

29.9.15  
Saturday

Soil Mechanics

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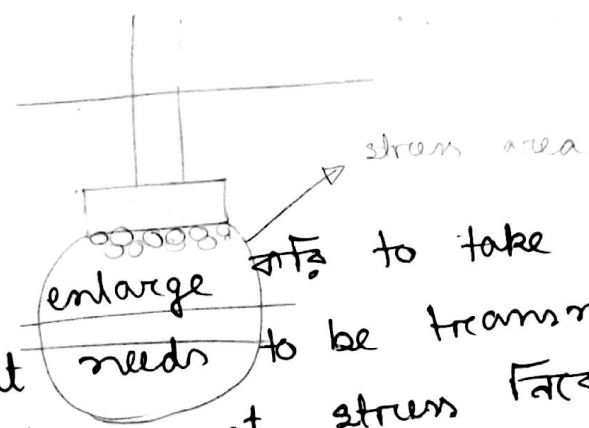
Lec - 1

CE - 341

Principles of Soil Mechanics:

Excessive stress and Excessive deformation are failure.

Soil is a granular mass, load particle to particle, individual particle like P/A.



Base of footing needs to take load. Footing loaded so granular mass. stress transmitted to base soil particle to particle stress distribute because of stress loading stress is propagated.

Smaller particle and voids, they are such particles want to go within soil. So void

Soil volume change, Soil & it can be filled with air, water or gas.

Soil is a three phase system.

2. Sizes of the particles will be varying.
3. Water filled voids develop pore water pressure (maybe).

\* Stress resist strength

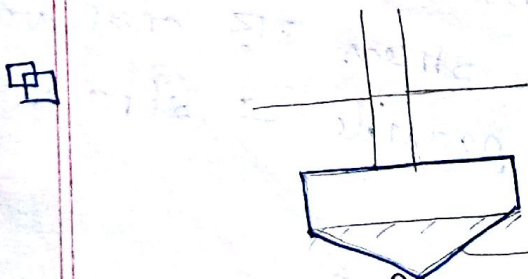
\* Settlement concept imp.

\* Permeability of soil.

3 properties:

- 1) Strength
- 2) Settlement
- 3) Permeability

} Engineering characteristic property of Soil



Immediate soil area compacted, so the whole material would be a wedge. Stress, wedge soil, lateral expansion.

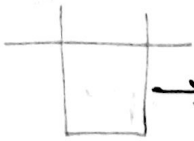
(\*) Soil



In some cases we want  $\downarrow$  permeability - like play ground.

Bank embankment  $\downarrow$  permeability.

(\*)



→ the whole soil collect  $\rightarrow$  its difficult & expensive foundation.

(\*) So we can have index properties of soil, like grain size  $\rightarrow$  strength  $\rightarrow$ .

These will depend on other properties of soil.

Some particles are very large, some small.

Depending on size & divisions

- 1) Gravel
- 2) Sand
- 3) Silt
- 4) Clay

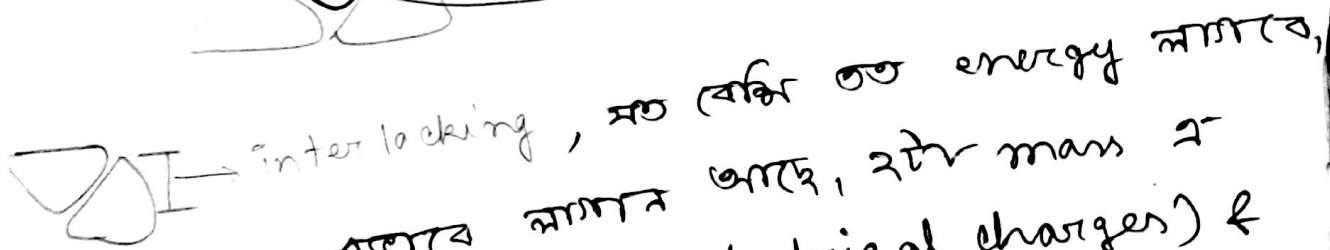
(\*) Soil is formed from rocks, rocks from minerals, minerals from elements.

Minerals  $\rightarrow$  base  $\rightarrow$  physical properties  $\rightarrow$ .

## Physical Property :

1) specific gravity : 2.60 - 2.65. ইনি খুবই heavy mineral হিসেবে বাসাত গড়ে খুঁজি

\* soil is particular failure surface বলা যায় না, Even we call the failure is a plane its actually wavy. cause mineral লেপেতে ইতি করে plane লাগতে ইতি, গড়ে possible না,



ইতি particle এটার কারণে energy লাগবে, vendar wall force (force electrical charges) & body force. So আলাদা করে bond লাগতে হবে, This bond এর ইতি energy depend করে,

(\*) কোন surface এ load দিলে (normal load) there must be induced friction. frictional property না থাকলে slipage হবে, & if the surface is rough.

(\*) So interlocking, cohesion, friction shear stress না জা. So we need to learn these.

\* BOOKS:

- 1) Foundation Engineering  
Peck, Hanson & Thornburn
- 2) principles of Geotechnical Eng.  
B.M. Das
- 3) Geotechnical Engineering Soil Mechanics  
Cernica
- 4) Craig → workout problem  
fluid flow through porous media

Lec-2Intro to soil Mechanics & Geotechnical Engg:Aspects of geotech:-\* Soil Mechanics:

that concerns with the mechanics and engg of soil

\* Rock Mechanics:

concerns mechanics of rock, not bed rock cause  
এই জন্যে stiff.

\* Engg. Geology:

1) Physical geology 2) Engg geology.

Fault / fold থাকলে foundation বিড়াবে হবে, কারণ  
place করে এদের মত analysis ~

\* Soil Engg:

soil mechanics এর knowledge use করে যে কাজ  
করে, when the foundation rests on soil

\* Rock Engg:

Rock mechanics এর application, when foun. rests  
on soil

\* Foundation Engg:

when foundation rests on soil and rock both.  
So soil & rock engg এর mix

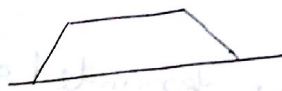
## \* Geoenvironmental Engg:

Earthquake, rain etc এর জন্য soil, rock এর change

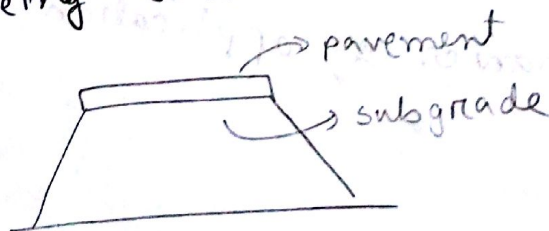
## ☐ Scope of Geotech:

- Foundation of structure
- Underground and earth retaining structure
- Embankment, excavation & dam
- Pavement
- Soil subsidence, soil heave, frost action, soil erosion, shrinkage and swelling

There needs to be a natural maintenance of slope when we excavate. Soil এর property এর উপর slope depend করে,



Pavement thin layer, এর উপর দিয়ে traffic যায়, এর embankment এর উপর বাক হয়, Thickness depends on underlying soil. The soil is called subgrade



soft soil  $\rightarrow$  load apply करने

flow of water  $\rightarrow$  soil eroded रहे, river bank erosion  
रहे और depends on shrinkage & swelling.



\* Inorganic soil - decomposition of rock

\* organic soil - " of organic matter

$\downarrow$  problematic

inorganic rock  $\rightarrow$  clay material और problematic.

According to size - 1) gravel

2) sand

3) silt

4) clay

clay size particle  $\rightarrow$  त्रि-विमीतीय dimension significant (bulky)

clay material  $\rightarrow$  प्लैकी (एक-विमीतीय त्रि-विमीतीय dimension prominent)

clay size particle may be bulky / flaky

flaky mat  $\rightarrow$  problem उत्पन्न charge carry करते.

usually -ve charge.

surface are एक-विमीतीय charge के लिए.

water can attract +ve & -ve. So when flaky part.  
comes in contact with  $H_2O$  उत्पन्न  $H_2O$  absorb करते.  
so उत्पन्न  $H_2O$  remove करना very difficult. As a  
reason the thickness of flaky particle increases

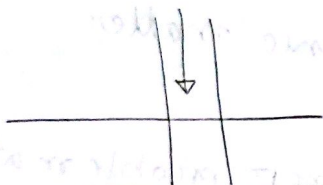
- Koolinite

- Illite

- Montmorillonite

} clay mineral

↳ এটা সবচেয়ে ছোট.



10 kN/m<sup>2</sup>

20 kN/m<sup>2</sup>

করবে & foundation expand

করবে, so 20 kN load (suppose)

↑ ছেঁড়ে যাবে.

So rainy এ ছেঁড়ে & dry season এ building নিচে যাবে. This is called shrinkage and swelling problem

## Development of Geotechnical Engg:

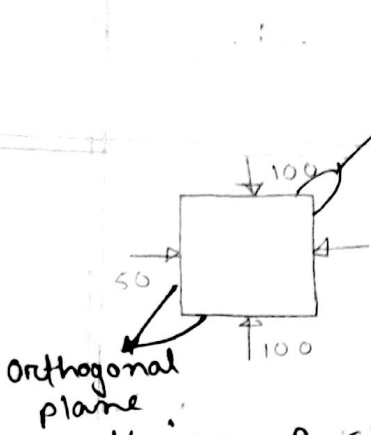
\* History of soil mechanics:

- i) Pre-classical
- ii) classical phase-I
- iii) classical phase-II
- iv) Modern
- v) Recent

⊛ Embankment এ circular slip surface এ failure ২৩



failure surface

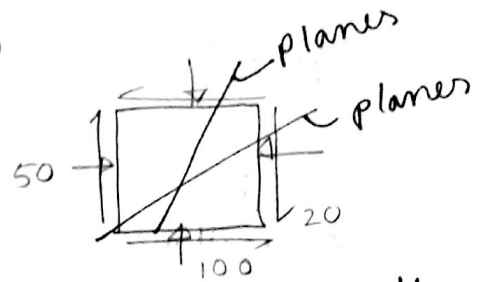


Stress element considered, the planes are orthogonal, when only normal stresses are there we call them principal stress.

Major P. stress :  $\sigma_1$  ( $\sigma_1$ )

Minor P. stress :  $\sigma_2$  or  $\sigma_3$

And shear stress is same on all planes, shear stress on plane is same as on other plane.



Mohr said we can draw a circle if we know the stress condition of orthogonal planes. (Mohr's circle of stress) circle of circumference is same.

\* Liquid Condition:

Condition of soil where the soil flows for its own weight.

\* Plastic cond: Mohr's shape given without cracks

\* Semi-solid cond: it is the condition of soil that can be given any shape with cracks

\* Solid Cond: No shape can be given.

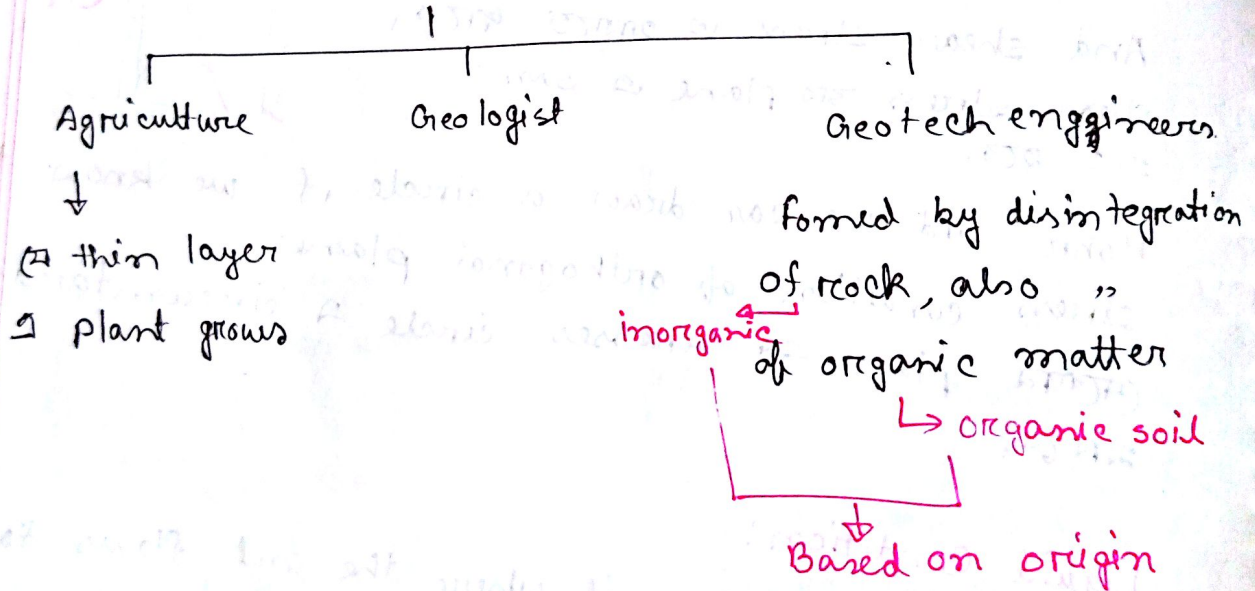
Limit of water content, after change state of soil (liquid) is not possible.

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Def<sup>n</sup> of Geotech:

Soil is used by diff professionals and their definitions are diff

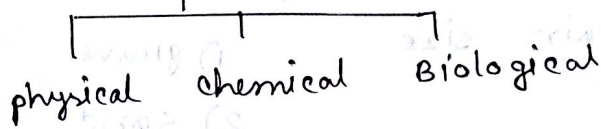


Def<sup>n</sup> of soil:

In our language agr. (मैटर soil वन) we call it top soil. For agr is good for us not, cause plants, organic matter वर shear strength वर. इकरा we remove top soil.

## Formation of Soil:

Disintegration of rock - weathering



Earth crust → rock & weathered rock

upto 20km depth → rock

Rock is formed of diff minerals

Surface → earth crust 80% sedimentary

Total volume → 90% igneous.

More than 4000 minerals. Only 8 are rock forming minerals.

## Earth Crust:

Based on silicate composition layers

1)

Crust

Mantel

--

Based on stiffness

② Mechanical layers

lithosphere

Asthenosphere

Meso sphere

Outer core

Inner core

Minerals can be expressed by chemical formula

Rock can't " " " "

↓  
Basic diff of rock & mineral

We can ~~and~~ classify rock on various criteria.

⊗ Formation History - 1) organic    11) inorganic

⊗ grain size

- 1) gravel
- 2) sand
- 3) silt
- 4) clay (size)

\* Minerals — 1) clay soil (mineral) → changes its property with water content  
2) non-clay soil

sand whenever confined is as hard as stone.

9. Underlining footing → sand/clay?

sand.

Monmorillonite is fine (1g fine) football field cover area, so extremely water absorbent.

So its expanding / swelling soil.

⊗ Igneous Rock

Metamorphic Rock

Sedimentary Rock

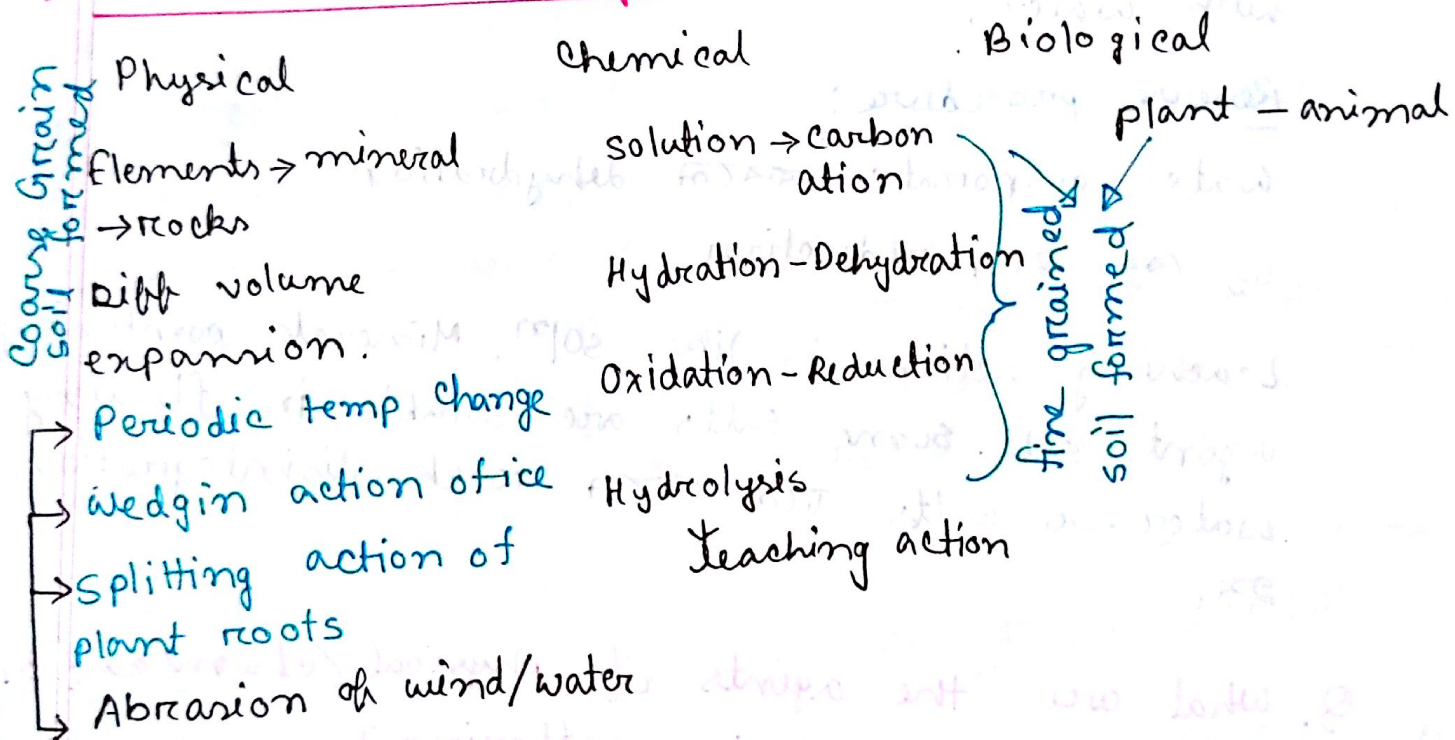
\* Diff bet<sup>w</sup> rock & mineral?

Rock → organic, made of more than 1 mineral, solid

Minerals → inorganic, solid, one mineral

Once rock is weathered it can be transferred and then deposited. With running water it is deposited and then called alluvial soil.

### Types of weathering:



Solid NaCl water is dissolved in water. So consistency change is, so soluble rocks in water disintegrate.

Cement & water form cement solid state. With mineral water is touch & water disintegration is.

Chemical composition of  $O_2$  with mineral.  $Fe + O_2 = Fe_3O_4$ . So iron solid, rust granular. So iron mineral is disintegrated. Usually redish color is.

water  $H^+$  &  $OH^-$  ସହ ମଧ୍ୟ disintegration  
ହୋଇ hydrolysis.  
water itself reacting is hydration

Carbonation rain +  $CO_2$  ବାର୍ଷିକ ବର୍ଷ, reacting  
with water.

### Reverse procedure:

Water evaporate ବାଷ୍ପୀଭବନ dehydration

$O_2$  ସହ ରକ୍ତ reduction

Leaching action is like sol<sup>n</sup>. Minerals combining  
agent salt. Some salts are soluble in flowing  
water. So salts ତଳେ ଗଲେ rock disintegration  
ହୁଏ.

Q. What are the agents of physical (chemical/Bio)  
weathering? (What is weathering?)

### Biological:

Soil (ମୃତ୍ତି) plant (ଜୀବ) ବାଷ୍ପ, rock (ପଥର)  
ବାଷ୍ପ, plant/animal enzyme secretion ବାଷ୍ପ,  
enzyme changes rocks. Enzymes are weak  
acids. So action done by insects, plants  
ହୁଏ biological.

## ☐ Factors Effecting weathering :

1) Temperature

2) Precipitation

Climate conditions control weathering

So Saudi Arabia ☉ (ଅଧିକ) weathering Bd ☉ (ଅଳ୍ପ) (ଅଧିକ) ☉

## \* Physical weathering :

### \* stress release :

Usually rock depth ଏ ଅବସ୍ଥାରେ ଏବଂ ଡେପ୍ଥ vertical soil or other ଠା pressure (ମାତ୍ର) (ଅଧିକ) overburden pressure Earthquake or any reason → pressure release ହେଲେ volume expansion ହେବ, so disintegration ହେବ।

→ Rock formation ସମୟ ଠା edge sharp ହାଏ, କିନ୍ତୁ ଅବସ୍ଥାରେ, abrasion ଏବଂ ଅବସ୍ଥାରେ edges rounded ହେବ, rock ଛୋଟ ହେବ।

→ Splitting action for larger trees, Biological for small plants.

## ☐ Soil Profile & soil Horizon:

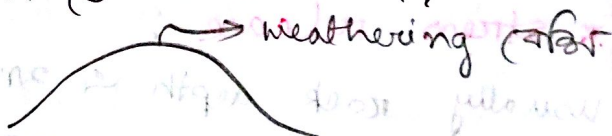
- 1) Whenever transporting → 1) transported soil
- 2) Staying at place → 2) residual soil

residual soil & transported soil are property different.

