-4$ (Not a stringent defn)

* Types of foundation

* Applicability (Load and soil condition)

Bridges + River adjacent structure = Unsupported height + Scour depth.

For Padma bridge, scour depth 60m, pile 120 m.

For transmission towers, significant lateral load, shallow foundation will be uplifted.

Raft and Mat has different design principle.

↓
Structure load < Soil load
Displaced soil
weight

5-6 কন্ক্রিট কন্ক্রিট 15-20m depth boring

Structure type.

Khulna = compressive soil.

Bored pile = 16" dia

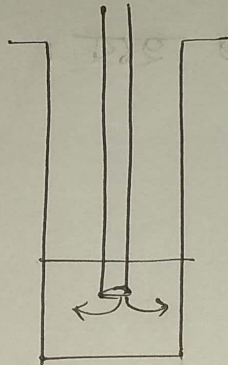
*Types of Deep foundation

- Material (RCC / steel)
- Construction / Installation Process

- ~ bored
- ~ driven pile (steel, hollow)

Steel: Hollow ; driven (River Jetty) : Easy to transport ^{steel}

RCC : bored / precast Tremie pipe. (May) be prestressed



Tremie pipe will always be under concrete surface.

- Segregation
- Mix with soil and water.

PHC = Prestressed Hollow Concrete pile

Dia = 1200mm

Wall thickness = 150 - 250 mm.

f_b MPa / 110000 psi

Strength / Longevity high

Cost less

Steel corroded / eaten by coral in marine environment

Driven pile based on type of driving mechanism.

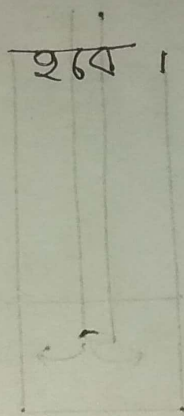
* Advantages and Limitation of driven + bored pile equipment + heading, Splicing

*Quality Control / Assurance Pile load test

Soil investigation এর সাথেই test pile এর উপর static and dynamic load test অথবা পরে service pile test (1-2%) but rectifying measures are not much available. উচ্চ building story এর limit.

Pile integrity test
Non destructive. Soundwave.

Tender এ mentioned থাকতে হবে।



Date: 30/07/19

C.W

Sat Sun Mon Tues Wed Thurs Fri

Factors of Safety

Justification by load sharing
Methods of Determining Ultimate Load Bearing Capacity

Single pile.

1. Soil and theoretical variation may be 2-3 times for the same zone.

3. Field test: relatively accurate, reliable.

For high rise building, field test must be done to verify the equations.

Pile construction এর দ্বারা spacing (3dia), symmetry break করে pile বাড়ানো যাবে, (eccentricity).

Load tests are costly and lengthy (2-3 months)
But safety and economy must be prioritized.

In the capacity equations, plane strain assumed.

but in real life piles are 3D. Only shape factors are applied to compensate.

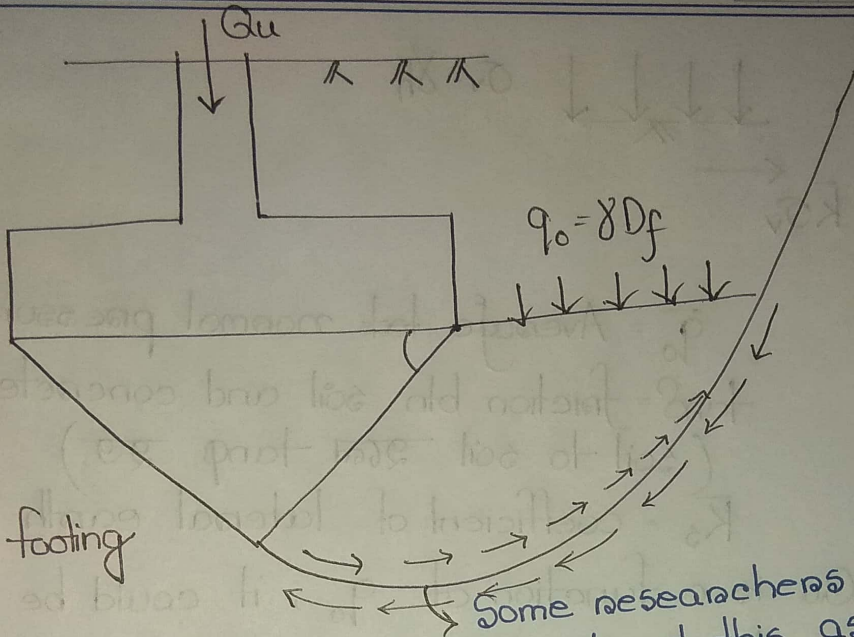
General Theory for Ultimate Bearing Capacity

For soil, deformation is very high at failure.

$$\bar{Q}_u = Q_u + W_p = Q_b + Q_f + W_p$$

$$Q_b = (C N_c + q_0 N_q + \frac{1}{2} \gamma B N_\gamma) A_b$$

Why N_c , N_q and N_γ values differs in different method?