Residual soil is lazy soil. Transported soil

ভাল.

Residual → rock disintegrate হয়, degree of weathering will depend on depth. যেহেতু weathering বেশি, 30m পর্যন্ত হল নাহা, Russia এ 100m এ হয়, but its exception.



### \* Horizon:

A → intense weathering

B → কাজ "

C → কাজ বেশি "

D → কাজ " "

soil profile & Horizon same

↓  
layering of transported soil

↓  
layering of residual soil

↓  
~~strata~~ strata 1, 2, 3, etc

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Soil of Bd:

Seven tracts. (morphological)  
3 soils - 1) recent alluvium 2) old alluvium 3) ~~old~~ raised alluvium ~~old~~

Most soils silty material.

# Modhupur: old alluvium, redish

# Tista silt:

# Bramhaputra Alluvium: Biggest tract

# Deposits: 6 types

# Geotech soil of Bd:

P.T.O.

## Chapter - 3

### Soil Deposit, Type Structure & Classification

Type is generalization

Classification more specific.

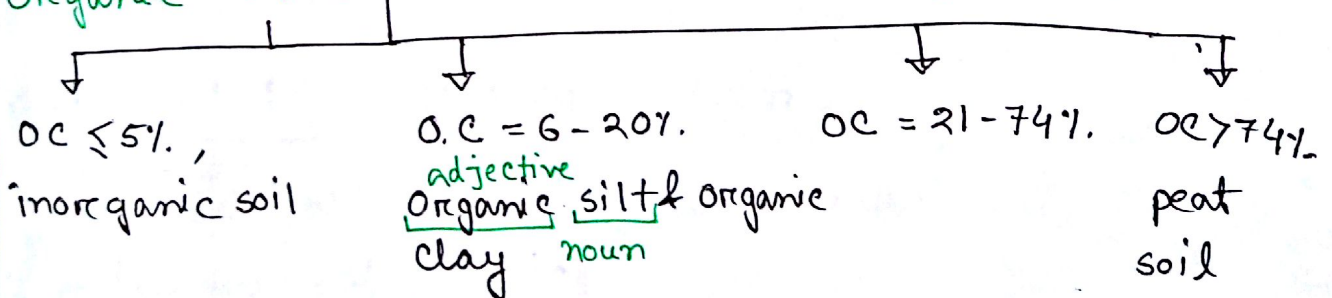
#### Classification:

Classification এর জন্য criteria is a must  
soil এর inherent property হল cohesion.

#### \* Classification Based on Reposition:

- 1) Organic → " of organic matter
- 2) Inorganic → disintegration of rock

Organic soil (formation time এ time grained)



#### \* peat soil:

very low shear strength

High compressibility - deformation করে, settlement হবে

অনেক পানি ধরে রাখে, like sponges

organic soil dark / black in color.

## # Inorganic Soil:


Residual Soil: (~~blackish~~ / Yellowish)  
redish

- 1) Laterite → mostly ~~coarse~~ fine grain, ~~100%~~.
- 2) Laterite → mostly ~~fine~~ coarse grain soil > 90%.
- 3) Black cotton → water contact, swells in volume  
very rare, cotton ~~जमा रहे~~.

## Transported soil:

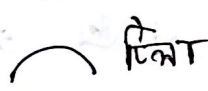
- 1) Water ~
- 2) Glacier ~
- 3) Wind ~
- 4) Gravity ~

## # Water Transported Soil:

- 1) Alluvial → deposited in running water condition,  
~~जमा रहे~~
- 2) Lacustrine → deposited in quite water, ~~बिना बिना~~  
very fine mat, very thin layer of soil.  
  
silt  
clay  
silt
- 3) Marine → ~~जमा रहे~~
- 4) Marl → deposit contains  $\text{CaCO}_3$ .  
 $\text{CaCO}_3$  dry ~~रहे~~ mudstone

## Glacier Transported soil:

glacier move করার অঙ্কন rock নিয়ে আসে  
plane land এ আসলে melting এর বেগ depend  
করে diff.

- Glacier Till → unstratified layer, **Glacier Drift**: sorted + unsorted  
Boulder clay → বুল্ডার ছোট & বড় deposit  
Moraine →  স্তম্ভ  
Drumlin → ড্রুমলিন  
Eskers → আকা বাকা বাঁধ  
Erratics → ~~কিছু কিছু~~ large man

## Wind Transported soil:

Dunes → high quantity of sand

Loess → silt, compaction ↑ রক্ত structure collapse  
করে & water এর জড় flow হয়, এটা mud  
flow & collapsible soil

Tuff - volcanic ash দিষ্ট, Also called Tufa.

Problematic soil

## Gravity Soil:

Colluvial soil or Talus

colluvial soils are basically unsorted soil. Cause size of particle varies.

Alluvial & sorted materials will be there.  
So according to gradation this is uniformly graded or poorly graded.

### # Grain size :

1) Gravel      2) Sand      3) silt      4) clay  
Basic classification of size of particle, size range  
coarse grained      fine grained

# ASTM → सूचिका रतन sieve opening and corresponding classification.

- 1) number of sieve
- 2) size of sieve

200 sieve and ~~above~~ ~~below~~ 200 sieve hydrometer analysis  
करि, ~~analysis~~ पान रतन

3" - 12" cobble, Boulder > 12"

### # ASTHO :

larger than 2mm → Gravel

ASTM → coarse sand, ASTHO → gravel  
" " medium " , " " coarse sand

# USCS : Gravel, sand, fines

# British :

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### Field identification of soil:

Silt 2 Types 1) reacts with  $H_2O$  - Plastic silt  
2) doesn't, " " - non plastic silt

When we consider fine grain soil we consider  
1) silt 2) clay 3) fine sand 4) organic soil

Feel: clay smooth feeling  $\text{দাঁত}$ , sand  $\text{খসখস}$

Wooden hammer used, cause steel use  $\text{করলে}$  particle  
 $\text{ভেঙে}$  যায় in dry strength test.

$\frac{1}{8}$ " dia এর thread করতে গেলে গুড়া গুড়া হয়ে গেলে silt.

particle  $\text{বড়}$  হলে void size  $\text{বড়}$ , silt এ void size  $\text{বড়}$ ,  
so এটা দিয়ে water passes fast. so tapping এ  $H_2O$   
তাড়াতাড়ি  $\text{বে}$  হবে cause  $\text{বড়}$  pore size  $\text{বড়}$ ,

clay minerals have affinity to cations. field এ  
impurity  $\text{এ}$  water দিন cation attach হয়ে diameter  
of soil particle  $\text{বেড়ে}$  যাবে, so  $\text{স্বাক্ষর}$  clog  $\text{করে}$ ,  
This is called flocculation.

একসাথে  $\text{দুটি}$  particle ও তাড়াতাড়ি settle  $\text{করে}$ ,

## Classification Based on Cohesive Properties:

silt & clay  $\rightarrow$  charge লড়ে, এদের মধ্যে attraction force cohesion.

## Soil structure & fabric:

We always work with soil mass, not a single particle. So mixture of soils থাকবে, so property change হবে.

Arrangement of particles in a soil mass is called structure.

In general structure & fabric same.  
Clay soil এর " fabric বুলি।

## Macrostructure:

soil এ crack থাকলে (যাখনি চোখে visible) এর strength কম।



## Micro-...:

crack খালিচোখে দেখা যায় না।  
Micro এর based এ 5 cm এর কম।

## Single grain:

void বেশি - loose structure  
void ↓ - dense ,,

## 2. Honeycomb:

silty soil ३, charge दिले attract श्ये, ring form वार, झरळ void.

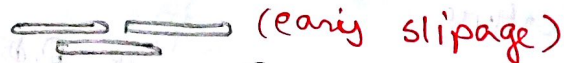


collapsible soil honeycomb structure, void ३  $H_2O$  श्ये & collapse.

## 3. Flaky structure:

३३ dimension, depending on diff charge arrangement diff.

parallel - Dispersed



(easy slippage)

Bundle - Packet or

ped, वा निचेर जावळ flocculated

flocculated -



(not easy slippage)

Dispersed ३ failure easy, shear st. वाझा comparison with flocculated

## Particle Shape:

Bulky - ३ dimension

Flaky - 2 "

little - 1 "

Angular shape desired cause interlocking वाळ

Angularity can be measured.

☐ sphericity:

$$S = \frac{D_e}{L_p}$$

☐ roundness and sphericity:

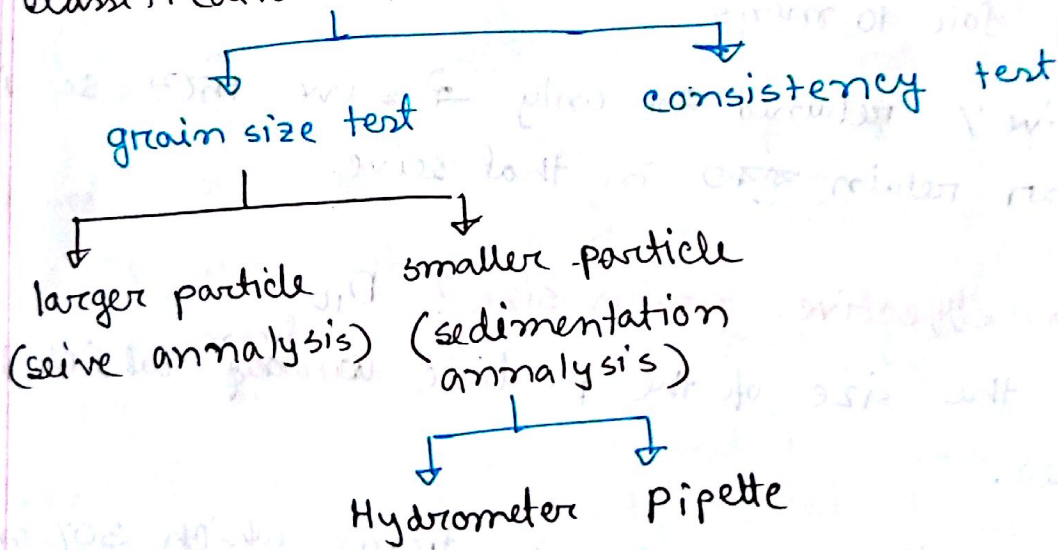
\*☐ Engineering Classification of soil: (most imp)

Several agencies classify as follows.

1) USCS

2) AASTHO

কোনো কোনো value আছে, সে test এর value করে (আর) classification test.



classification এর কোনো কোনো numerical value আছে,

Fineness modulus is the measure of coarseness.

But FM is not used in soil mechanics.

Q. what is classification test? এর ① grain size ann → coarse grain এর, consistency এর condition

☐ consistency test: fine soil এর strength. Depending on H<sub>2</sub>O content

strength changes.

Q. What is index value? property?

↳ The numerical results of classification test.

Seive Designation:

Mesh always square.

Number of linear length a square division

Horizontal shaking (not vertical shaking).

usually for 10 mins.

cumulative % retained only in seive sieving  
কম্পনে যা retain করত in that seive.

Q. What is effective grain size?  $D_{10}$

It is the size of the particle <sup>from</sup> which 10% is finer.

$D_{30}$  - it is the " " " " from which 30% material is finer.

$D_{50}$  (নরী) But for classification it's not important.  
সম)

① Uniformity Co-eff:  $C_u$

$C_u = \frac{D_{60}}{D_{10}}$ , यहाँ  $D_{60}$  बड़ा soil particle size है और  $D_{10}$  छोटा variation है।

② Co-eff of curvature: Spread of the curve

$C_z = \frac{D_{30}^2}{D_{60} \times D_{10}}$

यदि  $C_u = 1$ , then curve is vertical.

$C_u$  is a measure of spread of the curve.

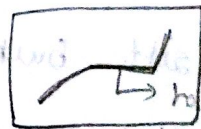
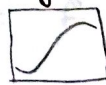
S shape curve is well graded soil.

Co-eff of curvature  $C_z$  is a measure of shape of the curve.

if  $1 < C_z < 3$  then S shape.

From  $C_u$  &  $C_z$  & curve we can determine gradation.

Gradation basically - well graded, poorly graded, uniformly graded, Gap graded.



horizontal line

3.10.15  
Saturday

## lec-6

### ☐ Grain size Analysis:

- 1) sieve analysis
- 2) sedimentation analysis

percent retained whole number, except #200 sieve.

if more than 12% or 10% is passing #200 100gm

soil then hydrometer / sedimentation analysis  
in some cases

### ☐ Sedimentation Ann:

Stokes Law  $\rightarrow$  larger particle, faster settlement.

sieve করা using #200, 50 gm soil, Then  
100cc jar এ soil + H<sub>2</sub>O মিশ্রিত 100cc করে, thoroughly  
mixed.

soil এ impurity  $\rightarrow$  salts ionized.

silt bulky / flaky, clay flaky.

flaky surface এ -ve, so সমস্যা +ve এর contact  
এ তখন একত্রে large particle form করে, so  
particle small হলে fast settlement. So prevent by  
Na Hexa metaphosphat defloculating agent.

অন্য -ve charge create করে,

vol<sup>m</sup> of suspension 1000 cc, After sometime density lower হবে cause particles settle হবে, After infinite time density H<sub>2</sub>O এর অক্ষান, So time থেকে reading বুঝি.

Density বন্ধনে hydrometer reading নিতে যাবে, Solid particle ফিলে S.G. determined হয়,

Intelligent hydrometer ব্যবহারি ~~disproportioned~~ ৩০ gm soil এর direct reading.

151H → density measured

152H → amount of soil in suspension.

usually 151H not used.

D = particle size

L = length of hydrometer

G<sub>s</sub> = S.G. of soil

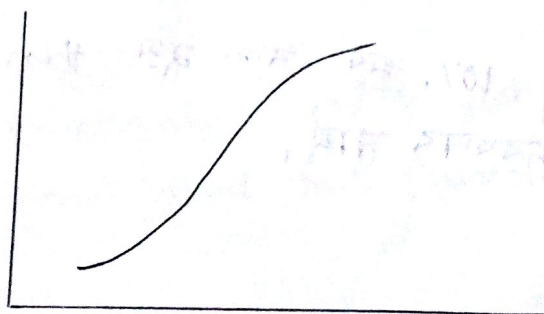
percent finer = N

V = 1000 cc

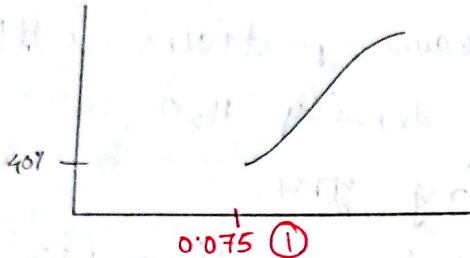
R = hydrometer reading

W = wt of soil usually 50 gm

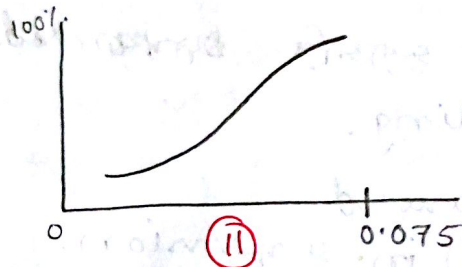
Grain size distribution curve



suppose 40% passes 200 sieve



So बाकिदार जस्य hydrometer max<sup>m</sup> dia 0.075.



अथवा % finer

$$0.075 - 100$$

$$0.05 - 80$$

$$0.033 - 73$$

① ए मोटे 40% , ①१ से मोटे 100%.

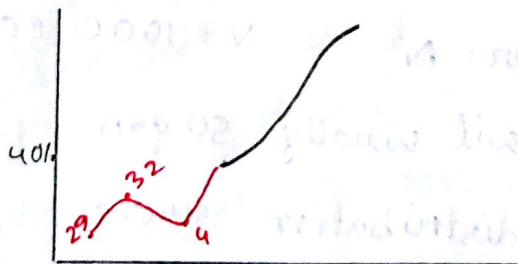
So % finer 100 को 40 बांटे रहे, 40

$$0.075 - 100 \times 0.4 = 4$$

$$0.05 - 80 \times 0.4 = 32$$

$$0.033 - 73 \times 0.4 = 29$$

So combined



मदि % passing 10% हव कम रूम then grain size analysis से दरकार नाई,

☐ Grain Size distn curve:

soil has high shear strength, deformation less.  
 for well graded soil.

⊛ If soil sand has  $C_u > 6$   $K_{Cz} < 3$ , then the soil is well graded sand.

⊛ But in case of gravel it's not correct.  
 If more than 50% is retained in #4, then gravel has  $C_u > 4$   $C_z = 1 < C_z < 3$  then well graded gravel

☐ 2nd Classification Test: Consistency test → Always passing by #40 sieve  
 Done for fine grain soil. water bipolar.



water has unique soil plasticity property. special property plasticity. Bipolar at same time. plastic property has na.

⊛ Limiting water contents are different.  
 for clay has unique limiting H<sub>2</sub>O diff, cause diff proportion of minerals.  
 So on minerals limits depend.  
 plastic soil not good for foundation. Shear strength  
 बल,

So कबल plastic तरै ना, So from limits we can conclude soil का ना काय,  $\tau = 1.7 \text{ kPa}$

Definition of limits:

liquid limit:  $w_L = \text{water content}$   $W_L = \text{weight}$

Small shear strength =  $1.7 \text{ kPa}$

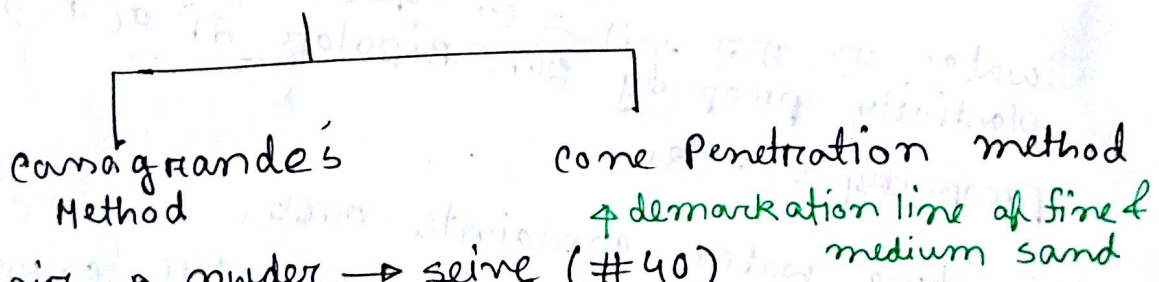
Plastic Limit:

Shrinkage Limit:

Smallest water content, saturated water content below this volume change  $\tau = 0$  even if we change  $H_2O$  content.

# small shear usually machine द्वारा करे जाये ना,

Liquid Limit Determination: for fine grain soil



Prep of soil

Dry in air  $\rightarrow$  powder  $\rightarrow$  sieve (#40)  $0.425 \text{ mm}$

mix with water  $\rightarrow$  keep for 24 hrs

thoroughly mix

7.10.15  
Wednesday

lec - 7

Determination of liquid limit:

1) Casagrande's Method: (Popular in USA)

25 blow  $\Rightarrow$   $\frac{1}{2}$ " close  $\Rightarrow$  it's in liquid limit.  $\Rightarrow$   $\Rightarrow$   $\Rightarrow$  soil  $\Rightarrow$  water content  $\Rightarrow$  then  $\Rightarrow$  error  $\Rightarrow$  water add

No. of blow	w. content
34	51
29	59
24	63
19	71
16	73

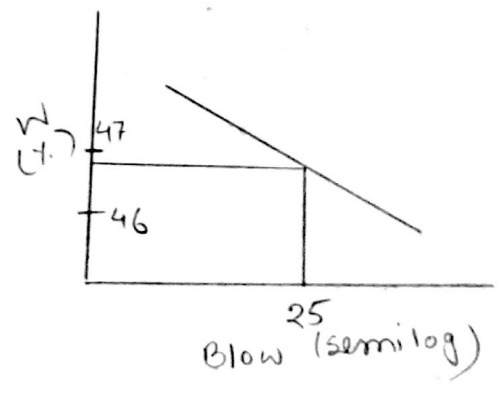
max 35  $\Rightarrow$   $\Rightarrow$  min 15 blows.

Try and error method.

25 blows  $\Rightarrow$   $\frac{1}{2}$ " closing  $\Rightarrow$   $\Rightarrow$  w. content liquid limit.

liquid limit whole number unless it's less than 10.

water 47  $\Rightarrow$   $\Rightarrow$   $\Rightarrow$   $\Rightarrow$  so it's 47.  
flow curve



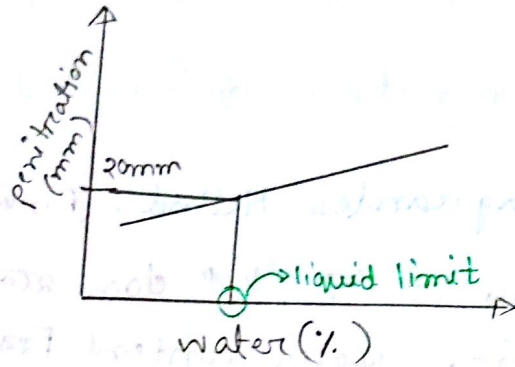
2) Cone Penetration:

penetration  $\Rightarrow$   $\Rightarrow$   $\Rightarrow$  surface  $\Rightarrow$  shear strength.

30 mm penetrate  $\Rightarrow$   $\Rightarrow$   $\Rightarrow$  liquid limit. suppose 12.5 mm  $\Rightarrow$ , so we need to add more water.

In scale  $\Rightarrow$   $\Rightarrow$  = 0.1 mm

previous  $\sigma$   $\times$   $\sigma$  blow  
 $\gamma$   $\sigma$   $w(\%)$   
 अथवा देखिए,



Q. What is flow index?

flow curve का slope flow index. इसे  $n$  strength measured

# we can use one point to determine liquid limit.

1st method  $\sigma$   $\sigma$  25  $\sigma$  काहे आकार के डाले.

Then for single point method in (1)

$$w_L = w \left( \frac{n}{25} \right)^{e-0.1}$$

$$= 63 \left( \frac{24}{25} \right)^{0.1} = 62.74 \approx 63$$

$$w_L = 71 \left( \frac{19}{25} \right)^{0.1} = 69$$

25  $\sigma$  काहाकाहि शकते better result

~~0.26 - 0.16~~

\* cone penetration  $\sigma$  single point method can be used

cone penetration for " " should be ~~26 - 16~~ 16.

26 - 16 (water content)

# Plastic limit almost 100% more strength than liquid limit.  
 folds

\* Plasticity index = diff bet<sup>n</sup> liquid & plastic limit

$$(PI \text{ or } I_p) = LL - PL$$

$$* \text{ Liquidity Index (LI or } I_L) = \frac{\overset{\substack{\uparrow \\ \text{natural water content}}}{w - PL}}{LL - PL} = \frac{w - PL}{I_p}$$

⇒ If the natural water content is LL or more then LI = 1. (soil soft)

⇒ if " " " " " " PL " " " " LI = 0 (soil stiff)

⇒ LL & PL of a soil is fixed, only determiner is w.

If a soil is dry then w = 0. So LI can be negative.

⇒ LI > 1 is unlikely, cause LI is when w increases flow starts, but soil slurry starts when it can be > 1.

$$\Rightarrow \text{Consistency Index CI or } I_c = \frac{LL - w}{LL - PL}$$

just reverse of LI.

⇒ Flow Index

⇒ Toughness Index: Measure of strength of soil =  $\frac{I_p}{I_f}$

□ Determination of shrinkage limit:

swelling soil can classify as [S],

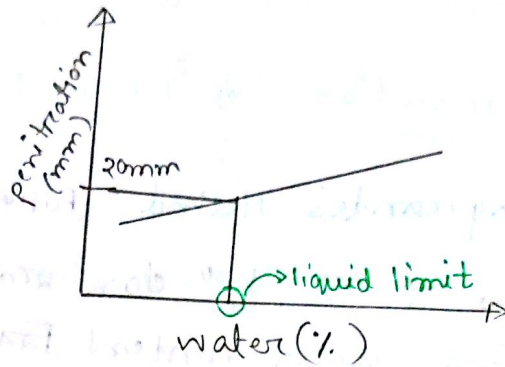
bet<sup>n</sup> solid and semisolid w-content.

Sh. Limit is the saturated water content of the soil at its minimum volume during the process of drying.

previous  $\sigma$  &  $\epsilon$  blow

$\gamma$  &  $w(\%)$

অথবা উল্লি.



Q. What is flow index?

Flow curve এর slope flow index. এর দিঃ strength measured

# we can use one point to determine liquid limit.

1st method এ যত 25 এর কাছে আসবে তে ভাল।

Then for single point method in (1)

$$w_L = w \left( \frac{n}{25} \right)^{e \rightarrow 0.1}$$

$$= 63 \left( \frac{24}{25} \right)^{0.1} = 62.74 \approx 63$$

$$w_L = 71 \left( \frac{19}{25} \right)^{0.1} = 69$$

25 এর কাছাকাছি থাকলে better result

~~0.075 - 0.25~~

\* cone penetration এর single point method can be used

cone penetration for " " should be ~~26-16~~ 16.

26-16 (water content)

# Plastic limit almost 100% more strength than liquid limit.  
↓  
fold



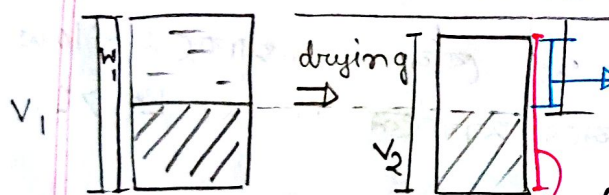
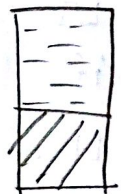
oven এ dry করলে irregular shape হবে, এই অবস্থায় (min volume এ) যে w content.

i) S.g of soil is unknown

ii) S.g " " " known

i) SG unknown:

When soil is made slurry then phase dia soil + water cause voids are filled with H<sub>2</sub>O



dry করলে এখানে air void. এর min volume. এখানে air না থেকে H<sub>2</sub>O থাকলে shrinkage limit

$$W_s = W_d$$

$W_1 - W_d$  করলে initial water weight.

$V_1 - V_2$  এ যে water content হলে কতটা water কমান,

This is  $(V_1 - V_2) \gamma_w$

$$\text{Shrinkage limit} = \frac{(W_1 - W_d) - (V_1 - V_2) \gamma_w}{W_d}$$

\* solid soil never changes volume.



irregular shape

এটার vol বের করতে mercury used.

এই পাত্রে mercury দেবে, whole soil shape immerse করবে, যে mercury replaced হবে ডিটর  $\frac{W_{Hg}}{13.6}$  হলে vol m.



## Determination of Linear Shrinkage:

Shrinkage कबि रतन length shrinkage measured.  
Linear shrinkage रतन  $\uparrow$  soil क poor. L. shrinkage  
कबि रतन deformation  $\uparrow$ .

Non-plastic soil better than highly plastic. Cause non  
plastic  $\rightarrow$  deformation कबि, Dry strength is not a  
criteria.

Relation LS, Plasticity Index  $\Rightarrow I_p = 2.13 LS$

Soil H<sub>2</sub>O क contact क कबि expansive रतन कबि  
see from shrinkage limit. SL  $\uparrow$  रतन linear shrinkage  $\downarrow$ .

\* Shrinkage potential low रतन when it comes in  
contact with H<sub>2</sub>O it will expand less.

## Significance of Indices:

Q. कबि index  $\rightarrow$  like flow, plasticity index  $\uparrow$  /  $\downarrow$  रतन कबि?

## Unified soil classification system:

Another classification is ASTHO.

construction  $\rightarrow$  USCS

Road, airport ASTHO

grain size characteristics and consistency test results used.

GW  $\rightarrow$  well graded gravel  
 ML  $\rightarrow$  silt of low plasticity

\* 100g soil, #200  $\rightarrow$  retained 52, passed 48. More than 50% retained  $\rightarrow$  #200 ~~is~~ coarse grain. So G or S. if passes 50 or more than 50 then fine grain. clay (C) or silt (M)

52g  $\rightarrow$  sieve through #4

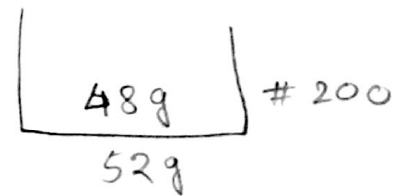
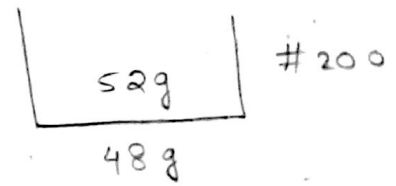
more than 50% retained

27	#4
25	

so the whole 100g will be known as gravel. So 1st letter G.

then 100g of whole soil is sand. So S.

25	#4
27	

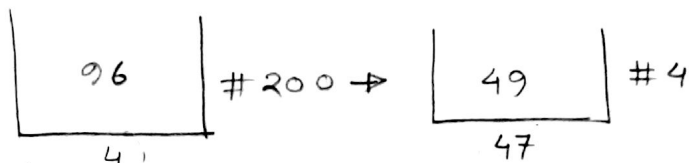


যখন G or S এর পরে সূক্ষ্মাকণা sieving by #200, 3, things are considered

- ① % passing #200 sieve  $< 5\%$ .  $\rightarrow$  clean Gravel / clean sand
- ② % " " " " " 5-12%.
- ③ % " " #200 "  $> 12\%$ .

Here % passing was 48g, so it's > 12%.

Again suppose



so the 1st letter is <sup>4</sup>G.

% passing #200 is < 5%, so we will call it clean gravel.

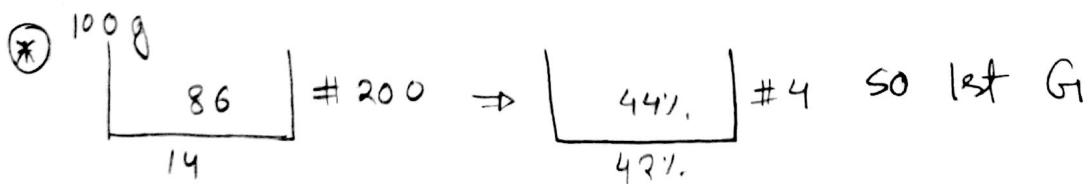
अगर clean gravel / clean sand अगर then to classify it the only criteria is Gradation (grain size)

Then if  $C_u > 4$  and  $1 < C_z < 3$  then it's called well graded soil.

So this soil is GW.

अगर  $C_u < 4$  and  $1 < C_z < 3$  अगर तब, then GP

अगर  $C_u > 6$  and  $1 < C_z < 3$  then SW. otherwise SP.



% passing #200 > 12%, then second letter determine <sup>New criteria</sup> can't use gradation. That's basically used for classifying fine grain.

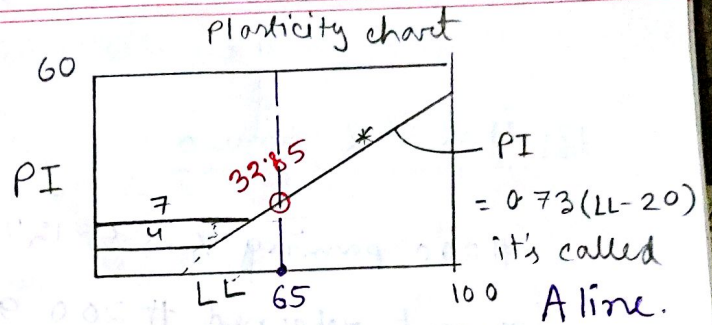
plasticity chart → Liquid limit vs plastic limit

$$PI = 0.73 (LL - 20)$$

If  $PI = 4$

and  $PI = 7$   $\rightarrow$   $U_{cl}$

if  $LL = 100$   $PI = 58 \dots *$



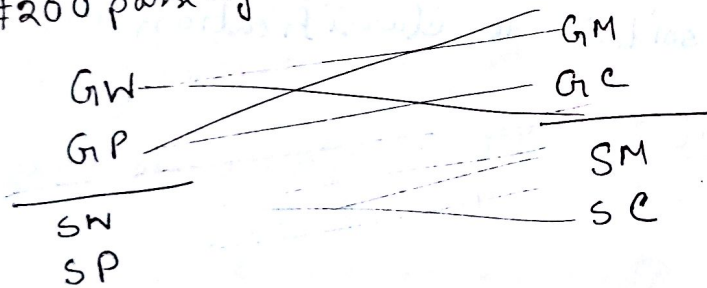
Suppose  $PL = 36$   $LL = 65$

$\therefore PI = 65 - 36 = 29$ ,  $(65, 29)$  A  $\rightarrow$   $\downarrow$  silt (M)  $\downarrow$  clay (C)

$$\therefore 0.73(65 - 20) = 32.85$$

32.85 on A line, 29  $\rightarrow$   $\downarrow$  silt (M), so it's silt (M).  
So it's called silty gravel.

#200 passing  $\leq 5\%$   $\# \dots \geq 12\%$



(1)  $\dots$

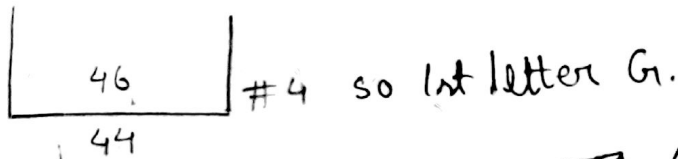
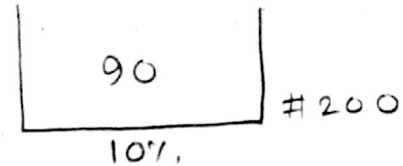
(2)  $\dots$

(3)  $\dots$

USCS Continued:

#200 passing % 5-12% 2(m) ⇒

percent retained #200 90



Here dual classification 2(m), (Previous pg 25(4) combination)

well graded  
silty gravel

- GW - GM
- GW - GC
- GP - GM
- GP - GC

and for sand SW - SM

- SW - SC
- SP - SM
- SP - SC

coarse grain soil 16 classification.

\* Fine grain soil:



so it's fine grain.   
 52 → passing more than 50% or over 50%.   
 silt (M)   
 clay (C)

Then LL = 65  
PL = 36

∴ PI = 29

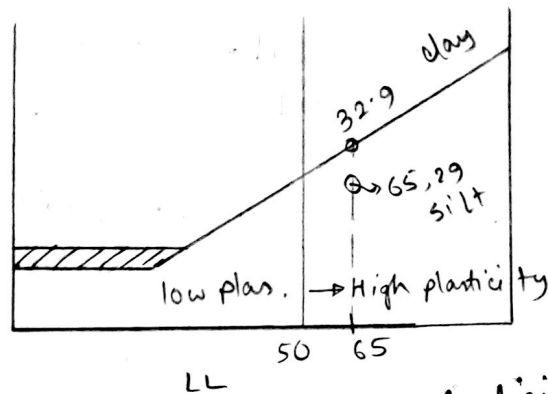
silt or clay or curve plasticity curve 2 error

Then plot (65, 29)

$$\text{Again } PI = 0.73(LL - 20) = 0.73(65 - 20) = 32.9$$

so 29 falls below 32.9, so 1st letter is silt M

Then we draw another line



LL greater than 50 or high plasticity.

Here  $LL = 65 > 50$   $\therefore$  high plasticity.  $\therefore$  MH

or classification

MH	CH
ML	CL

\* Hatched area or point or dual classification  
CL-ML : silty clay or low plasticity

organic soil or determine liquid limit in 2 ways

1) dry it in air

2) dry it in oven

oven dry ~~করলে~~ organic soil ~~র~~ liquid limit will be less.

Inorganic ~~র~~ air & oven dry  $\Rightarrow$  same.

$\frac{LL_{\text{oven dry}}}{LL_{\text{air dry}}} < 75\%$ , so we say organic soil.

~~এ~~ ~~করে~~ organic soil is always fine grain soil.

Air dry  $LL > 50$  ~~র~~ OH - organic soil of high plasticity

Air dry  $LL < 50$  " OL - " " " low "

$\square$  organic content  $> 75$  ~~র~~ peat soil. ~~এখন~~ we go for ~~test~~ on ignition test.

soil ~~ক~~ air dry, then oven  $\approx 400-500^\circ\text{C}$   $\Rightarrow$  heat ~~করলে~~ organic matter burned out, ash residue ~~শাকবে~~.

Here Ash content  $> 75\%$  ~~র~~ then we call peat soil.

$\square$  Problem:

sample ~~কিলাই~~, Grain size Analysis ~~করলে~~,  
Then grain size Analysis ~~করবে~~:

% passing # 4 = 85

% " # 40 = 60  $\Rightarrow$  0.425 mm

% " # 100 = 30  $\Rightarrow$  0.149 mm

% " # 200 = 10  $\Rightarrow$  0.075 mm

LL = 48 , PL = 25 , SL = 10 , LL<sub>air dry</sub> = 65

overdry

classify the soil as per USCS.

$\Rightarrow$  1st step % passing # 200, Here retained 90%, so coarse grain. coarse grain  $\Rightarrow$  organic check करके रहेगा.

Then retained in # 4 = 15 in 100 gm

But coarser soil  $\Rightarrow$  90 gm

$\therefore$  % of coarser fraction retained in # 4 =  $\frac{15 \times 100}{90}$   
 $= 16.65$  gm

this is less than 50% of 90 gm. So this is **S.**

# 200  $\Rightarrow$  passing 10,  $\therefore$  fines 5-12%, so dual classification

Now classifications can be

- SW-SM
- SW-SC
- SP-SM
- SP-SC

अतः, so go to grain size & plasticity

$$\therefore C_u = \frac{D_{60}}{D_{10}} = \frac{0.425}{0.075} = 5.67$$

$$C_z = \frac{0.149^2}{0.425 \times 0.075} = 0.69$$

so  $C_u \geq 6$  or  $1 < C_z < 3$  or  $3$  or, so not well graded.

so we know SP

$$PI = 0.73(65 - 20) = 32.85 = 32.9 \text{ (on A line)}$$

$$\text{Determine } PI = LL - PL = 65 - 25 = 40$$

40 lies above A line.  $\therefore$  the sample is *clay*

$\therefore$  The soil is SP-SC

### ASSTHO Classification System:

Suppose data given of previous math and

$\gamma_p$  passing # 10 = 70

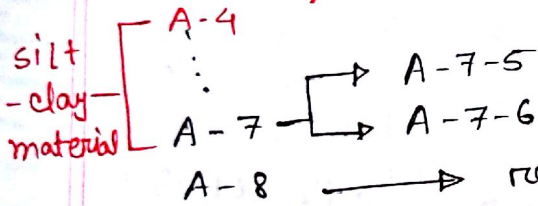
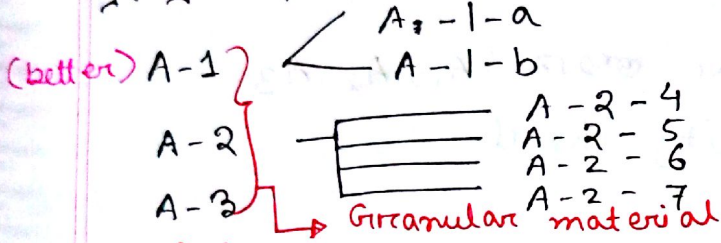
ASSTHO used for pavement design,

- 1) Granular material
- 2) silt-clay material

ASSTHO 23 symbol सिस्टम classified.

A-1 to A-8, ২য় ৬-র classification.

প্রথম প্রকারের প্রথম প্রকারের কাঙ্ক্ষিত অন্য ডাল



A-1 থেকে A-7 for inorganic soil.

⊗ Chart এ A-1 এর ৭য় A-3.

A এর number যত বড় তত ভাল soil.

⊗ For classification basis

% passing # 10

# 40

# 200

LL

PL

} ২য় 5-র data judge

⊗ Given data of previous math & chart compare

# Non plastic সিল্ট LL & PL can't be determined.

SO the soil is A-2-7, (যেকোন ১-র criteria meet না করলে discard)

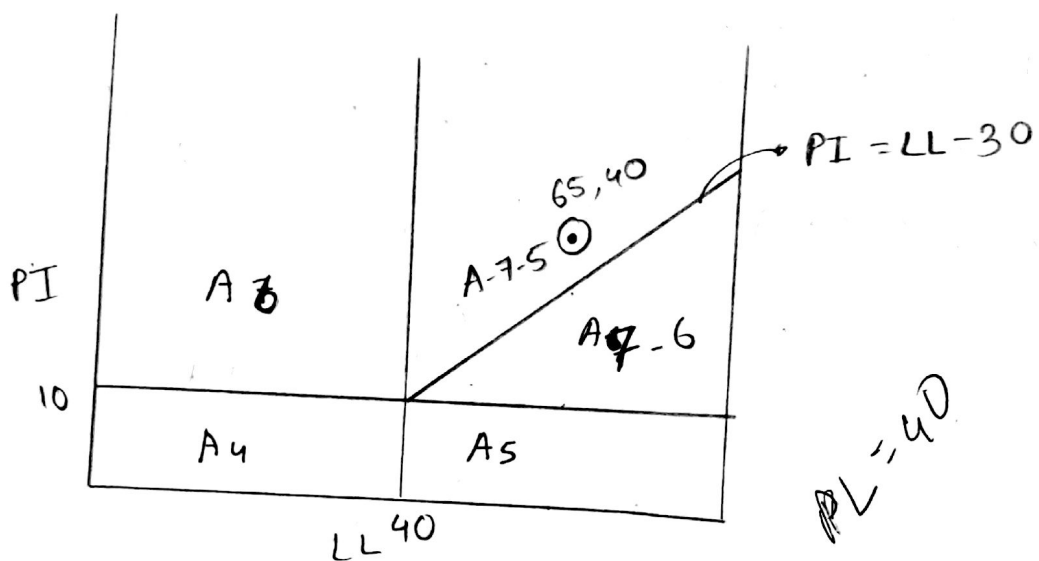
For A-7-5

A-7-6

আমার solution note করে,

35 or less passing through # 200 is called  
(granular material)

ସମ୍ବନ୍ଧରେ ଦେଖନ୍ତୁ granular ଭେଦ A<sub>1</sub>, A<sub>2</sub>, A<sub>3</sub>  
silt clay ରେ plasticity chart



if silt & clay  $LL = 65$   $PI = 40$

(65, 40) put karay, so it is above 40 is above 35,

$$PI = 65 - 30 = 35$$

so A-7-5

Project (मकसद पूरक रक (कम) classification.  
ASTHO is done for roads & airports.