* For footing

Some researchers considered this as parabolic/circle+straight line/logspiral. Hence, the difference in N_c, N_q, N_γ

* For piles.

Different failure pattern than footing. different q_0

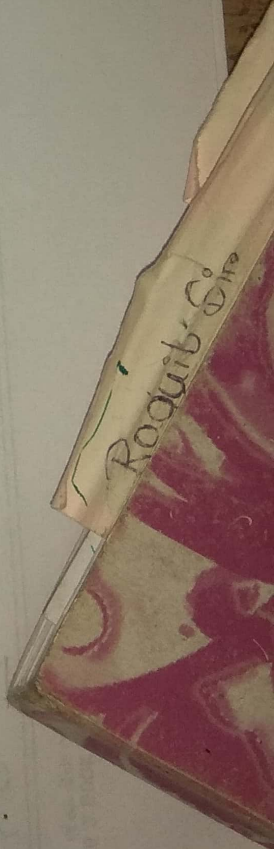
$cN_c = 0$ [Cohesionless]

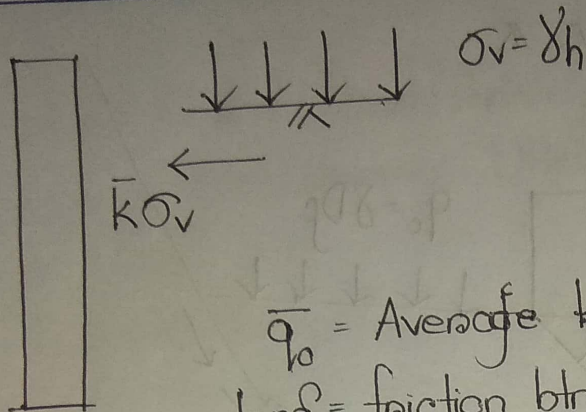
$\frac{1}{2} \gamma B N_\gamma \approx \text{negligible}$ [Pile dia = B very small]
[Safer as Q_u is smaller]

$Q_u = q_0 N_q A_b + A \bar{q} K_s \tan \delta$

Soil friction parameter = $\tan \delta$

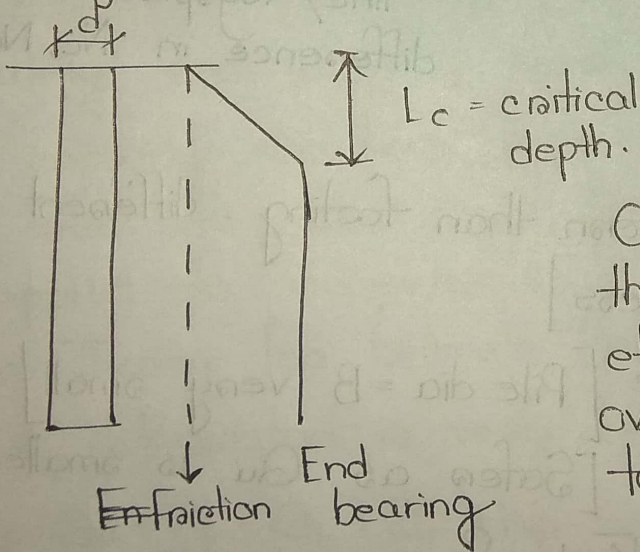
Friction force = Friction factor \times Normal force.





\bar{q}_0 = Average ~~let~~ normal pressure.
 $\tan \delta$ = friction b/n soil and concrete.
 (soil to soil δ \leq $\tan \phi$ \leq δ)
 K_s = coefficient of lateral earth pressure.

Since Q_u is a function of q_0 , it could be expected that $D_f \uparrow, Q_u \uparrow$. But in reality that doesn't happen after a certain depth.



Only in granular soil, there is an 'arching' effect which causes overburden pressure to not increase.

N_q from different curves:

ϕ can be assumed if not given (according to $\frac{L_c}{D_f}$)

C.W

Ref: Murthy (3rd Ed)

L-18

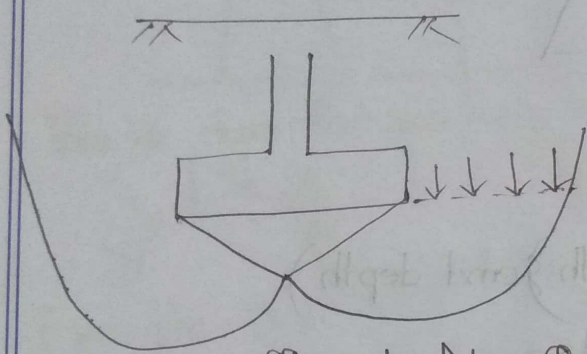
Date: 24/08/19

Chapter 8: Deep Foundation

For cohesionless soil, $Q = q_0 N_q A_b$ [$c=0$]

$$N_q = f(\phi)$$

N_q will be different for pile than footing as failure block will be different.



Failure block
for
footing

11 টি different $N_q - \phi$ curves.