Group Index:

$$GI = (F - 35) [0.2 + 0.005(W_L - 40)] + 0.01(F - 15)(I_P - 10)$$

It should be round figure. It can't be negative.  
For inorganic it's 0-20 usually. But best value 3 रक

कम,

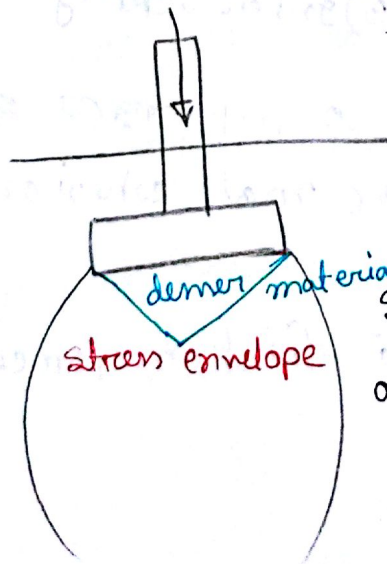
GI = 0 = Best soil GI ↑ worse soil

GI = 20 = worse "

A 2-6 A-2-7 कककककक GI partial use रक,  $0.01(F-15)$   
(IP-10)


GI is stated in parenthesis. Like A-3(10)  
↓  
GI

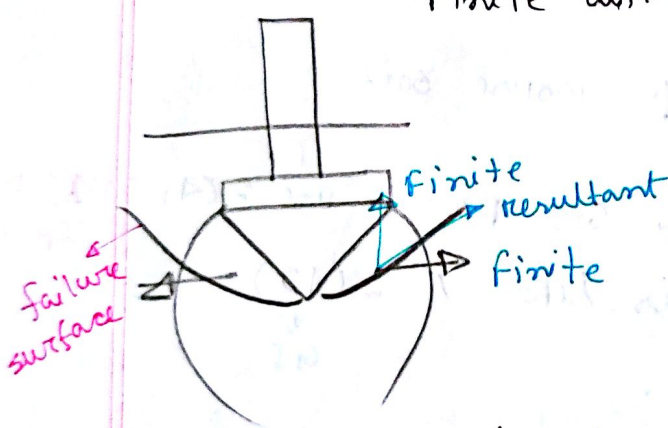
Chapter-7



Footing is loaded, soil & granular material शककन soil in contact with footing will be stressed. रक कककककक Shift कककक, कककककक propagation of stress over area रक,

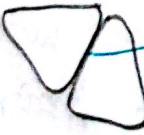
When load certain area  $\rightarrow$  propagation  $\rightarrow$  that area stressed to infinity. But envelop of stress  $\rightarrow$  stress significant.  $\rightarrow$  area different stress deliver  $\rightarrow$  that soil particles <sup>roll</sup> load over each other, so fail  $\rightarrow$  rolling

 When wedge  $\rightarrow$  soil  $\rightarrow$  pressure  $\rightarrow$  finite, so  $\rightarrow$   $\rightarrow$   $\rightarrow$  move  $\rightarrow$  finite distance  $\rightarrow$  move  $\rightarrow$



Failure surface  $\rightarrow$  plane  $\rightarrow$  actually curve.  $\rightarrow$  fail  $\rightarrow$  strength.

- Strength criteria 3 :
- i) cohesion
  - ii) friction
  - iii) interlocking

  $\rightarrow$  surface  $\rightarrow$  roll  $\rightarrow$  bonding bet<sup>n</sup> similar mat cohesion overcome  $\rightarrow$

smooth  $\rightarrow$  friction force develop  $\rightarrow$

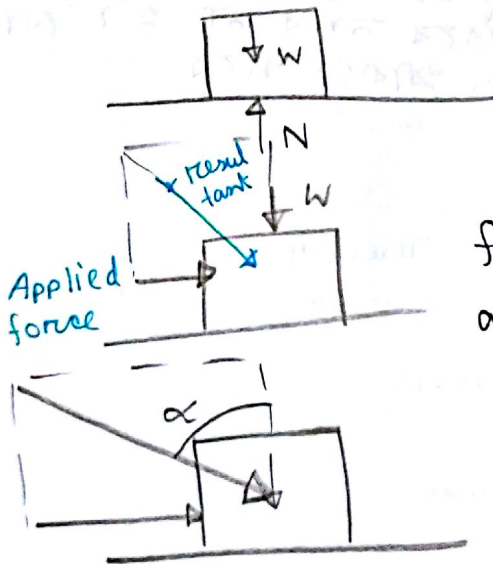
$$F = \mu N = N \tan \phi$$

$\downarrow$                                        $\leftarrow$   
 co-ef. of friction                      Friction Angle

roll કરતા રત્ન distance travelled, no energy  
 નાશ, પર interlocking.  
 length of contact સમી રત્ન સમી interlocking.

Friction:

N should be = W



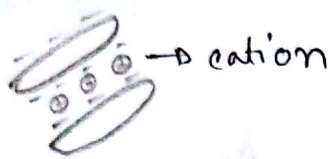
with the increase of horizontal  
 force so verticle જાં આજે  
 angle  $\alpha$  increase કરાવે.

verticle force જાં આજે resultant  
 જે angle કરાવે that is called  
 angle of obliquity.

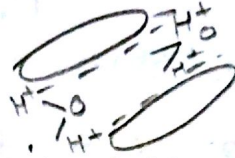
Impending motion રત્ન angle of friction.

In case of angle of obliquity movement રત્ન ના,

Cohesion: 2 -ve charge. Fine grain soil રત્ન -ve charge  
 4. Nature 2 H<sub>2</sub>O. Flaky particle -ve charge carry  
 કરાવે.



if  $H_2O$  is there

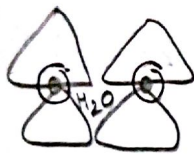


in fine grain soil cohesion is prominent.

In coarse " " " " not "

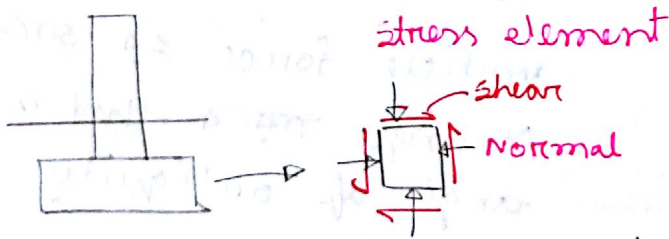
OO tremendous stress, ভারসর

$H_2O$  এ উঠা stress নাই, pore pressure  
 Depending on  $H_2O$  content, soil stress  
 নিচে পড়বে নাকি না এটা বোঝা যায়,  
 etc



clayey soil রকম cohesion থাকতে পারে

### Mohr - Coulomb failure Theory :



if we know normal & shear stresses then we can draw a circle.

According to Mohr কোন particular plane এ

fail করলে failure angle ডানতনে এ plane এ

N & shear stress must lie on the circumference of the circle.

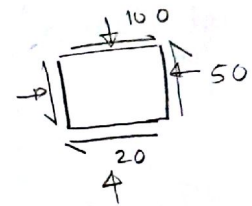
### ☞ Mohr Circle Diagram:

Soil is most of the load compressive. This is (+ve).

counter clockwise = (+ve)

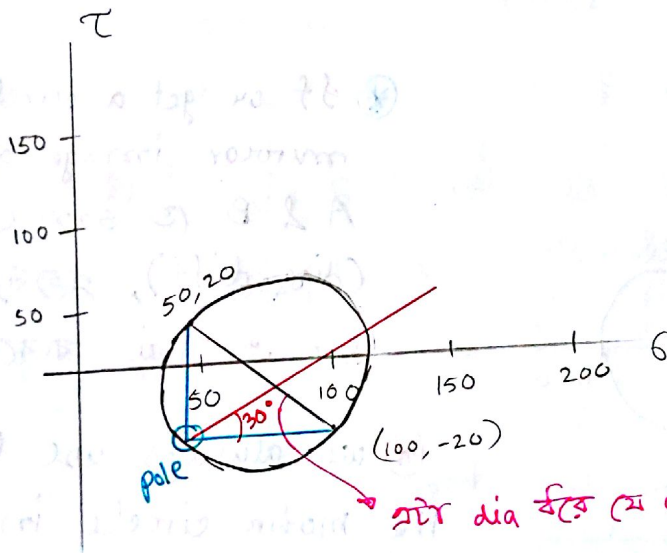
Shear

$\sigma, \tau$  plane. in same scale



# consider two orthogonal plane

in horizontal plane  $(100, -20)$   
 counter clockwise  
 In vertical  $(50, +20)$



pole of the Mohr Circle / centre of controlling point

100, -20 acts on a horizontal plane,  $\sigma$  parallel  $\Delta$  line

50, 20 " " a vertical plane,  $\tau$  "  $\Delta$  line.

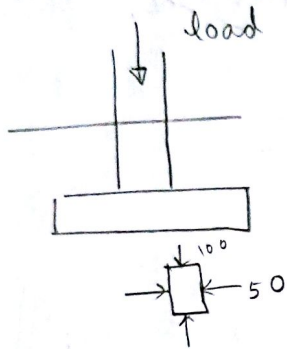
Intersection  $\Delta$  pole of Mohr circle

30°  $\Delta$  horizontal  $\Delta$   $\Delta$  plane

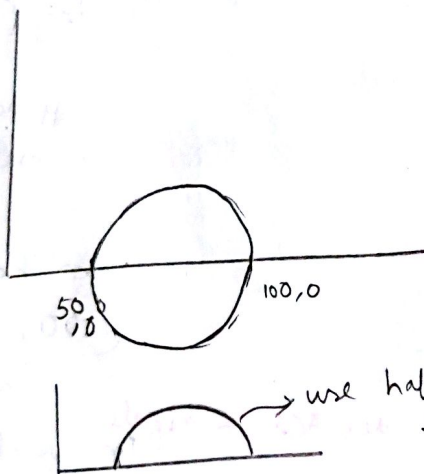
4.11.15

Wednesday

lec - 11



soil granular and lateral force exists on stress element  
 if no shear then we call it principal stress



\* If we get a circle which is mirror image of x axis A & B (same shear (dir. diff), opposite shear & dir. diff. fail - karabe and diff.

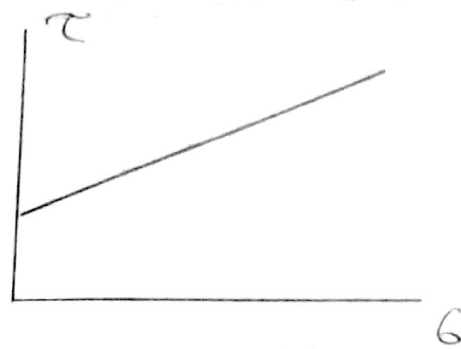
we always use half of the Mohr circle in soil mecha. Cause opposite shear & exists.

# Mohr Coulumb Failure theory:

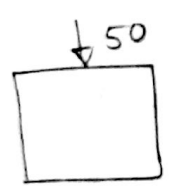
$$\tau = c + \sigma \tan \phi$$

$\downarrow$  intersection of y  
 $\downarrow$  slope angle  
 $\downarrow$  shear strength parameter

Mohr's circle failure stresses on the circumference, Coulomb's failure stress on a particular plane is shown by a st. line.



So a line satisfy Mohr's circle the st. line must be a tangent on the Mohr's circle.



$$\tau_f = c + \sigma_f \tan \phi$$

So  $\sigma_f$ , so  $\tau_f$  to determine  $\tau_f$  we need to know  $c$  &  $\phi$   
 $\downarrow$   $\downarrow$   
 apparent cohesion      apparent angle of internal friction.

4] Dete. of shear strength parameter:

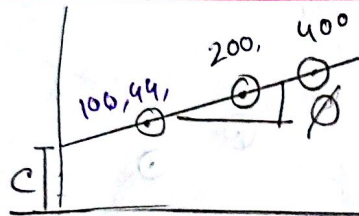
Various method, we use 4 in this course.

x) Direct shear:

Suppose normal 100, shear 44. on particular plane a failure

Again  $N = 200, \tau = 50$

$N = 300, \tau = 55$

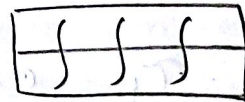


Adv → simple & quick

Risdy → particular pre determined plane → failure, weakest plane →  $\sigma_1$ .

In case of plastic soil deformation of fiber

But shear  $\sigma_1$   $\sigma_2$  fibers



$\sigma_1, \sigma_2$  shear failure

वर्तमान  $\sigma_1$   $\sigma_2$  like 

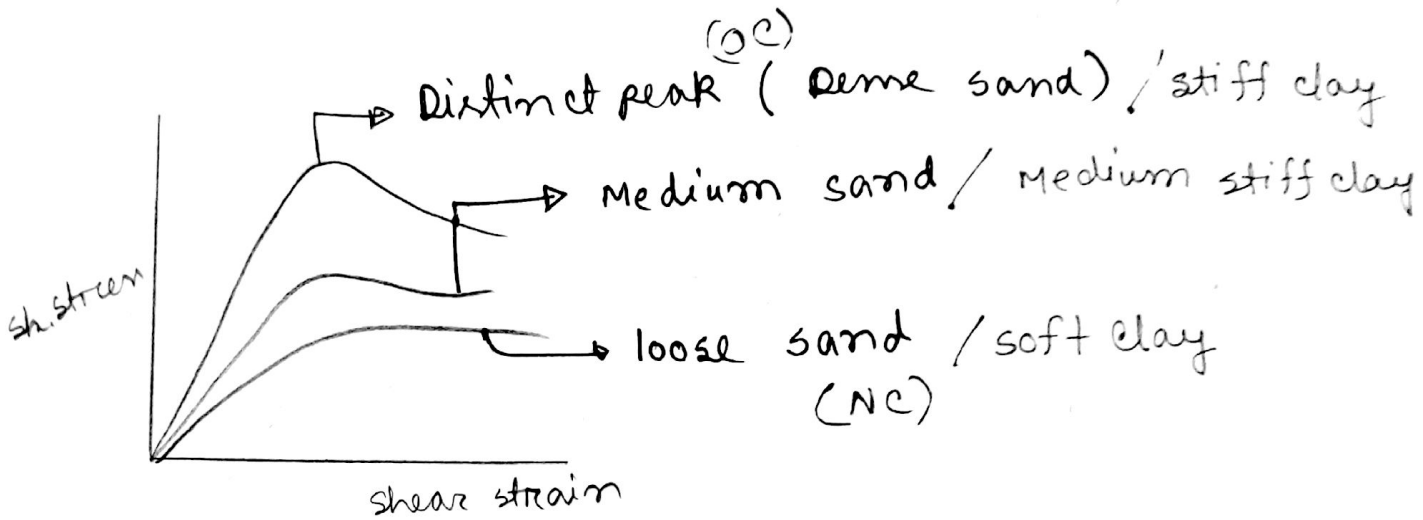
→ false imp  
ression

गर्ज,

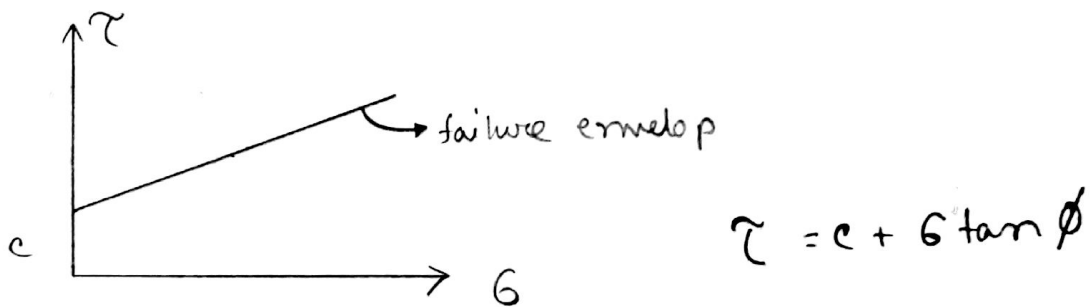
lec-12

Continuation of last lecture:

shear gradually apply करें.

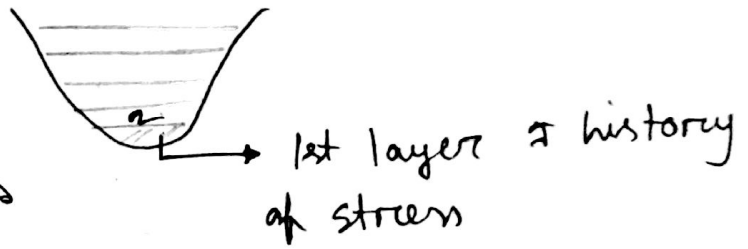


for claye soil we use diff tetron soil का formation का shear strength dependent



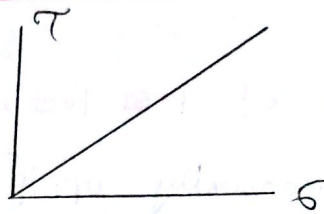
Alluvial soil river bed का उदाहरण दें.

1st yr का small layer  
 1st a very thin layer,  
 normal load का, it was  
 like slurry



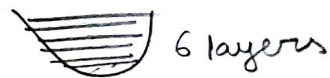
का (2) deposit का density का and normal stress का, so shear का.

যে soil টা, কোন point of time এর v. load তার সীমিত max load



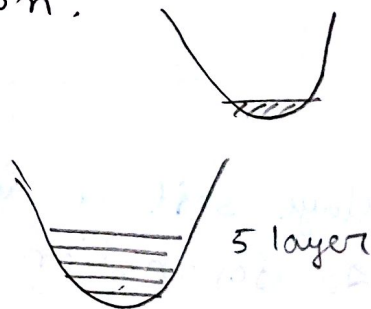
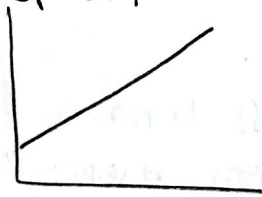
২টা Normally consolidated soil.

6 years ১ ভঙ্গা।



Geological কারণে erosion.

then single layer, এর উপর certain shear শক্তি for previous denudation. then আর deposit ২টা



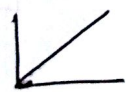
usually over consolidated soil stiffer, N.C. S softer

↓  
কিন্তু সে stress তার চেয়ে বেশি stress নিতে পারবে. cause এখন উপর ৭টা layer. আর ৫টা ছিল.

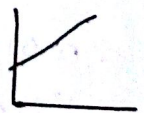
Then ~~৫টা~~ মধ্যস্থত ~~৫টা~~ উপর add ২টা layer and ৫টা layer then - N.C. এর পরে এর additional load হলে N.C.

Normal applied loads যদি N.C. এর range এ

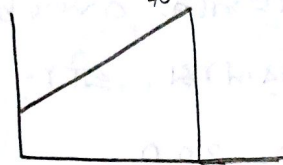
শক্তি then



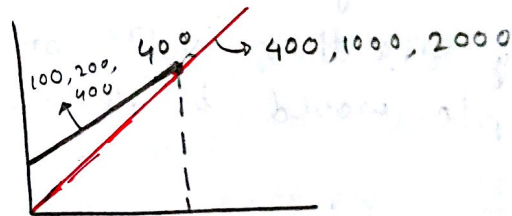
if N. load over c এর range এ শক্তি



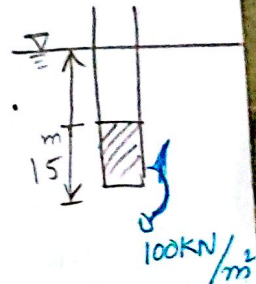
Maximum post pressure / over consolidation pressure  
 100, 200, 400 N load ତାର ଉପରେ max<sup>m</sup> load ଠାରୁ  
 ଥିବା line



400 max<sup>m</sup> ଥିଲେ  
 if 400, 1000, 2000 ଫିଟିସ୍ ବାଡ଼ି ଯାଏ then line passes  
 through origin:



Foundation ଥିବା ଠାରେ soil ତରଳ N.C.  
 ଥିବାର ଠାରେ lab ଥିବା ଠାରେ O.C. cause no v. load.  
 so all the soil samples in lab are O.C.