Maybe diff dependent on $\frac{L_c}{d} = \frac{\text{Length of pile}}{\text{Dia of pile}}$.

N_q varies wildly

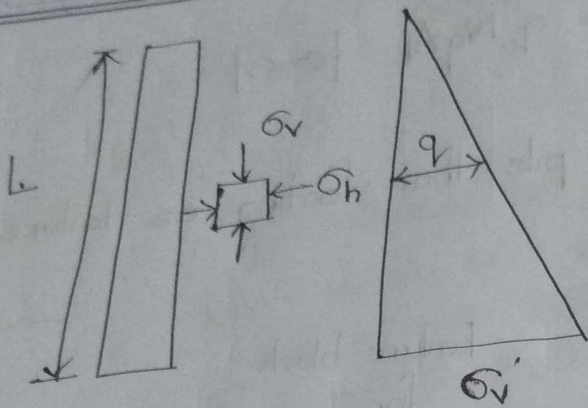
Maxm base resistance = 11000 KN/m^2 [Based on experimental findings]

* Theoretically এর চেয়ে বেশি
প্রাপ্ত হলে maxm নিতে হবে।

$$F = N \cdot f$$

= $N \tan \delta$ [Soil to concrete, δ = Angle of wall friction]

= $N \tan \phi$ [Soil to soil]



$$\sigma_v = \bar{q}$$

$$\sigma_h = k\bar{q} = N$$

$$F = k\bar{q} \tan \delta \quad (\text{per unit length and depth})$$

$$F = P k \bar{q} \tan \delta \quad (P = \text{perimeter})$$

$$Q_f = \int_0^L P k \bar{q} \tan \delta \, dz$$

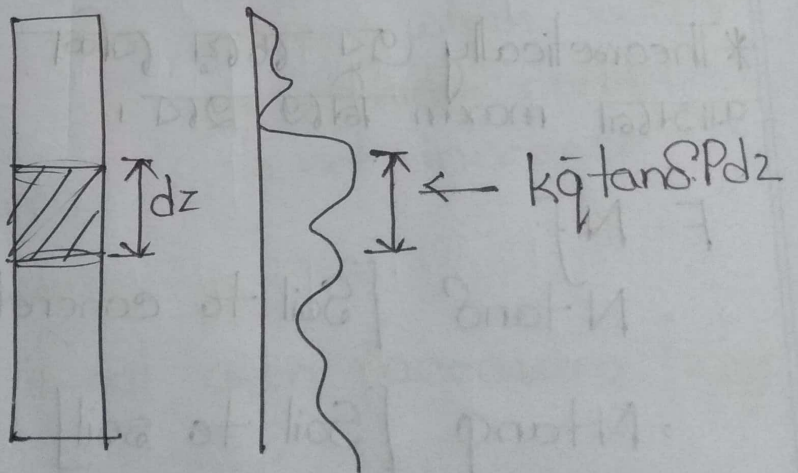
Triangular σ_v কে সুবিধে জানতে হবে)

Non-homogenous soil

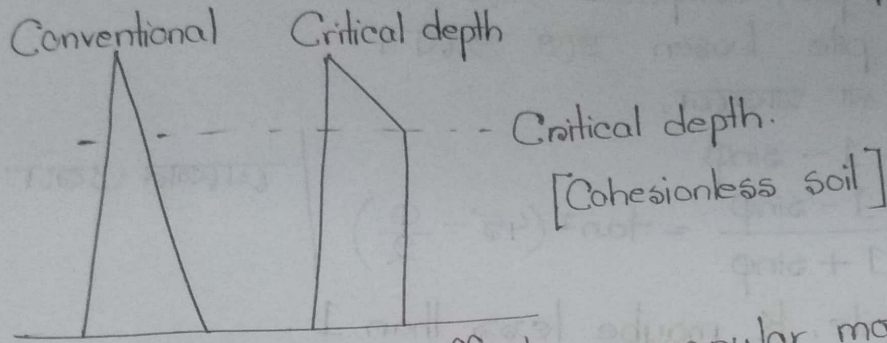
$$\sigma_v = \gamma' h$$

(Since, $\gamma' < \gamma$,

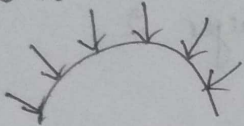
saturated অবস্থায় capacity কম থাকে)



Overburden pressure doesn't increase linearly with depth of embedment after a certain critical depth.



This is due to arching effect in granular material.



Example 9.1

$FS = 3$ [Minm 2.5]

Assume depending on soil homogeneity and confidence in determination of properties FS can be taken as 4.