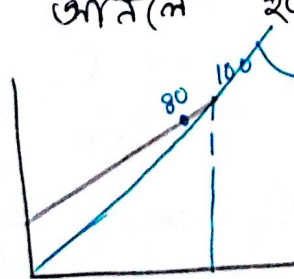
Soil ଥିବା Bulk unit wt  $16 - 20 \text{ kN/m}^3$

Effective unit wt  $16 - 9.81 = 6 \text{ kN/m}^3$

↓  
 H<sub>2</sub>O ଥିବା unit wt

so 15m ଥିବା around  $100 \text{ kN/m}^2$  Effective verticle pressure

then lab ଥିବା ଠାରେ 20, 40, 80 load ଠାରେ then

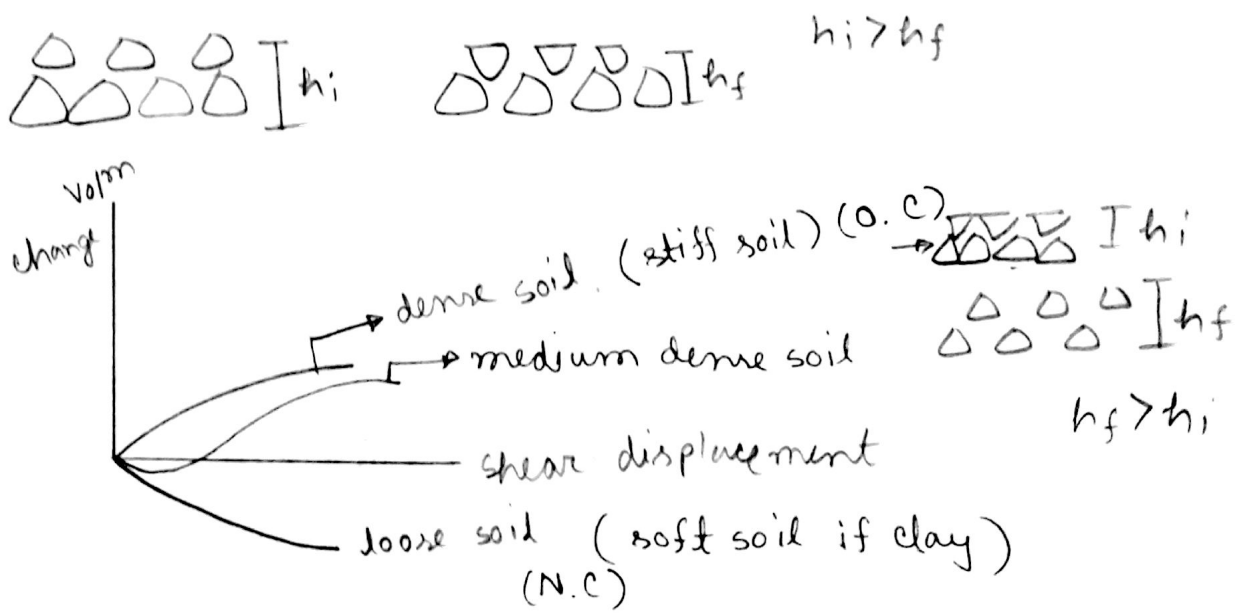


100, 400, 800 if test 100, 400, 800  
 load ଠାରେ ଥିବା then  
 origin ଠାରେ pass

cause H<sub>2</sub>O table खोनाका करे,

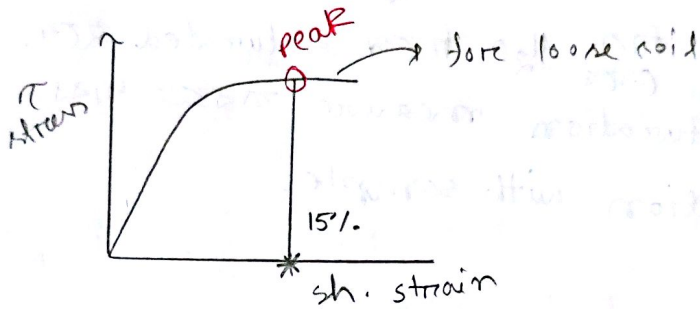
(\*) Exact pressure ज्ञान अज्ञान नर, काहीकाहि (ब्रह्म) rounding करे, testing का अज्ञान वरुका overburden pressure 20, 50, 100 वरुका, जोरा 1/2 & 2/3 use करे, 50, 50, 100, 200

# soil initially loose 20% & shear displacement apply करे then vol<sup>m</sup> or the height of the soil sample would be reduced.



Q. Typical vol<sup>m</sup> change shear displacement dia fore N.C, o.c, loose, dense - ... ?

If a soil is loose / soft & distinct peak exists, so 15% strain is reading of stress at peak.



soil is  $H_2O$  saturated softer mat & strength is not known if it is fully saturated, so degree of saturation is not known.

To overcome these disadvantages of test.

Field is v. load applied, no lateral load is applied (may be 2 side fixed), But a direct shear is lateral load is value is not known.

For all these do direct shear test.

Direct Shear Test: 2 or specimen used.

cylindrical soil sample. Dia = 38 mm L = 75 mm  
Field is collect by sampler.

We want to saturate it, but shape is not known.

so sample लेखि कण्डा पर filter paper दिव trap करे  
rubber membrane मिः fully encased, so H<sub>2</sub>O गारब ना,  
But देखर & निरु H<sub>2</sub>O मिल saturated रहे, एकर  
degree of saturation measure करल जाय,  
3tr connection with sample.

11.11.15  
Wednesday

Lec-13

Direct Shear Test (continued):

→ failure occurs by vertical & by horizontal load.

↓ Triaxial  
~~direct shear~~  
compression

↓  
direct shear  
Extension

Triaxial  
    / compression  
    \ Extension (not very common)



A fails in vertical load, so compression

B fails horizontally, though the vertical load is constant.

cell pressure is equal to (cell pressure) soil sample pressure. loading ram load.

Here we can make the soil sample saturated. Bottom & top water connection.

connect water, water back pressure.

water back pressure, saturated water sample, crack formation, no balance by back pressure.

Saturated triaxial test.

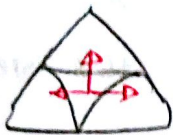
construction stage  
loading "

} both are 2 excess pore  $H_2O$  pressure stages.



At  $H_2O$  pressure stage static pore " "

इस क्षेत्र extra load दिले excess pore  $H_2O$  pressure stage concern.



इसलिए extra pore  $H_2O$  p रोकता है, so क्षेत्र छोड़ता है.

Depending on two stages

- 1) consolidation (in construction stage) - Consolidated
- 2) Drainage (in loading ") - Drained

$H_2O$  का एकलकत pressure develop करने leakage शुरू करते हैं, interparticular gap दिले कति कम हो रहे हैं so expansion of  $H_2O$  & E.P  $H_2O$  p. decrease करते हैं. Drainage उ करे as consolidation, just to diff the stages के नाम.

\*) Triaxial test 3 divisions:

- 1) Unconsolidated Undrained — UU Test — Quick Test — Q Test
- 2) Consolidated Undrained — CU Test — R Test
- 3) Consolidated Drained — CD Test — slow Test — S Test

We don't want the  $P_{H_2O}$  pressure to decrease.  
 So fast load apply করতে হবে, তাহলে UU present  
 so quick test

CD → Slow load apply করে মোট  $H_2O$  decipit করে

Soil sample saturation এর পর construction এর load

দেখ cell pressure দিচ্ছে,

Extra load এর পরে দিচ্ছে দিচ্ছে।

If we want Q Test then top & bottom connection  
 close করে, so  $H_2O$  বের হতে পারবে না।

R-Test : construction এর পর slow ~~এর~~ ২ম consolidated  
 loading fast দিলে undrained.

Undrained হলে connection of  $H_2O$  tube closed.

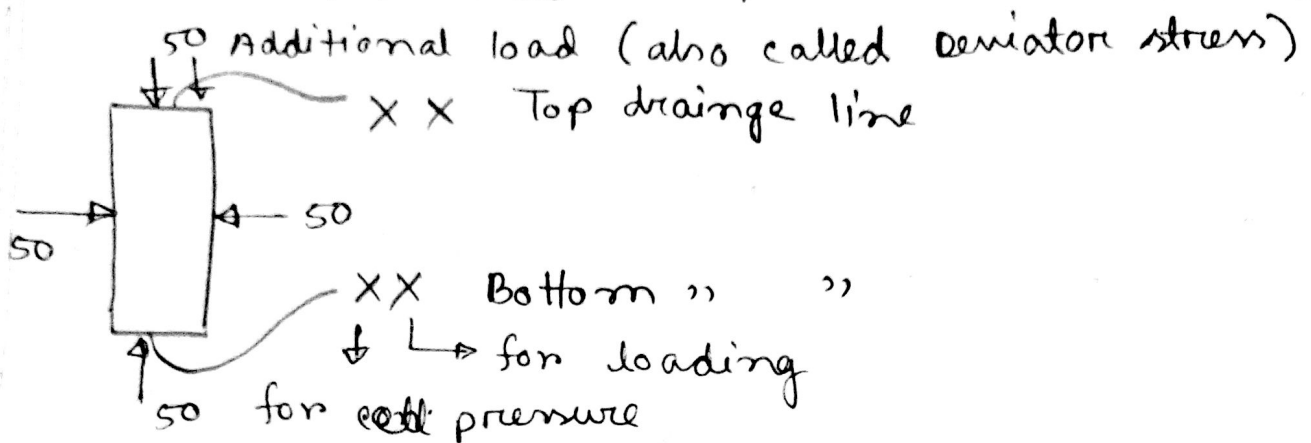
Drained " " " " " open.

⑦ cell pressure apply করে, construction stage stimulate  
 করে and তাহলে  $H_2O$  tube খোলা, তাহলে consolidated  
 হবে।

⑧ water expell হবে যদি সুস্থিত drainage tube এ  
 পিকুরেট লাগায়, তাহলে  $H_2O$  এর পরিমাণ determine  
 করতে পারি, usually takes 2 days for total drainage  
 according to cell pressure.

# Unconsolidated Undrained Test :

All the test need 3 specimen.



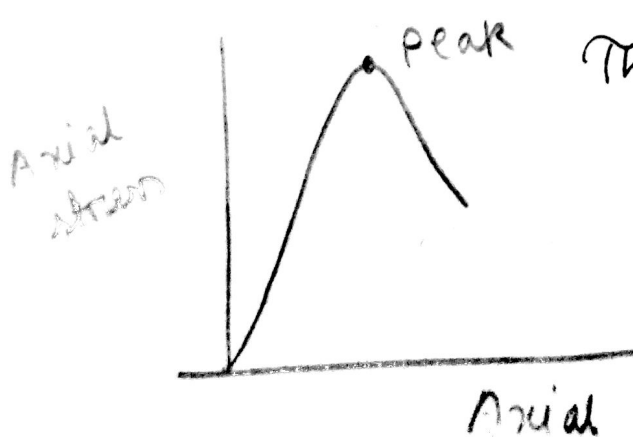
ଉତ୍ତର saturated କରା, ମିଳି 2ଟା, 90-95% saturated ହଲେ 2ଟା, we can check if it's saturated.

Cell pressure applied 50, all around pressure same

laterally pressure ମିଳି 3 vertically 3 same pressure ଉପରେ

Saturated କରା, 90 drainage 2ଟା ନା ମିଳି pressure ମିଳି no  $V_{ol}^m$  change.

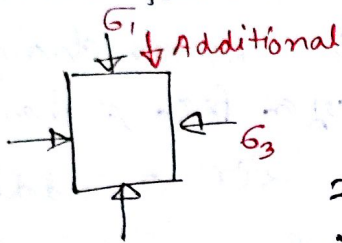
Progressively additional load ଦିଆ.



This graph is for only Additional stress

↳ measured with strain gage

At the failure 2<sup>nd</sup> load working

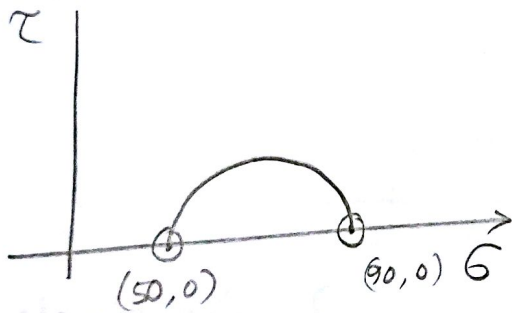
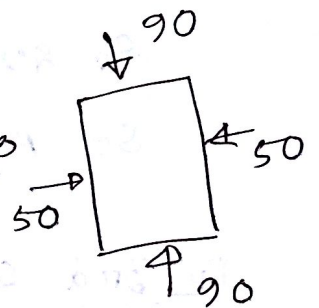


2<sup>nd</sup> load v. 1<sup>st</sup> load cause additional stress  
 v. 1<sup>st</sup> load so  $\sigma_1$   
 H 1<sup>st</sup>  $\sigma_3$

$$\sigma_1 = \sigma_3 + \Delta \sigma$$

cell pressure
deviatoric stress

Suppose Add. load needed 40, 1<sup>st</sup> load 50. so



So the diameter of the Mohr circle is 40.

$$\sigma_1 = 90$$

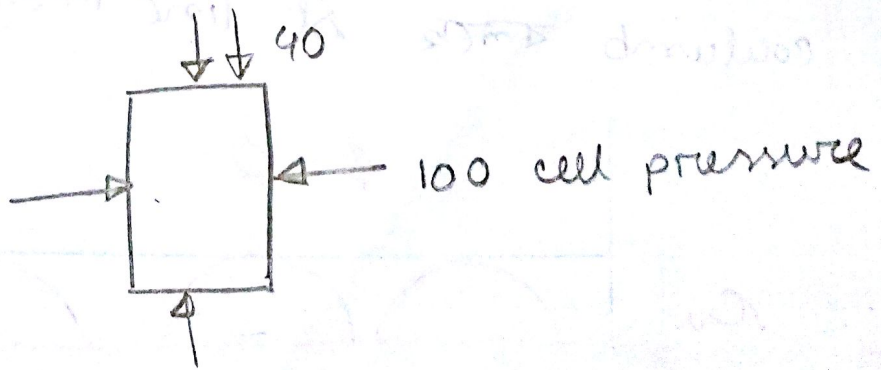
$$\therefore \sigma_1 = \sigma_3 + \Delta \sigma$$

$$\Rightarrow 90 = 50 + 40$$

So Diameter of the Mohr circle = deviatoric stress

2<sup>nd</sup> specimen:

Top & bottom drainage line closed

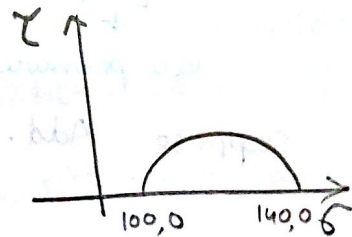


sample ① & ② a vol'm same as drainage line closed and saturated. So no ~~any~~ change in density. [drainage line खुला होने पर  $\rho$  change होता है] So same density का मतलब है  $\sigma$  का additional load a fail कराता है  $\sigma$  same.

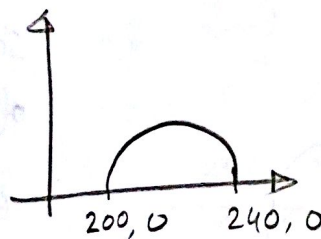
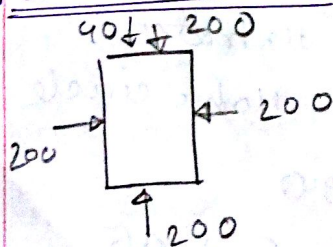
Additional load is a function of density.

So अगला add load 40.

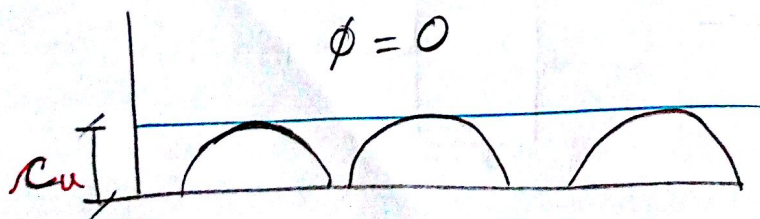
So Again, Mohr circles dia 40.



3rd specimen:



Mohr काटे failure stress से 3rd circle का circumference का मतलब, Coulumb काटे  $\sigma$  line को represented



As we get this  $c$  काटे for undrained condition

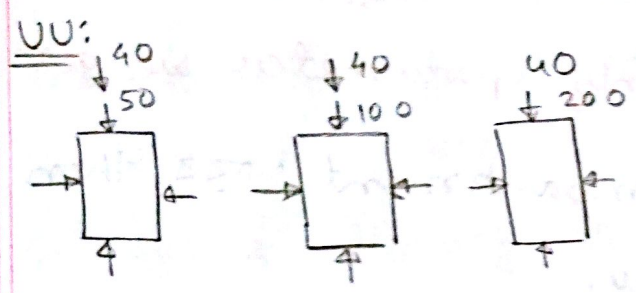
in both cases we call it  $c_u$ .

So in UU Test the only parameter we get is  $c_u$ .

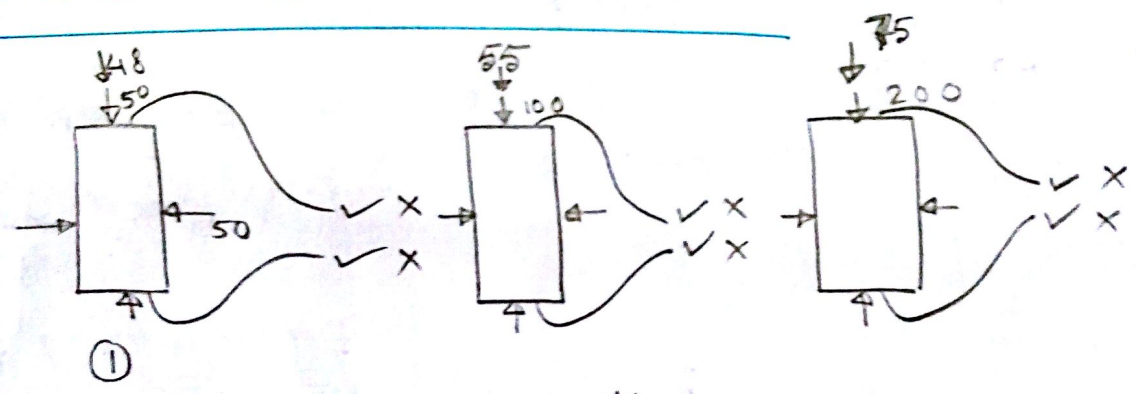
यदि यदि 1 week a embankment बड़ा then the parameter will be  $c_u$ .

कमरा कमरा time फ्रि बरिने लरज parameter.

Lec-14



☐ Consolidated Undrained Test (CU) : 5-15 min time  $\approx$  5



consolidated undrained - - fail.

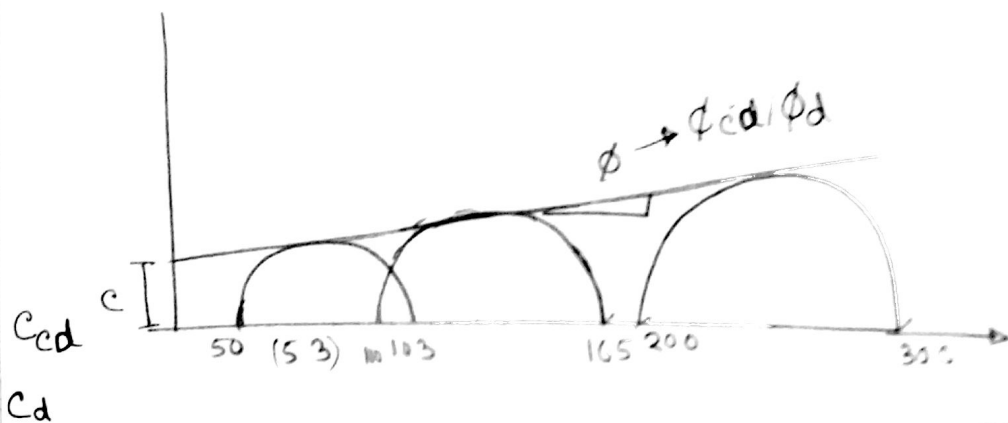
cell pressure apply  $\approx$  time 2 top & bottom  $H_2O$  line open.

water  $\approx$   $\approx$ , so vol<sup>m</sup> change  $\approx$ .  
Then additional load, then  $H_2O$  line closed.

\* strength is a function of density  
water expelled  $\approx$  vol<sup>m</sup>  $\approx$   $\approx$ , so  $\rho \uparrow$ , so  
the load needed will be higher.

\* 100 दिने प्रस  $\approx$   $\rho \uparrow$   $\approx$   $\approx$  than 50,  
so load  $\approx$   $\approx$ .





Slope will be higher than  $c_u$ .

अथवा pore  $H_2O$  pressure शक्यता ना, 3A stress effective. Cause  $T. Pressure = P. H_2O pressure + Eff. stress$   
 So we call it effective cohesion  $c'$   
 " angle of friction  $\phi'$

Drained अथवा pore  $H_2O$  pressure develop करेता ना,  
 so fail करेता very slow load अ.  
 एकरे fail करेता min 5 days. method.  
 so एकरे अत्यंत time consuming. So alternate, करेता  
 मास

(\*) con. Undrained अथवा अथवा  $c'$  &  $\phi'$  मास  
 मास, Here 3 days अथवा save करेता मास.

Bottom अ एकरे connection अथवा, एकरे अथवा एकरे  
 अथवा by pressure Transducer.