* যইধে ভুল $Q = A_b q'_b$ হবে।
 $q'_b = 9 \times 7.4 + 4 \times 11.2$ হবে

$d = \text{dia (circular)}$

= smallest dimension / eqv dia (rectangular)

ϕ from Table 3.6. Interpolate না করলেও হবে।

যেহেতু base resistance, bottom layer ϕ লাগবে।

Limiting value 11000 নিব।

$\bar{q} = \text{Avg pressure} = \frac{0 + 9 \times 7.4}{2}$

K depends on compaction:

Driven pile: compacted হতে থাকে
 Bored pile: loosen হতে হবে।

* Table না থাকলে,

$$k_0 = 1 - \sin \phi$$

$$k_a = \frac{1 - \sin \phi}{1 + \sin \phi} = \tan^2 \left(45^\circ - \frac{\phi}{2} \right)$$

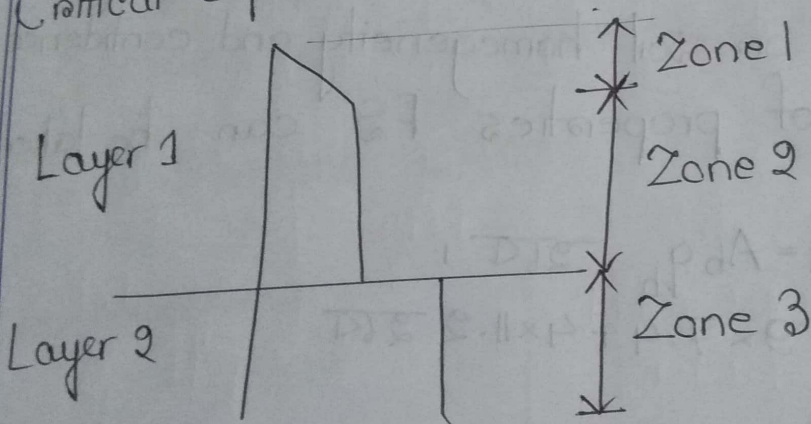
যেকোন একটা

Bored pile, K maybe less than 1.

\bar{q}_2 = Avg pressure at midpoint of layer 2.

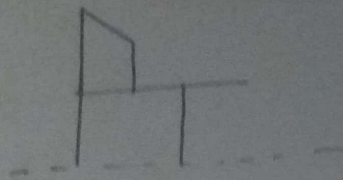
Limiting value for friction 110 kN/m^2 .

Critical depth consider করলে, 3 components



CW

Example 9.2



β -method (For cohesionless soil)

$$Q_f = \int_0^L P \bar{q}_0 K_s \tan \delta dz$$

For a given soil and pile material, β constant.

$$\beta = K_s \tan \delta$$

Poulos's curve will give greater friction than Meyerhof. So, Meyerhof should be used when conservative.

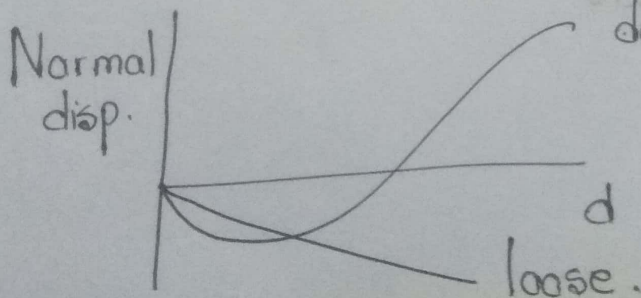
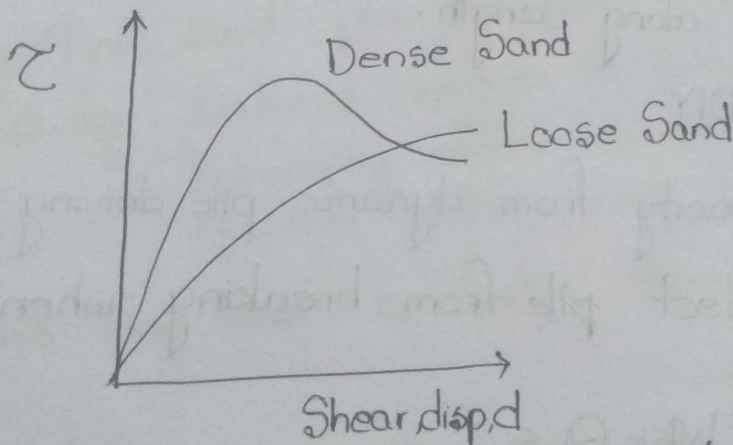
Boring friction < Driven pile.

When holes are made, soil becomes loose.

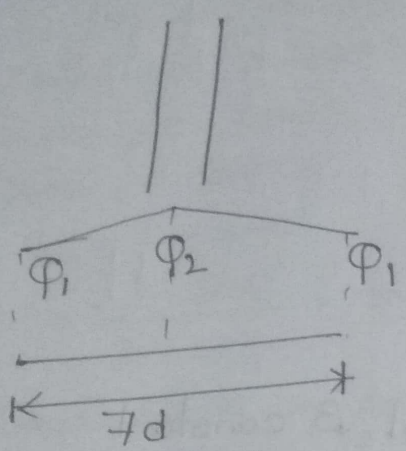
$$\phi = 0.75 \phi_1 + 10^\circ \text{ [driven]} \sim \text{becomes compact while driving}$$

$$\phi = \phi_1 - 3^\circ \text{ [bored]} \sim \text{becomes loose while boring}$$

যত ছুঁয়ে যাবে ϕ কমাবে।



dense (Dilatancy - Volm বাড়ে কারণ একটা particle আবেগের উপরে উঠে যায়)



$$\phi_2 = \frac{\phi_1 + 40}{2} \quad \phi_1 \text{ from test}$$

In situ $\phi = \sqrt{20N_{cor}} + 15^\circ$ (For sand)

* Example 9.1, 2 లో ϕ modify કરવા જરૂર નથી ।

Bearing capacity of piles in granular soils based on SPT-N

Unit sensitive.

N = SPT near end bearing zone

\bar{N} = avg SPT along length.

Example 9.3 DIY

Pile bearing capacity from dynamic pile driving formula.

Pile cap: to protect pile from breaking when driving.

Ideal condition, $Wh = Q_{us}$

Energy loss.

Hiley formula

η_h = hammer efficiency.

$$E = \frac{\sigma}{E}$$

$$\Delta L = \epsilon L$$

$$= \frac{\sigma}{E} L$$

$$= \frac{P}{AE} L$$

C_p = coefficient of restitution
= $\frac{\text{velocity after collision}}{\text{" before "}}$

Engineering News Formula

$$G_a = \frac{Wh}{6(s+c)} \quad \underline{F.S = 6}$$

Applicability is important

VIP Comments on dynamic formulae

Silty / Fine sand - pore pressure - liquefaction.

Sensitivity: Reduced strength in remoulded clay.
Thixotropy effect causes to regain strength within some time.

Dynamic load test is faster than static load test.

CW

Pile Load Test

Driven pile - Driving record থাকলেও PLT করা যায়।
 Different loading arrangement: vertical / uplift / horizontal
 Load বেশি resist করতে পারলে uneconomic.

" কঠিন " " " " ভাঙতে হবে।
 Test pile test purpose এ construct করা হয়।
 Pile হয়ে যাওয়ার পর test করতে চাইলে
 service / working pile.

PLT for bored pile requires 3-4 months.

But design revision is also difficult due to
 influence zone and group action.

So, design should be on conservative side.

Loading

Cement bag filled with sand on platform which is
 on girder than pile. Hydraulic jacking.

Certain eccentricity. Load $1.5 \times$ desired load
 to prevent uplift of platform.

Reference beam is used. It should remain static.
 Sufficiently long and away from pile command
 area.

Magnetic attachments to measure settlement.

For high load: Brick wall as supports.

on Anchor wall piles - tension

Active resistance < Passive

Tension pull

Compression

Loading Method

SM	Different load settlement curves.
GM	
CRP	
SC	

SM: (যদি করা যায়)

Design load from theoretical capacity.
 Reading each 5 minute until 0.25 mm/h or 2 hr.

Loading - unloading - reloading
 25% 25% 50% 10%
 2h 1h 20 min 20 min
 (design load) (failure load)
 যদি load ইনলে কাত
 হয়ে পড়তে পারে, so
 pre-planning reqd.

GM:
 5 min loading, 2.5 min loading,

CRP:
 Settlement $\sim 0.05 \text{ in/min}$, 2-3 in

Limitation: ① Run length of jack }
 ② If service pile, it will become useless } 2-3"

SC:
 Cyclic loading
 A silo where loading-unloading is unimportant SC
 is done.

Dynamic load test is also done along with SM.

Perpetual Pavement

Traditional lifetime = 10-15 years, then maintenance.

In BD, $\text{সিঙ্ক্রিয় উল্লঙ্ঘন}$: Huge deviation from standards.

Perpetual ~ lifetime 50 years with routine maintenance.

~ no capital intensive redesign required.

~ costly initial development.

Full-depth pavement ~ binders in all layers

Tension zone: ~ bottom layers tension. Migrates to top. Req's high elastic range.

Fatigue resistant. High amount and high quality binders.

Compression zone: ~ $\text{সিঁট$ strong foundation. উপর compression layer

Abrasion zone ~ Surface will take wheel wear and tear.

[G. Conceptual Figure important]

Considerations:

Compression members are perpetual. But pure compression members are hard to make.

Arch = pure compression member.

= after installing keystone,

pressure only increases stability)

Though factor of ignorance was high in ancient structures

Roads have continuous support, it should be stable.

Soil properties vary both horizontally and vertically.

Hard to achieve uniform construction. Staggering density.

Following data:

C.W

Ref: Sharma, Prakash

L-21

Sat Sun Mon Tue Wed Thu Fri

Date: 03/09/191

Lecture-6

Interpretation of Pile Load Test Data

Objective: Failure Load

Allowable load

Settlement (Dial gauge, outside reference beam
Failure pattern outside influence zone of pile)

Load settlement curve, showing failure pattern.
We want gradual/progressive failure, not sharp.

1. Davisson's method

Unit important inch

Quick maintained load test

For OA line, $\Delta = \frac{PL}{AE}$, BC limit line can be drawn before test. We can only test upto the limit for service pile.