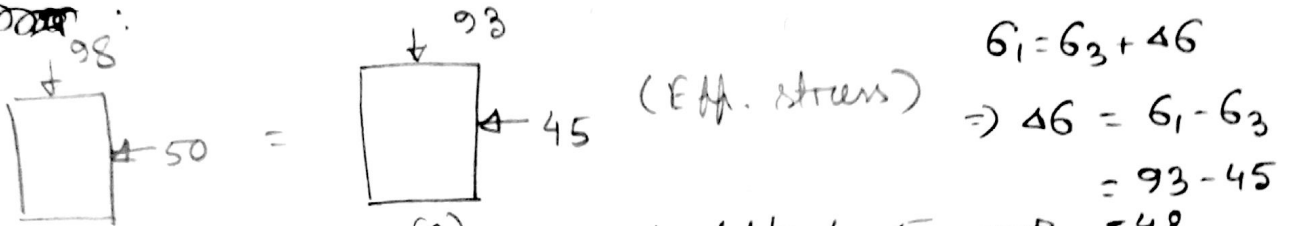
$c_u$  अ deviator stress अथवा अथवा pore pressure  
 अथवा, एकरे pore pressure can be measured by  
 pressure transducer.

poore pressure all around, so horizontally 3 reduced

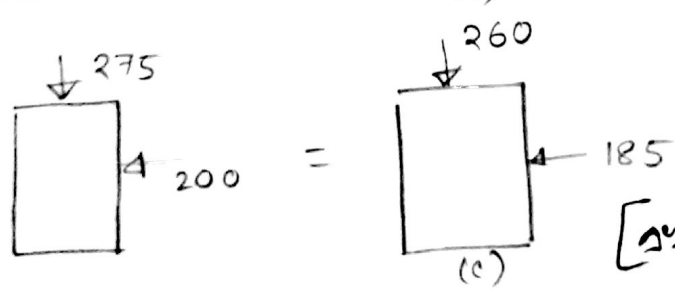
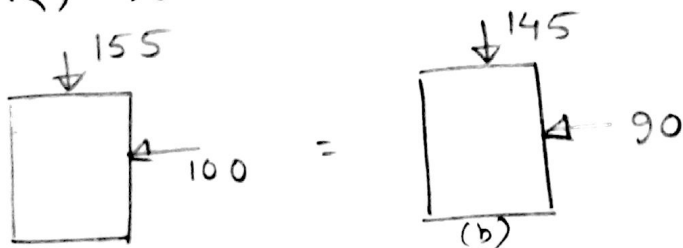
एतः,

Suppose CU ए 1st ए P.P = 5

उदाहरण :

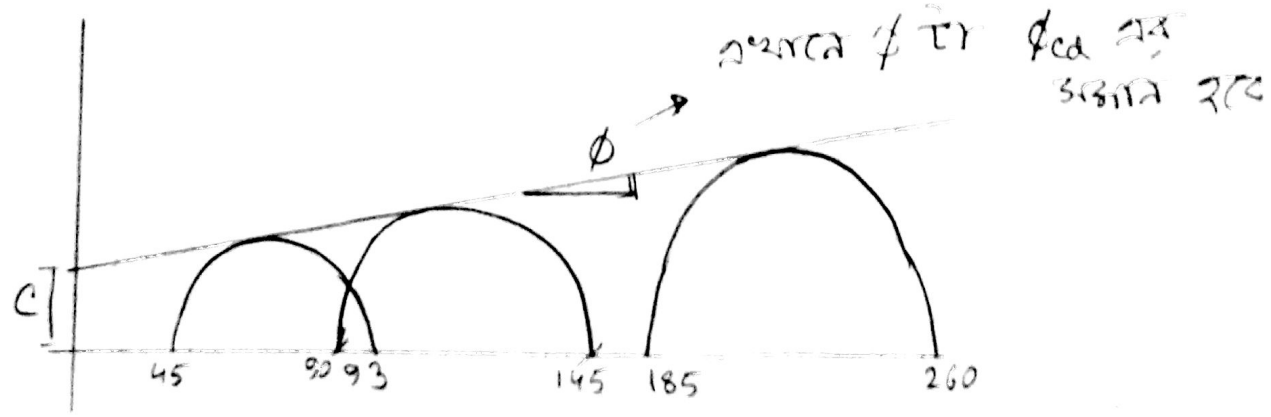


अक्षर dia same but it will go to left by 5 →  
 volm कम एतः pore size (हरे, अंतरा compression करे, so 2nd ए P.P. Let it be 10



[Eff stress = T.S - P.P]

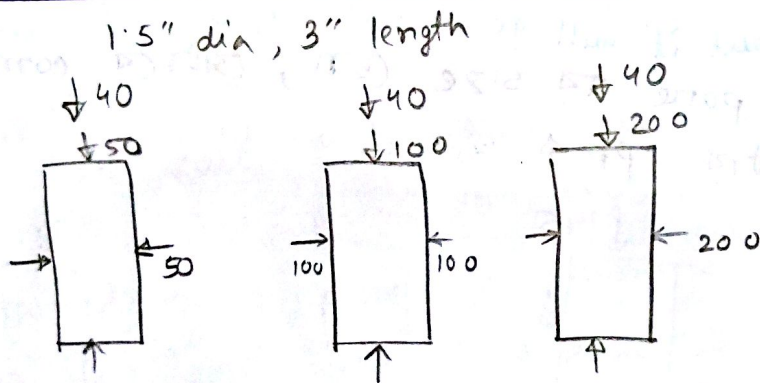
[अंतरा P.P = 15 एतः एतः]



C<sub>u</sub> or  $\sigma$  (সকোম্পন) এর মান নির্ভর করে  $\sigma_{cr}$  নির্ভর করে depending on the 1st circle.  
 অবস্থানের dia আরও  $\sigma_{cr}$  just shifts to left by 5, 10, 15

⊗ CU test with pore pressure measurement.  
 written as  $\bar{C}_u$  or CU Bar

⊞ Unconfined Compression Test:



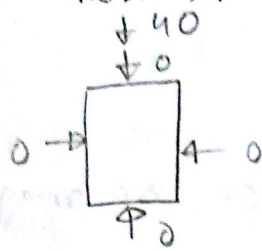
UU এর সময় always 40 লাগবে; 0 দিলে 40 এর আকারে, 50 প্রথম ব্যাকসেলার দরকার ছিল না, but 3 বা 100 দিলে saturation সাফল্যে.

- i) If we are sure that the soil is saturated then প্রমাণ করার দরকার নাই.
- ii) আবার H<sub>2</sub>O line বন্ধ রেখে বললে water can't expell out → প্রমাণ " " না করে যদি অনেক fast fail করবে তাহলে H<sub>2</sub>O can't expell out.

so unconfined com. এর ২টা condition/assumption

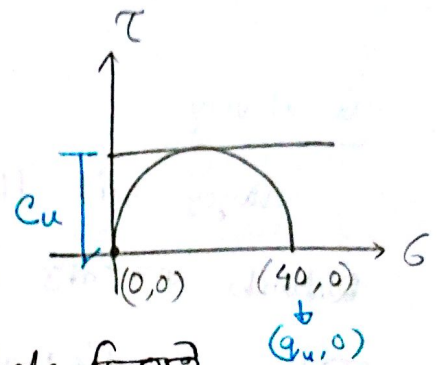
- 1) soil must be cohesive
- 2) soil " " saturated

अरे test ए cell pressure zero



(40, 0) in H. plane

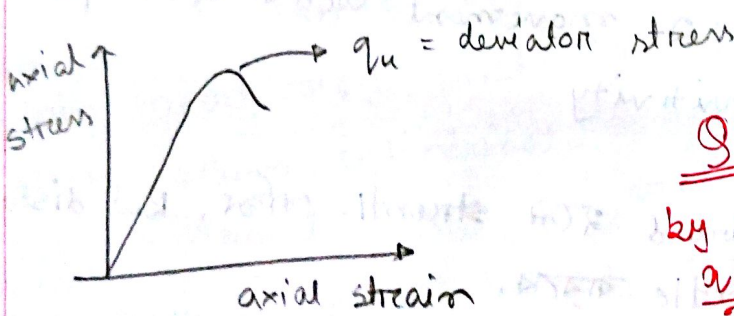
(0, 0) in v. plane



अरे cell pressure 2 (अरे dia 40 and line horizontal 2रे, so अरे circle दिखे

कि,

$$\therefore C_u = \frac{q_u}{2}$$



Q. Shear strain parameter by unconfined com. test is  $\frac{q_u}{2}$  ?

\* यद्वे वनि same value नर but slight diff आउरवे, suppose  $q_{u1}, q_{u2}, q_{u3}$ , avg निरु माएव नर, judgement apply करए 2रे से (बान एवः बानदे निरु. ग्  $q_{u1}, q_{u2}, q_{u3}$  काहाकाहि रस then we can take an average.

Sensitivity:

clayey soil flaky, electric charge থাকে, so magnetic, Disturb করলেই same orientation 2 থাকে।  
কিন্তু soil disturbed হলে strength বি পরিষ্কৃত change হবে।

if  $S < 2$  then ok,  $> 2$  হলে diff consideration.  
excavation এর time 2 movement অনেক হলে problem & then consider sensitivity

Quick clay  $\rightarrow$  undisturbed হলে strength বেশি, But disturb হলেই settle করবে।

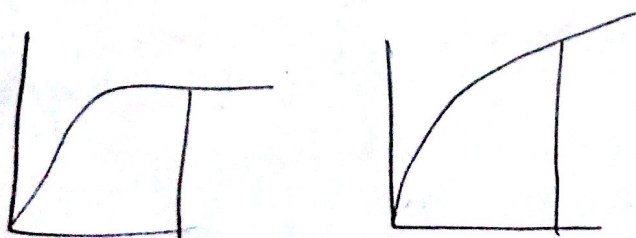
clayey soil magnetic ক্ষমতা time allow করলে strength gain করে।

অত্যা no time delay, Remold করবে আরও আরও test.

Q. What is thixotropy?

Regaining strength for reorientation of particle.

\* সঠিক peak না করে / increases then 15% strain এর stress



□ Condition of unconfined consolidation test:

soil must be clay

soil must be saturated

clay 20 20 10 10 stand 10 10 10 10

visually soil sample a crack then go for UU test.

□ Vain Shear Test:

it can be done both for field and lab.

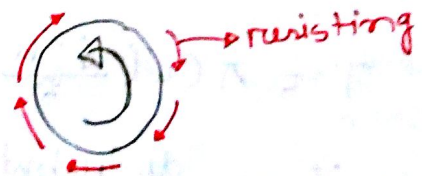
vain insert rotate fails in 3 planes.

Top, bottom, cylindrical.

let a resist torque, so applied torque measure.

we know applied torque = resisting torque

Section of cylindrical surface



⇒ clay soil, undrained (on very quick loading) ~~from~~ for undrained con.  $\phi = 0$

then  $\tau = c + \sigma \tan \phi$

$\therefore \tau = c_u$   
↓  
force per area

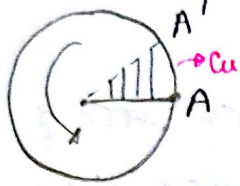
if dia d, height H

$\therefore \text{Area} = \frac{\pi DH \cdot c_u}{\text{force on surface}}$

$\therefore \text{Moment} = \pi DH \cdot \frac{D}{2} \cdot c_u$  (resisting moment of the surface)

\* Resistance at surface and top, bottom edge  $\rightarrow$

Resisting moment at edge:



centre  $O$  displacement  $0$

At particular moment  $\Delta$  fail there will be max<sup>m</sup> displacement. So point  $A$  will go to  $A'$

So  $AA'$  is the failure.

As the triangular distribution is not known, we never know the dis. of strength on the surface.

\* Rod is area  $\pi r^2$

\* distribution is depends

for  $\Delta a = \frac{1}{2}$

for parabola =

$$T = \pi C_u \left( \frac{d^2 h}{2} + \frac{a d^3}{4} \right)$$

uniform distribution  $\frac{2}{3}$  (for  $a = \frac{2}{3}$ )

$$\therefore T = \pi C_u \left( \frac{d^2 h}{2} + \frac{2}{3} \frac{d^3}{4} \right)$$

$$= \pi C_u \left( \frac{d^2 h}{2} + \frac{d^3}{6} \right)$$

Mostly  $h = 2d$

$$= \pi C_u \left( \frac{d^2 \times 2d}{2} + \frac{d^3}{6} \right)$$

$$= \frac{7\pi C_u d^3}{6}$$

$$\therefore C_u = \frac{6T}{7\pi d^3}$$

Applied torque জানলে  $C_u$  জানা যায়.

Exam এ derivation, integration করে  $T = \pi C_u \left( \frac{d^2 h}{2} + \frac{A d^3}{4} \right)$   
 এর derive করতে হবে। [See from book]

Porc H<sub>2</sub>O pressure:

no derivation needed.

$$\Delta u = u_3 + u_1$$

$$= B [\Delta G_3 + A (\Delta G_1 - \Delta G_3)]$$

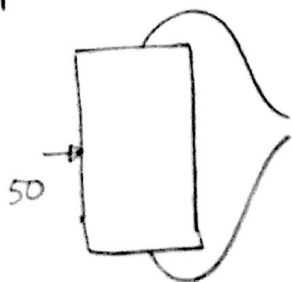
২৩৪৩৩ p.w.p develops → 1) when apply cell pressure  
 2) when apply additional load

$G_3$  = change in lateral pressure

If we apply both the cell pressure and additional load at same time then  $\Delta u = \dots$   $G_1$  is change in add. load at a small time

$B$  = depends on <sup>degree of</sup> saturation of sample parameter

$A$  = " consolidation of sample parameter



cell pressure 50      change to 60  
 the p.w.p = 30      p.w.p = 35

$$\therefore B = \frac{35 - 30}{60 - 50} = \frac{5}{10} = 0.5$$

saturated condition, cell p.f., the increase in p.w.p. if B is from .9 to .95 then it is considered saturated practically. (is theoretically saturated)

Fully saturated state p.w.p = 1.

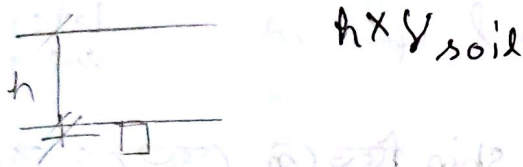
⇒ p.w.p can be negative: Highly o.e state highly dense state p.w.p decreases with application of cell pressure.

dense state volume ↑, so void ↓, so water content (is) increases, so volume ↑, so water content (is) increases, so pressure will decrease.

LATERAL EARTH PRESSURE

Earth pressure 2 types

- 1) V. pressure - fore overburden, <sup>easy</sup> to determine



- 2) Lateral E.P :  $K \times V \times h$   
 $\rightarrow$  co-eff of lateral earth pressure.

Automatically induced in soil.

Depends on: 1) Physical characteristic of soil  
 2) Deformation " of structure.

Soil 2 types: cohesive, cohesionless

- 1) So from phy. characteristic of soil  $\rightarrow$  cohesionless soil  
 $\rightarrow$  cohesive soil

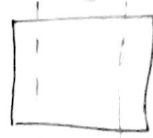
if 2 ~~para~~ parameters exist then  $c - \phi$  soil.  
 of friction

- 2) Def. of strc — i) No deformation  
 ii) lateral expansion (Active Earth pressure)  
 $\downarrow$  lateral stress  
 max<sup>m</sup> due to shear  
 so failure condition taken



3) fails due to lateral contraction.  $\uparrow K_{yh}$ , so contract করে, fail করে,

so  $K_p =$  co-ef of passive E.P

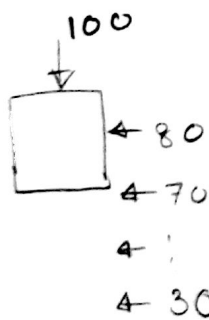


9. Def<sup>n</sup>  $K_o, K_p, K_a$ .

The ratio of ~~to~~ Lateral E.P at this condition is co-ef of  $\sim$  to V.  $K_o = \frac{K_o \gamma h}{\gamma h}$

A.E.P:

\* To reduce L.E.P we can move the support apart



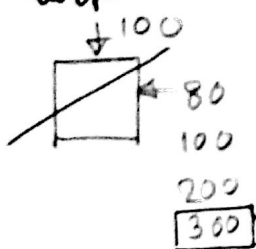
suppose 30 কৰিলে failure surface develop কৰিলে, 20, 10, 0 হ'ব " " অৱস্থাত, so max<sup>m</sup> shear at which failure 30

$\therefore$  A.E.P = 30  $\therefore K_a = \frac{30}{100} = \frac{63}{61}$

At failure condition  $\downarrow$  30 = 63

P.E.P:

~~lateral~~ lateral contraction  $\uparrow$  fail কৰিলে  $\uparrow$  L.P.



300  $\uparrow$  L.P তিল failure surface.

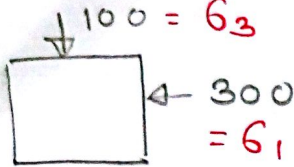
400, 500, 600 হিলে " " অৱস্থাত,

so the min<sup>m</sup> shear = 300

100 ft always 300 ft 2B, 2C, 2D?

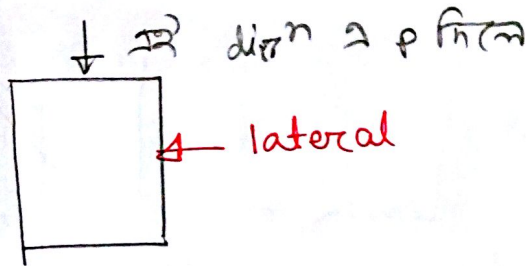
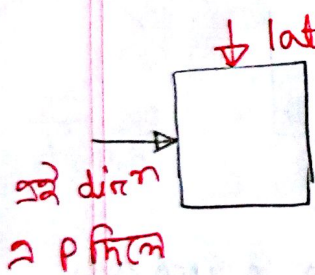
$\therefore P.E.P = 300$

$\therefore K_p = \frac{300}{100} = 3.00 = \frac{G_1}{G_3}$

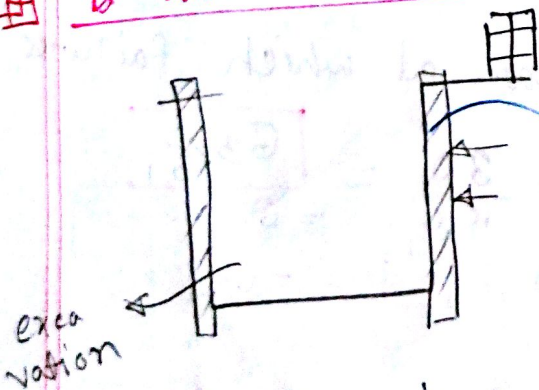


\* Practically v. load doesn't change that much. so we are only considering lateral load.

$K_a < K_0 < K_p$



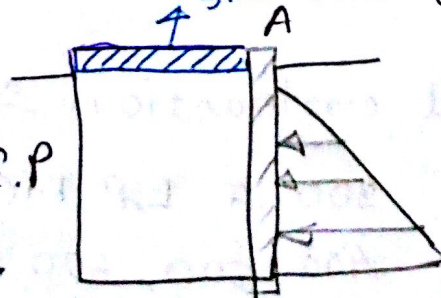
E.P at rest:



stiffness बढा शकत moves away, so A.E.P

still शकत E.P @ π.

slab (2nd 3rd)



so if the p is so this will be A.E.P cause A point free.

এ মমেন্ট এ স্লাব বাতানো, A আটকে গেল, so E.P @ rest.

যদি A.E.P এ fail না করে (অভ্যন্তরীণ strutting/bracing দিয়া) হয়, Then consider E.P @ Rest.

Bracing না দিলে consider A.E.P.

We don't want deformation, so want E.P @ R.

□ E.P @ Rest :

$$\sigma_h = \sigma_3 = K_0 \sigma_v = K_0 \gamma h \quad \therefore \sigma_v = \gamma h$$

$\downarrow$   
vertical p.

$$K_0 = \frac{\sigma_h}{\sigma_v}$$

$$\text{Lateral strain } \epsilon_h = \frac{1}{E} [\sigma_h - \mu (\sigma_v + \sigma_h)]$$

$\downarrow$   
poisson ratio

$$\Rightarrow \sigma_h =$$

We won't allow deformation  $\therefore \epsilon_h = 0$

$$\sigma_h - \mu \sigma_v - \sigma_h \mu = 0$$

$$\therefore \sigma_h = \frac{\mu}{1-\mu} \sigma_v \quad \text{and} \quad \sigma_h = K_0 \sigma_v$$

$$\Rightarrow \sigma_h (1-\mu) = \mu \sigma_v$$

$$\therefore \text{from these two} \quad K_0 = \frac{\mu}{1-\mu}$$

determination of  $\mu$  is very difficult, so try to avoid it.

So we use empirical relations.

1) ~~cohesionless~~ ~~consolidated~~ soil এ  $\phi$  জানলে  
(sandy)

for flat ground surface

Jaky's formula:  $k_0 = 1 - \sin \phi'$

$\therefore \phi$  determined in drained condition (for sandy and NC)

$k_0$  for over C =  $(1 - \sin \phi) \cdot \text{OCR}$   
over consolidation ratio

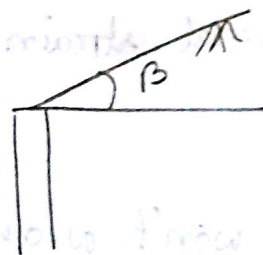
(\*) If we determine LL, PL and PI: for clayey

$k_0 = 0.19 + 0.233 \log (IP)$  (NC)

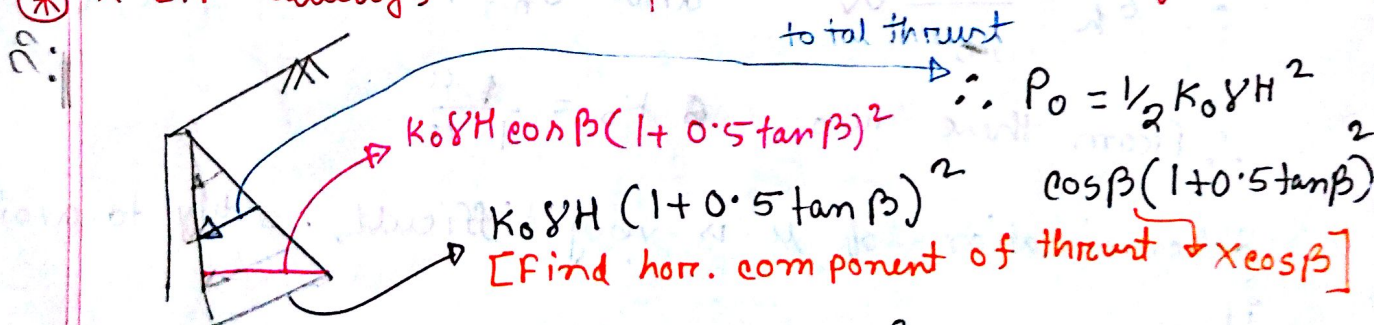
$k_0(oc) = k_0 \sqrt{\text{OCR}}$  (OC)

(\*) If inclined soil then  $P \uparrow$   $\Delta$   $\text{fr}$

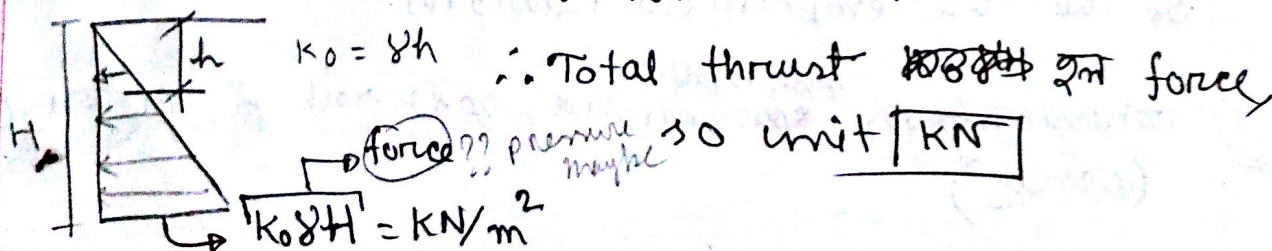
$\therefore \text{ff. } (1 + 0.5 \tan \beta)^2 k_0(oc) = \sqrt{\text{OCR}} \cdot k_0$



(\*) L.E.P. always works parallel to earth surface



$\gamma = 16 \text{ kN/m}^3$   $h = 5 \text{ m}$



$$\therefore \text{Total thrust per unit width} = \frac{1}{2} K_0 \gamma H \times H$$

$$= \frac{1}{2} K_0 \gamma H^2$$

Lec - 17

25.11.15  
Wednesday

Earth P. Theory:

- 1) Rankine's theory
- 2) Coulomb's theory

for A & P E.P } for cohesionless and cohesive soil  
of horizontal and inclined ground

And under the heading of surface

- Water Table
- Soil stratification
- load

Graphical method  
Culmann's method  
2)

A.E.P

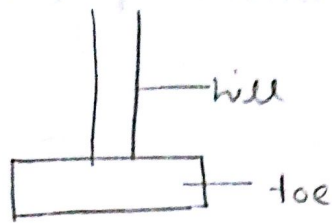
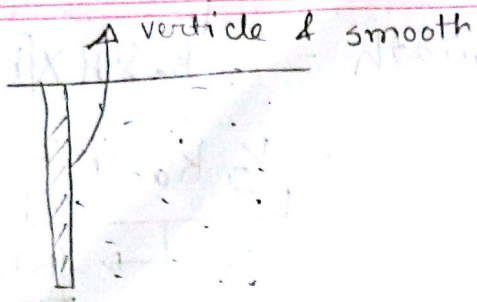
Cohesionless soil:

Rankine's theory:

- infinite soil
- homogeneous

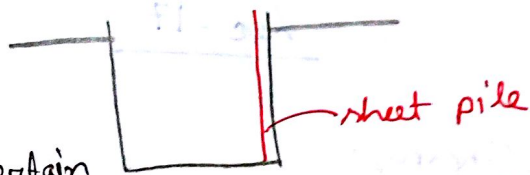
Ground surface horizontal/inclined

most important: soil and retaining wall in contact  
surface vertical & smooth



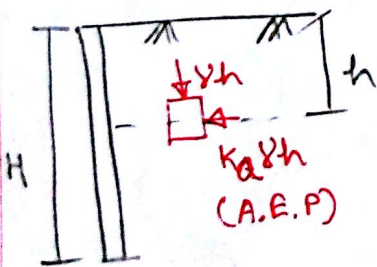
basement করতে retaining wall design করা যায় না, শুধু sheet pile / pile.

wall smooth করতে certain কাজ করতে হয়, plastic দিয়ে casting করলে smooth.



4. stress element এর stresses A parallel to PQ  
stress at B parallel to PC

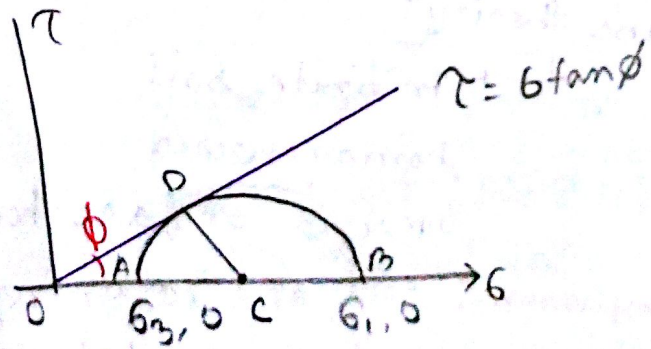
Let's assume that active earth pressure prevails



$$K_a \gamma h < \gamma h$$

$$\downarrow \gamma h = \sigma_1$$

$$\therefore \left[ \begin{array}{c} \sigma_1 \\ \sigma_3 \end{array} \right] \leftarrow K_a \gamma h = \sigma_3$$



cohesionless soil  $\therefore \tau = \sigma \tan \phi$

$\therefore \tau = \sigma \tan \phi$  (failure envelop) passing through origin

$$\begin{aligned}
 K_a &= \frac{\sigma_3}{\sigma_1} = \frac{OA}{OB} = \frac{OC - AC}{OC + BC} \\
 &= \frac{OC - CD}{OC + CD} \\
 &= \frac{OC/OC - CD/OC}{OC/OC + CD/OC} = \frac{1 - \frac{CD}{OC}}{1 + \frac{CD}{OC}}
 \end{aligned}$$

$\frac{CD}{OC} \rightarrow \sin \phi$

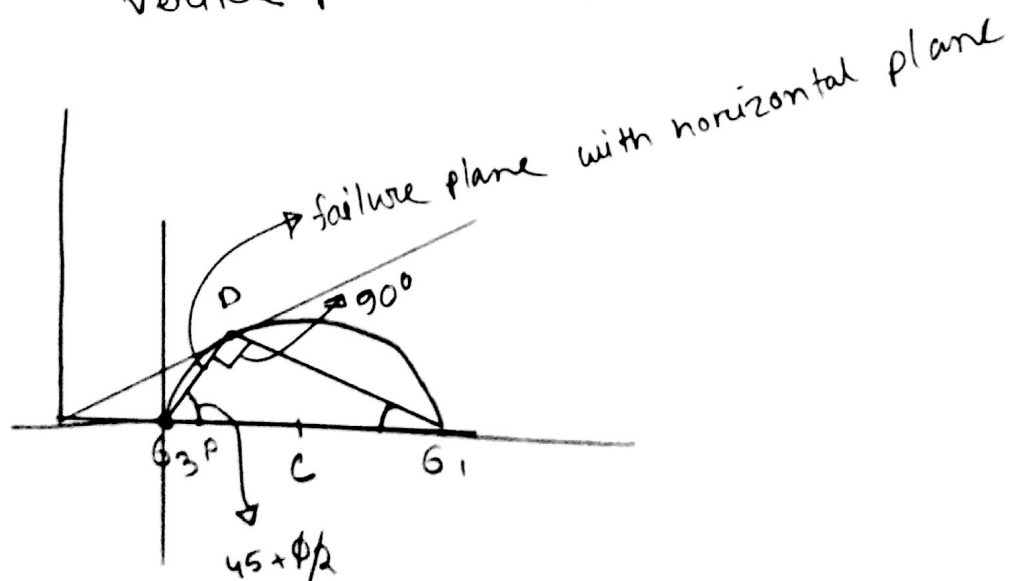
$$\therefore K_a = \frac{1 - \sin \phi}{1 + \sin \phi} = \tan^2 (45^\circ - \phi/2)$$

\* Angles must be in degrees.

\* orientation of failure plane:

$\sigma_1$  working horizontal so —

$\sigma_3$  " vertical plane so |





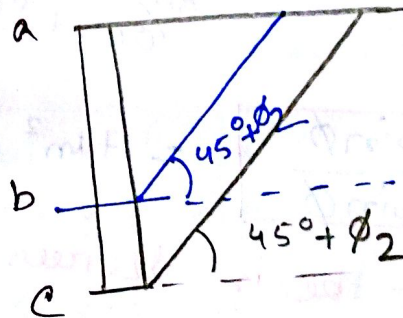
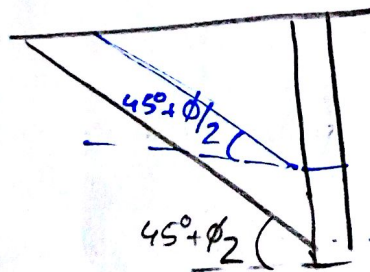
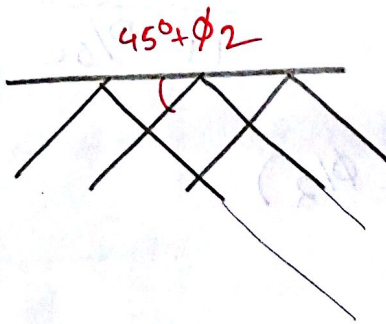
slope maintain  $\phi$  cause always

fails at  $45^\circ + \phi/2$

Depending on height of retaining wall failure ori.

$45^\circ + \phi/2$

Q. Draw ori. of failure plane for A.E.P

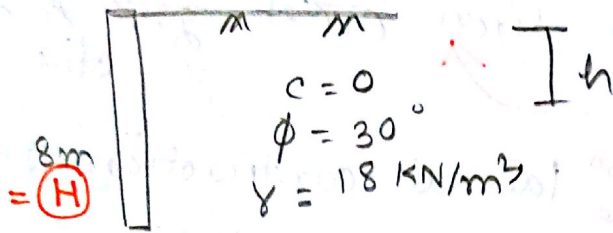


ab height  $\Rightarrow$  blue failure orientation.

ac height  $\Rightarrow$  failure

so 2 failure  $\Rightarrow$  failure depending position of soil.

Problem:



Ac. Thrust = ?

↓  
force

Active E. Pressure का ग्राफ बनाना

st-1:

$$K_a = \frac{1 - \sin \phi}{1 + \sin \phi} = \frac{1 - \sin 30^\circ}{1 + \sin 30^\circ} = 0.333$$

st-2:

Active E.P  $P_a$  at any depth  $h$   $P_a(h) = K_a \gamma h$

$$= 0.333 \times 18 \times h$$

$$= 6h$$

$\therefore P_a(h) = 6h$  (st. line eqn)

Step-3:

$$P_a(0) = 6 \times 0 = 0$$

$$P_a(8) = 6 \times 8 = 48 \text{ kN/m}^2$$

↓  
it is pressure

\* Area का ग्राफ unit length consider

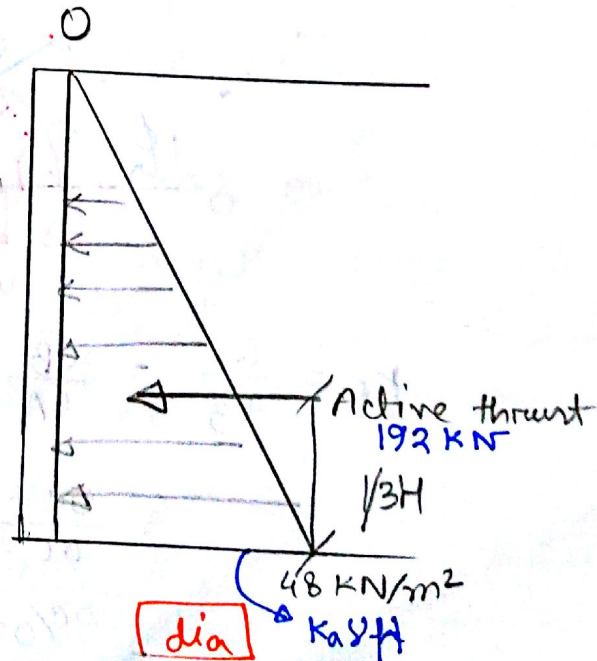
$$P_a = \frac{1}{2} \times 48 \times 8 = 192 \text{ kN}$$

(Thrust)

$$P_a = \frac{1}{2} K_a \gamma H \times H$$

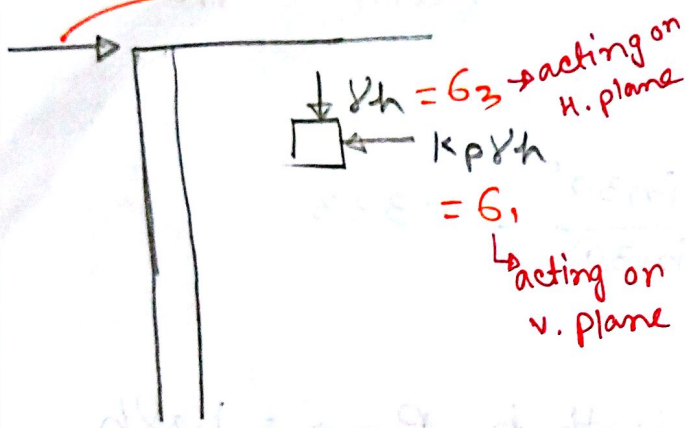
$$= \frac{1}{2} K_a \gamma H^2$$

} dir. ग्राफ में ग्राफ बनाना if diagram not wanted



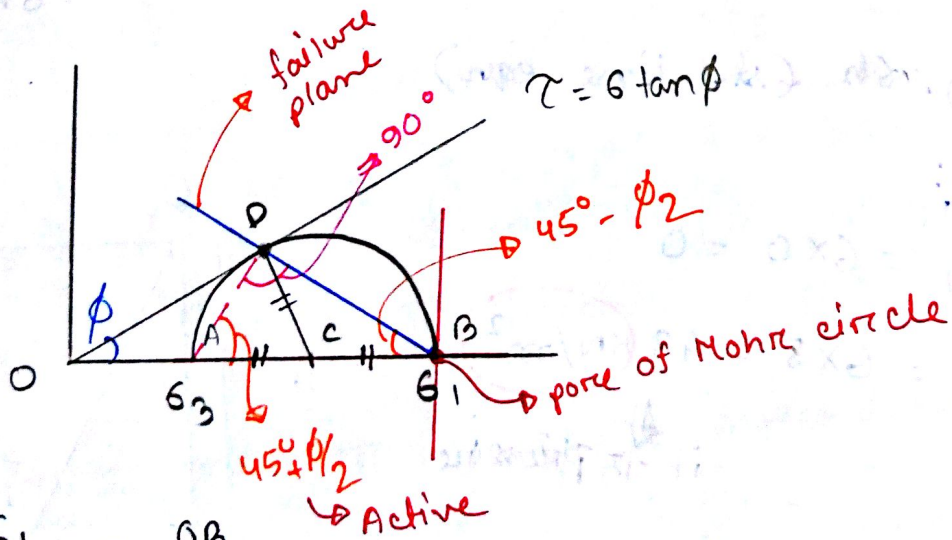
Pr-2: Passive

(Exm 2 का का भागले दिरन लरुय बूकर A तग P) ctive anive



lateral contraction of soil fail करत ररर.  
so  $K_p \gamma h > \gamma h$

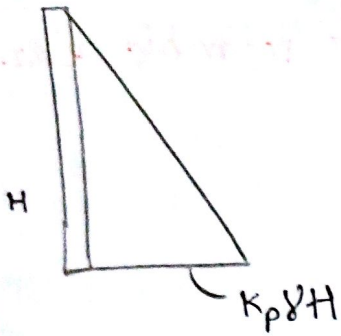
soil element very close to retaining wall, wall is smooth, so downward movement is no friction



$$\begin{aligned}
 K_p &= \frac{\sigma_1}{\sigma_3} = \frac{OB}{OA} \\
 &= \frac{OC + BC}{OC - AC} = \frac{OC + CD}{OC - CD} \\
 &= \frac{OC/OC + CD/OC}{OC/OC - CD/OC} = \frac{1 + \sin \phi}{1 - \sin \phi} = \frac{1}{K_a}
 \end{aligned}$$

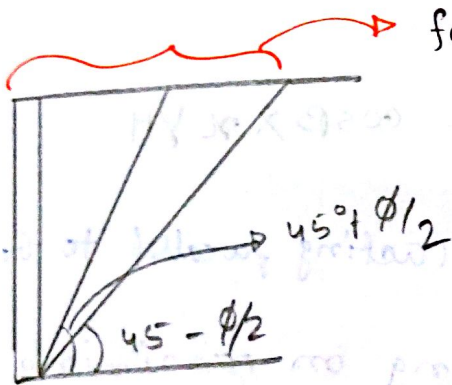
Total Thrust for P.E.P

$$P_p = \frac{1}{2} K_p \gamma H^2$$



Q. Draw orientation of failure plane for P.E.P?

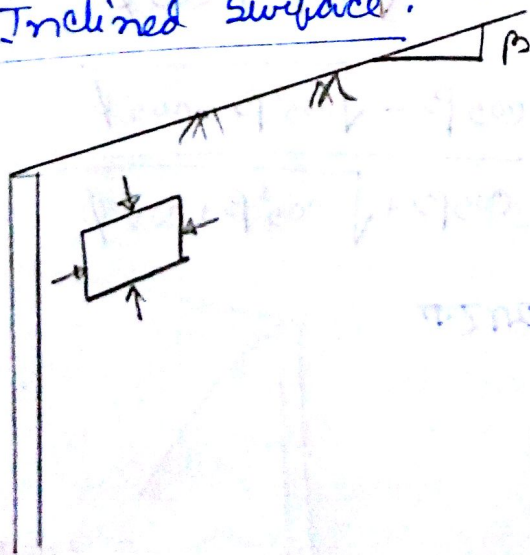
passive २ fail করতে movement  $\phi$  লাগবে,



for passive, so passive ২ fail করতে distance বেশি  
cause failure in passive ২  $45 - \phi/2$  ২ fail করতে, এটা achieve করতে অনেক deformation লাগবে,

Q. কারণ  $\phi$  movement & why?

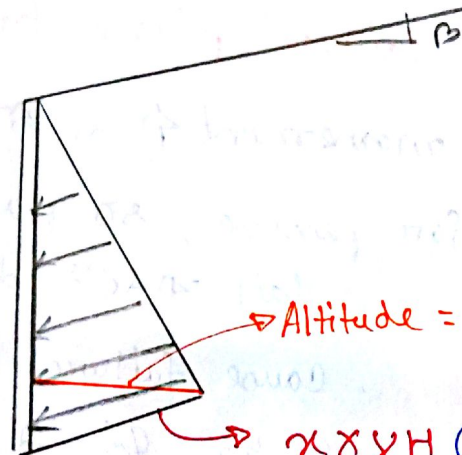
Q. A.E.P  $\rightarrow$  Inclined surface:



কারণ earth p. parallel to ground surface, so rambick element টুটকি হবে,

$$k_a = \left( \frac{\cos \beta - \sqrt{\cos^2 \beta - \cos^2 \phi}}{\cos \beta + \sqrt{\cos^2 \beta + \cos^2 \phi}} \right) \quad [\text{For recombic element}]$$

Pressure Distribution Dia:

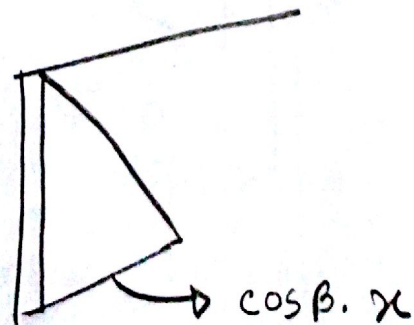


Total active thrust coming on retaining wall

$$P_a = \frac{1}{2} \cos \beta \frac{\cos \beta - \sqrt{\cos^2 \beta - \cos^2 \phi}}{\cos \beta + \sqrt{\cos^2 \beta + \cos^2 \phi}} \gamma H \cdot H$$

$$= \frac{1}{2} \gamma H^2 \cos \beta \frac{\cos \beta - \sqrt{\cos^2 \beta - \cos^2 \phi}}{\cos \beta + \sqrt{\cos^2 \beta + \cos^2 \phi}}$$

\* in most cases  $\cos \beta \cdot x$



21.11.89

20/11/89

21-11

$$P_a = \frac{1}{2} K_a \gamma H^2$$

Pressure dis. diagram  $\Rightarrow$  must use  $\gamma$  as  $K_a$ .