2. Chin's method:

Δ/Q vs Δ (linear scale)

Slope = $c_1 = \text{Ton}^{-1}$, Failure load = $\frac{1}{c_1} \text{Ton}$.

QM and SM.

Limitation: constant time increments.

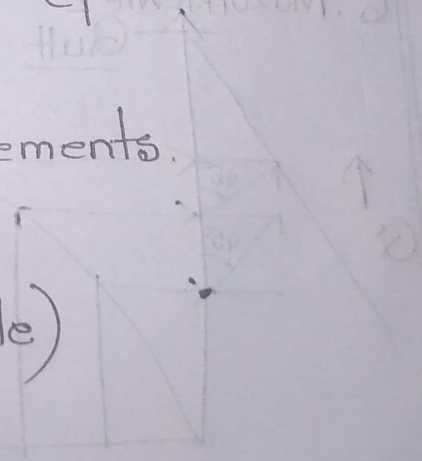
3. De Beer's method

Load vs settlement (Log scale)

Two straight lines (limitation)

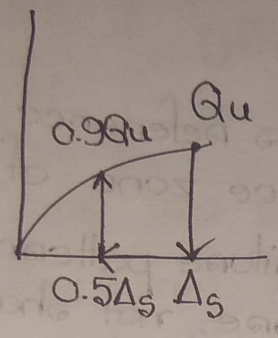
4. Brinch Hansens 90% criterion.

Linear



Qult

So, 90% Load at 50% deformation



CRP

5. Brinch Hansens 80% criteria

$\frac{\sqrt{\Delta}}{Q_{ult}}$ vs Δ

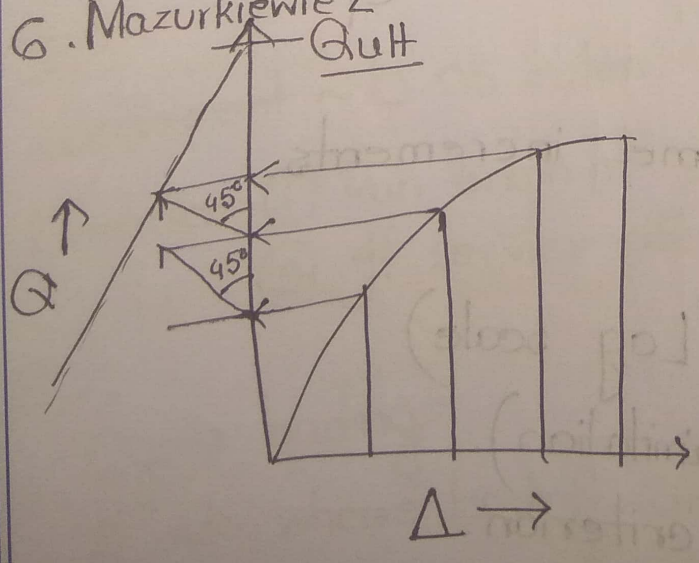
০ থেকে আকার দরকার নাই

$\frac{\sqrt{\Delta}}{Q} = C_1 \Delta + C_2$

$Q_{ult} = \frac{1}{2\sqrt{C_1 C_2}}$ (DIY)

SM, GM

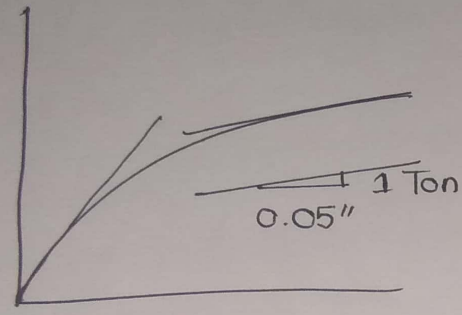
6. Mazurkiewicz Q_{ult}



Failure load, 80% criterion method same.
Limits: Not all points fall in straight line.

7. Fuller and Hoy's

Slope = 0.05 inch/ton. QM. long pile.



→ Draw this then move to match tangent parallel.

8. Butler and Hoy's method:
Rebound on initial tangent.

9. Vander veens method:
Trial failure load (In scale)
Until straight line.

Differential 12mm

Allowable settlement বিবেচনায় নিতে হবে 25mm।
* Find pile failure, Qult determination in BNBC
Justify the above methods.

C.W

Sat Sun Mon Tues Wed Thurs Fri

Pile Group

Most of the time: group pile
Isobar = Same pressure line.

Influence zones are created which reduces group pile capacity - to prevent that adequate spacing reqd.

If the pile causes displaced soil to be compacted then closer piles can be installed. Driven pile in sandy soil. Cast in situ installation does not impact the pile beside, so smaller spacing can be allowed.

- Minimum spacing $3d$ - (Soft alluvial deposit + Friction pile)
- $2.5d$ - (end bearing pile)
- $2d$ - (compaction pile)

Fig 11.2: Pile arrangements:

Building - (7, 8, 9)

Symmetric about both axes

Difficult to modify

Pile Group Efficiency:

$$E_g = \frac{Q_{gu}}{\sum Q_u}$$

100% means single and group piles have the same capacity

Sand

4 and 9 pile groups. $2d, 3d, 4d, 6d$. Effect of pile cap.

Maxm efficiency at $3-4d$.

Spacing এর যেকোনো ফিলে block effect হয়না.

Pile no যেকোনো ফিলে efficiency বারান

Spacing depends on column to column spacing.

Loose sand এ pile drive করা হলে $E_g > 1$ (Compaction)
 Dense sand এ pile drive করা হয়না. Dilation occurs

Bored pile in sand
 General loosening of soil.
 Soil yield করবে -

$E_g < 1$
 $E_g = 1$ (if optimum spacing maintained)

Preview: Settlement

Settlement in sand ~ Vertical

~ Lateral

We cannot measure group capacity as load test is done on single pile.

Settlement is not linear.

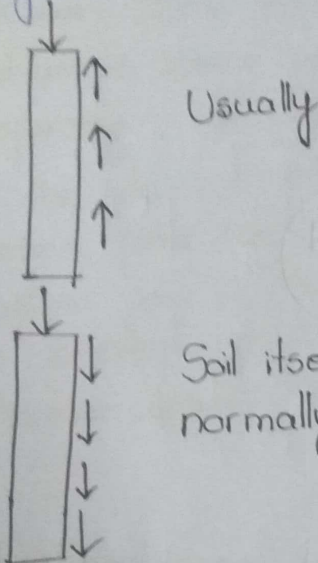
Models can be erratic.

Group factor, $F_g > 1$

$$S_g > S$$

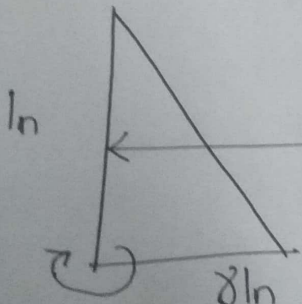
Settlement cannot be allowed more than 1" $B/d \uparrow F_g \uparrow S_g \uparrow$

Fig 11.3: Group Efficiency vs Spacing
Negative Friction



Usually

Soil itself is moving downward (soft, fill normally consolidated, recent deposit)



$$F = -\frac{1}{2} k \delta l_n^2 \tan \delta$$

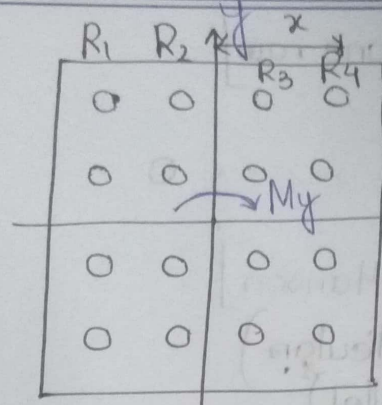
$$F = -\frac{1}{2} p k \delta l_n^2 \tan \delta$$

$$F_{ng} = s l_n p_g + \frac{\delta l_n A_g}{2}$$

↳ Soil to soil friction

$$F_{ng} = n f_i$$

Take maximum

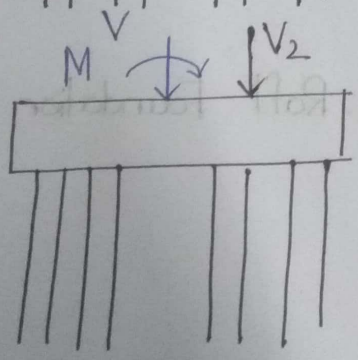
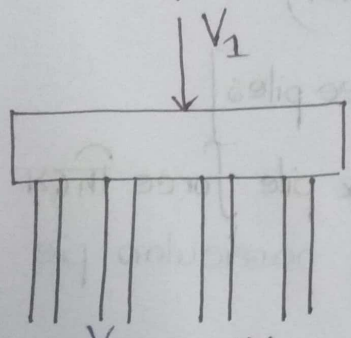


$$R_n = \frac{V}{n} \pm \frac{M_y x}{\sum x^2} \pm \frac{M_x y}{\sum y^2}$$

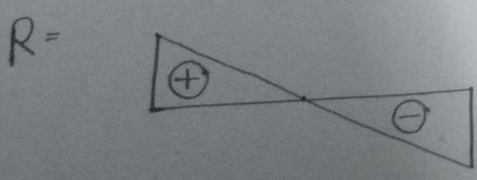
$$M = 4R_1 x_1 + 4R_2 x_2 + 4R_3 x_3 + 4R_4 x_4$$

$$= \frac{4R_1}{x_1} [x_1^2 + x_2^2 + x_3^2 + x_4^2]$$

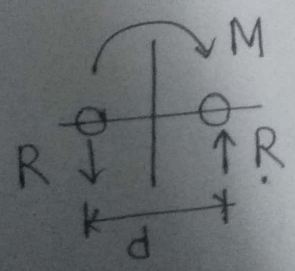
$\frac{V_1}{n}$ (V_1 cg and pile group cg coincide)



$V_2 = V + M$
 Moment from
 - eccentric loading
 - horizontal loading
 (Wind, Transmission towers)



As pile cap is rigid, reaction can be assumed to be linear.



$$M = R d$$

C.W

Sat	Sun	Mon	Tue	Wed	Thurs	Fri
			✓			

Date: 17/09/19

Raft Foundation
 Ref: Chapters 18 (Peck, Hanson, 2nd Ed)
 Like a combined footing. Shallow foundation.

Why are rafts chosen?

- ~ Basement [Although costlier than pile]
- ~ Individual footings overlap and covers half the area.
- ~ Underground space required due to height restriction (road width, analysis) airport)

Footing on clay:

$$q_d = cN_c + \gamma D_f$$

$$q_d = q'_d - \gamma D_f \quad \left[\begin{array}{l} \text{Overburden pressure থেকে কত} \\ \text{অতিরিক্ত load নিতে পারবে।} \end{array} \right]$$

$$= cN_c$$

$$= \frac{q_u N_c}{2}$$

$$q_{\text{safe}} = \frac{q_d}{3} = \frac{q_u N_c}{6}$$

$$N_c = f \left(\frac{D_f}{B} \right)$$

Figure 18.3 for q_{allow} vs q_u [FS=3, continuous footing]

For square and rectangular footing, multiply shape factor.

To determine pressure from column load,

$$q_{\text{net}} = \frac{Q}{A} - \gamma D_f = q_b - \gamma D_f$$

$$F = \frac{cN_c}{q_b - \gamma D_f} \quad \left[\begin{array}{l} \text{Theory} \\ \text{Field} \end{array} \right]$$

To $F \uparrow$ $q_b \downarrow$ $A \uparrow$

Raft foundation পুরে plot ঠিকে থাকে, তাই A বাড়ানো যায়না, তাই D_f বাড়তে হবে।

$$F = \infty = \frac{cN_c}{0}$$

$$q_b - \gamma D_f = 0$$

$$q_b = \gamma D_f$$

Fully compensated foundation. as if floating in soil medium [Archimedes]
 Anticipated load থেকে বেগি আসলে F দুট করে থাকে।

Example:

$$q_b, D_f = 20.5'$$

Available depth for basement = $20.5 + 3 - 5' - 1.5'$

\downarrow PL to EGL \downarrow Raft thickness \downarrow Slab thickness
 = 16.5' [One or 2 basement] 8.5'

For $F = 3$

Assume, $\frac{D_f}{B} = 0.1$ to determine N_c

(Assume less than 20.5')

$$F = 3 = \frac{cN_c}{q_b - \gamma D_f} \quad [\text{Use this equation or use the chart}]$$

$$D_f = \frac{q_b - q_a}{\gamma} \quad [q_a \text{ from chart}]$$

Determine F for any particular depth.

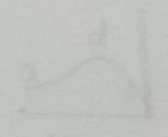
Chart use করা যাবে।

q_b 25% and 50% increase করলে F কত কমবে?
 \downarrow
 in % [non linear]

Effect of increase in load on factor of safety
Fully compensated foundation - y axis

Preview: Raft Foundation on Sand

Horizontal cutoff from settlement consideration
[Horizontal settlement = 2% (Horizontal cutoff)]



Water table depth
Connection required
Horizontal pressure to be calculated
It may be that where soil is heterogeneous
bearing capacity should be checked
in case of raft foundation

C.W.

18/09/19

L-25

Raft Foundation On Sand

$$q_d = \frac{1}{2} B \gamma N_{\gamma} + \gamma D_f N_q$$

$$q_d = \gamma_d' - \gamma D_f = \frac{1}{2} B \gamma N_{\gamma} + \gamma D_f (N_q - 1)$$

N_{γ}, N_q dependent on ϕ

B - smaller dimension

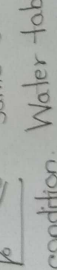
$$q_d = \left\{ \frac{1}{2} \gamma N_{\gamma} + \frac{\gamma D_f}{B} (N_q - 1) \right\} B \text{ Design Eqn.}$$

$$q_d = \frac{q_u}{F}$$

Chart given for $F=3$

Horizontal cutoff from settlement consideration (1")

Raft allowable settlement = 2" [Large rigid object]



some settlement curve.

Dry condition. Water table deep.

Correction required.

Overburden pressure to be calculated.

where soil is heterogeneous/large

Raft may vary

variability.

Bearing capacity doesnot gover in shallow

soil. $\frac{1}{2} B, \text{ far } \rightarrow \text{mountain}$

$B \neq D$

N- Corrected equation ~~for~~ Mats at

hom.

Bored notbook

Dewater

Dewater

वर्षा
fail - 20
One fr
Why 0.1
qu = 0

পানি ঢুকলে বা seepage হলে সামান্যই fail করে।

One-trick.

Why not 8' - ?

$q_u = 0.11N (1'')$

$q_u = 0.22N (2'')$