Thrust  $\Rightarrow$  अतमानते can be used.

lec - 18

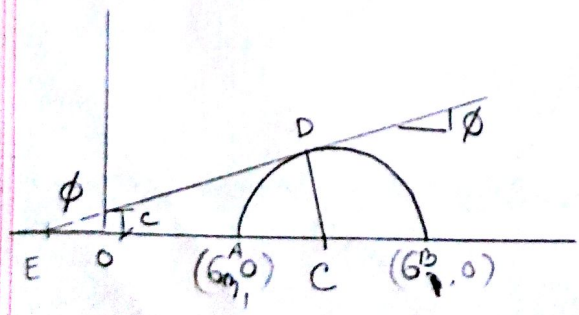
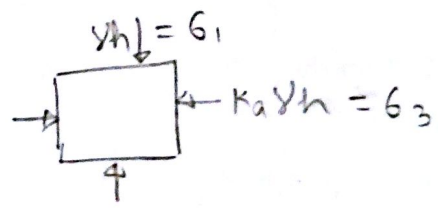
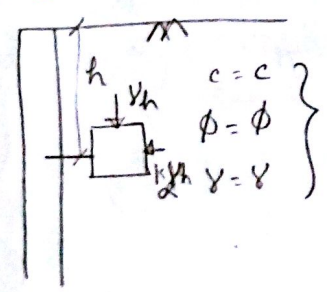
$$K_a = \frac{1 - \sin \phi}{1 + \sin \phi}$$

$$K_p = \frac{1 + \sin \phi}{1 - \sin \phi}$$

$$K_a = \frac{\cos \beta - \sqrt{\cos^2 \beta - \cos^2 \phi}}{\cos \beta + \sqrt{\cos^2 \beta - \cos^2 \phi}}$$

$$K_p = \frac{\cos \beta + \sqrt{\cos^2 \beta - \cos^2 \phi}}{\cos \beta - \sqrt{\cos^2 \beta - \cos^2 \phi}}$$

If a soil has cohesion & friction both:-  $c \phi$  soil  
Active condition:



$$\sin \phi = \frac{CD}{EC}$$

$$= \frac{CD}{EO + OE}$$

$$= \frac{G_1 - G_3}{2} \rightarrow \text{diameters}$$

$$= \frac{2r \cot \phi + \frac{G_1 + G_3}{2}}{2}$$

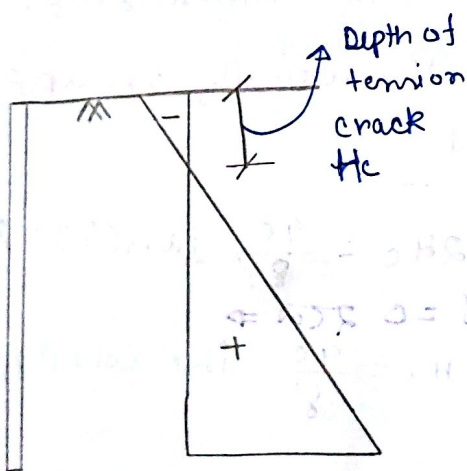
$$= \frac{G_1 - G_3}{G_1 + G_3 + 2r \cot \phi}$$

$$\therefore \sigma_3 = \left( \frac{1 - \sin \phi}{1 + \sin \phi} \right) \sigma_1 \rightarrow \frac{2c \cos \phi}{1 + \sin \phi} \rightarrow \text{simplify} = \sqrt{K_a}$$

$$= \left( \frac{1 - \sin \phi}{1 + \sin \phi} \right) \sigma_1 \rightarrow 2c \sqrt{\frac{1 - \sin \phi}{1 + \sin \phi}}$$

$$\sigma_3 = K_a \gamma h - 2c \sqrt{K_a}$$

Active E.P for  $c\phi$  soil



$$h = 0 \text{ at } \sigma_3 = -2c \sqrt{K_a}$$

Pressure (-)  $\Rightarrow$  tension, soil can't take much tension

Tension  $\Rightarrow$  tension crack,

At  $H_c$  lateral pressure zero.

$$\therefore \sigma_3 = 0$$

$$\therefore 0 = K_a \gamma H_c - 2c \sqrt{K_a}$$

$$\Rightarrow H_c = \frac{2c \sqrt{K_a}}{\gamma K_a}$$

$$= \frac{2c}{\gamma \sqrt{K_a}}$$

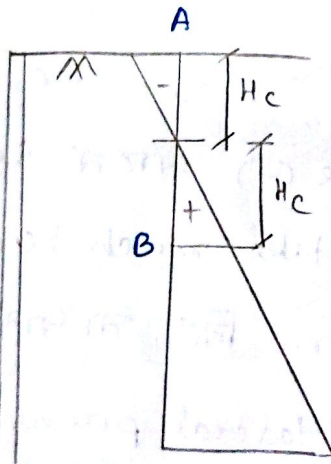
$$= \frac{2c}{\gamma} \frac{1}{\sqrt{\tan^2(45 - \phi/2)}}$$

$$= \frac{2c}{\gamma} \cos(45 - \phi/2)$$

$$= \frac{2c}{\gamma} \tan(45 + \phi/2) \quad [\text{Prove for a } c\phi \text{ soil the depth of tension crack...}]$$

for purely cohesive soil  $\phi = 0$

$$\therefore H_c = \frac{2c}{\gamma} \quad [\text{Prove for cohesive soil}]$$



AB  $\Rightarrow$  total thrust zero.

called **theoretically unsupported height**

$$H_u = 2H_c = \frac{4c}{\gamma} \tan(45 + \phi/2)$$

$$\phi = 0 \Rightarrow \tan 45 = 1$$

$$\therefore H_u = \frac{4c}{\gamma} \quad (\text{for cohesive soil})$$

$$c = 20 \text{ kN/m}^2$$

$$\gamma = 16 \text{ kN/m}^3$$

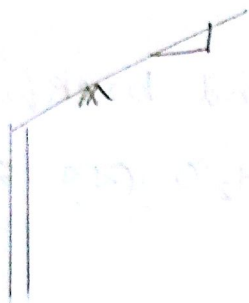
$$\therefore H_u = \frac{4 \times 20}{16} = 5 \text{ m, so theoretically } \frac{4c}{\gamma}$$

cohesion  $\frac{4c}{\gamma}$  & excavation a support  $\frac{4c}{\gamma}$

**For Passive E.P.:**

$$P_p = k_p \gamma h + 2c \sqrt{k_p} = 61$$

☐  $c-\phi$  soil with sloping surface:

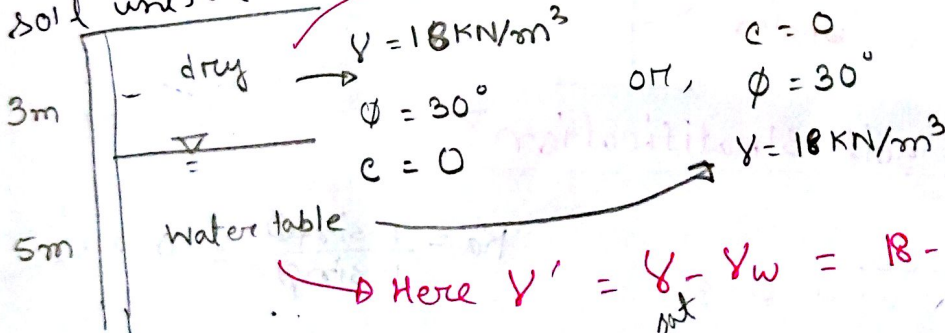


graphical method used,  
But formula error, don't need to  
memorize.

☐ Effect of water table on A. & P earth pressure:

Active E.P is only for soil.

soil uniform



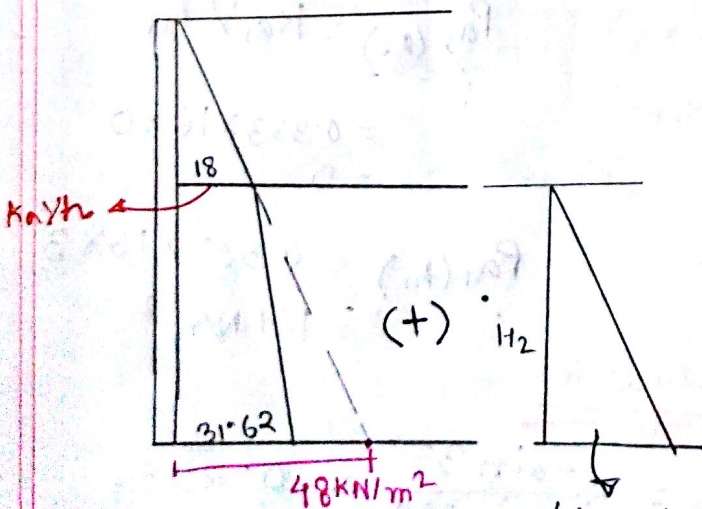
\*  $\gamma_{sat}$  3 वनर  
 $\gamma_{sat}$  3 वनर  
 गलत ।

Here  $\gamma' = \gamma - \gamma_w = 18 - 9.8$

$K_{aH} = 0.333 \times 18 \times 3 = 18 \text{ kN/m}^2$

for  $H_2O$

$0.333 \times 18 \times 3 + 0.333 \times (18 - 9.81) \times 5$   
 $= 31.62 \text{ kN/m}^2$   
 submerged unit wt



$H_2O$  नर शकल,  $K_a \gamma H$

$= 0.333 \times 18 \times 8$   
 $= 48 \text{ kN/m}^2$

if whole was filled  
 with  $H_2O$  then  $P = \gamma_w H_2$   
 $= 9.81 \times 5 = 49.2$

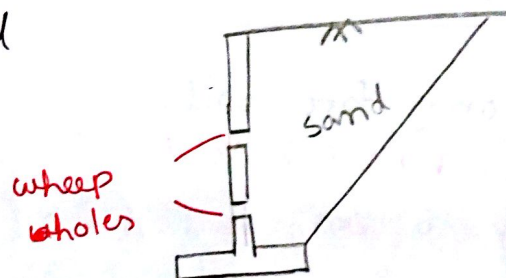
∴ water শাকলে pressure develop করবে, its not good.

কাজ retaining wall এ holes, and backfill material sand/coarse soil. যেন H<sub>2</sub>O বের হতে পারে।

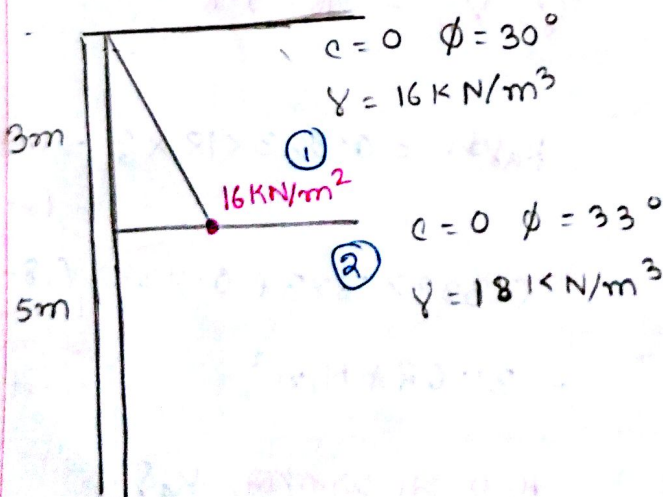
clay শাকলে হবে না,

যদি earth pres. থাকবে  $45 + \phi/2$  or  $45 - \phi/2$

অন্য backfill



### Effect of soil stratification:



$$K_a = \frac{1 - \sin \phi}{1 + \sin \phi} = 0.333$$

Layer ①:

$$P_{a1}(h_1) = K_{a1} \gamma_1 h_1$$

$$= 0.333 \times 16 \times 0$$

$$= 0$$

$$P_{a1}(h_1) = 0.333 \times 16 \times 3$$

$$= 16 \text{ kN/m}^2$$

2) Layer 2

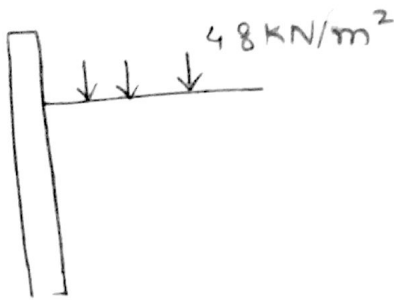
$$K_{a2} = \frac{1 - \sin 33^\circ}{1 + \sin 33^\circ} = 0.295$$

কাজ soil uniform না

3m → soil layer due to vertical pressure

$$= \gamma \times 3 = \frac{48}{2} \text{ KN/m}^2$$

→ further replace with  
 48 KN/m<sup>2</sup>

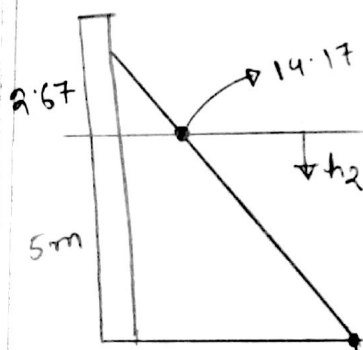


→ 48 KN/m<sup>2</sup> → soil layer  
 → soil layer then height  
 height of soil of layer?

$$\therefore 48 = \gamma_2 H \Rightarrow \frac{48}{18} = 2.67$$

∴ Equivalent height,

$$H_e = \frac{a}{\gamma_2}$$

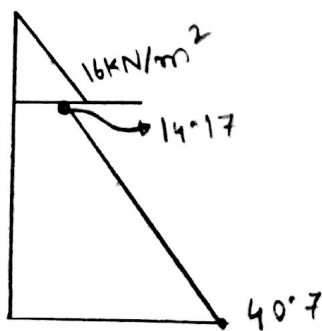


$$K_a \times \gamma_2 \times (5 + 2.67) = 0.295 \times 18 \times 7.67 = 40.7$$

$$P_{a_2}(h_2) = K_{a_2} \gamma_2 (H_e + h_2)$$

$$\text{If } h_2 = 0 \quad \therefore P_{a_2}(0) = K_{a_2} \times \gamma_2 \times H_e = 0.295 \times 18 \times 2.67$$

$$= 14.17 \text{ KN/m}^2 \rightarrow \text{force layer ②}$$



→ break due to because of  
 change of angle of friction.

φ ② → break, so → break.

φ ② → break, so → break.

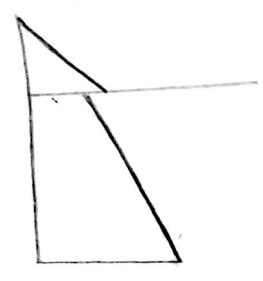
slope of the lines depend on  $\gamma$  if  $\gamma$  slope flat.

$\gamma \downarrow$  " " " still.

Q. Exam  $\gamma$  वनन  $\gamma_1 > \gamma_2$  and  $\phi_1 < \phi_2$  then pressure distribution वनन.

$\downarrow$   
① slope flat

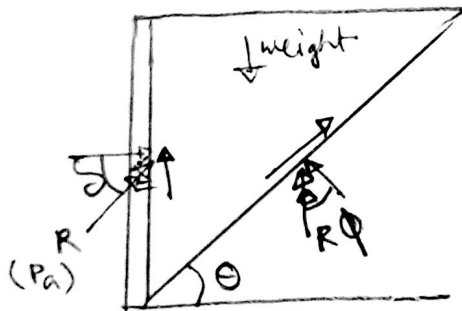
$\downarrow$   
① break inside



lec-19

Coulomb's Method:

- 1) Soil homogenous & isotropic
- 2) Coulomb considering the equilibrium of failure wedge.  
(Rankine's said the equilli of a soil element)  
Coulomb says failure always in a wedge.  
Wedge is rigid body.
- 3) Wall verticle & smooth or rough or rough

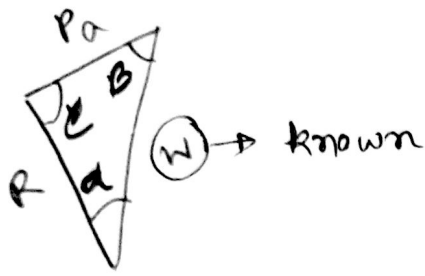


pressure acting normal to surface. ( $\rightarrow$ )

A.E.P a wedge wants to go down. = surface smooth  
or, so friction  $\rightarrow$  friction (up) ( $\uparrow$ )

3 forces acting:

- 1) W (weight)
- 2)  $P_a$
- 3) Reaction (R)

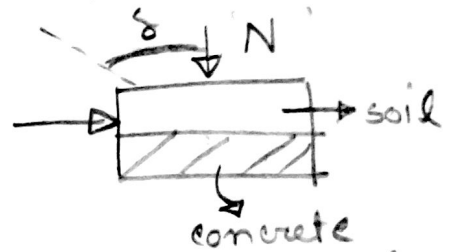


$$\frac{P_a}{\alpha} = R/\beta = \frac{W}{\gamma}$$

soil and soil  $\alpha$  friction  $\gamma$  failure angle of friction. ( $\phi$ )  
 soil & concrete  $\alpha$  " " failure " " wall " ( $\delta$ )

angle of wall friction can be calculated.

or (max)  $\delta$  is  $2/3$  of  $\phi$ .



max  $\delta$  failure angle is  $\phi$ .

$$\frac{P_a}{\sin \alpha} = \frac{W}{\sin \epsilon}$$

$$\therefore P_a = W \frac{\sin \alpha}{\sin \epsilon}$$

$W$  is area of wedge or failure angle  $\alpha$  is fixed, but failure angle  $\epsilon$  is not fixed.

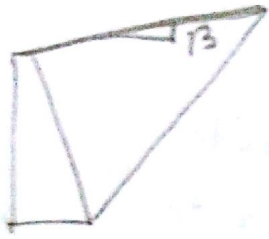
$P_a$  max  $\alpha$  is failure  $P_a$  value depends on —

retaining wall and G.L fixed, so  $W$  depends on  $\theta$ .

$\therefore P_a$  vs  $\theta$  respect  $\alpha$  differentiate,

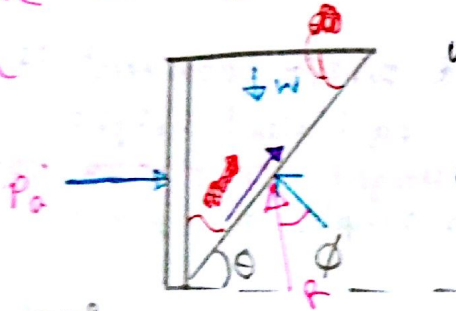
$$\frac{\partial P_a}{\partial \theta} = 0 \text{ when } \theta \text{ value is}$$

then  $W$  ??

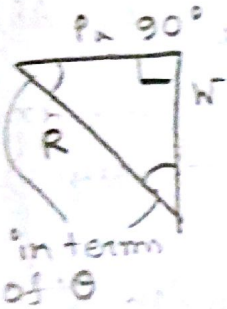


$K_a$  } Exam এ হিসেব দিবে,  
 $K_p$

Derive an eqn for A.E.P using Coulomb's theory when wall smooth & vertical, soil surface horizontal.



wall smooth, so friction শূন্য  
wall is smooth, so friction শূন্য



$$\frac{P_a}{\sin \phi} = \frac{W}{\sin \theta}$$

$$\frac{\partial P_a}{\partial \theta} = 0 \quad \text{সর্বোত্তম বা সর্বনিম্ন value এর জন্য}$$

then  $P_a$ .

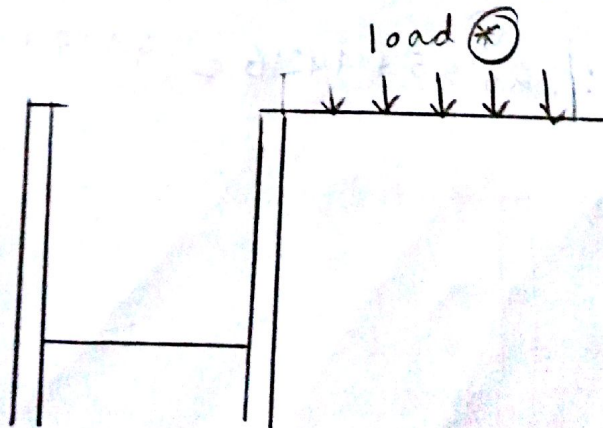
[B.M. Das Introduction to soil mechanics এ দেখা]

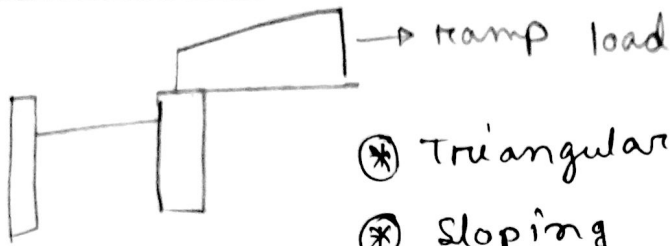
Coulomb's theory wall smooth না হলেও শূন্য, but Rankine's theory wall must be smooth

L.E.P on a rigid wall due to surcharge load on the surface backfill

load  $\otimes$  কারণে এর জন্য, for various reason. Called **surcharge load**

diff types of loading (PDF)

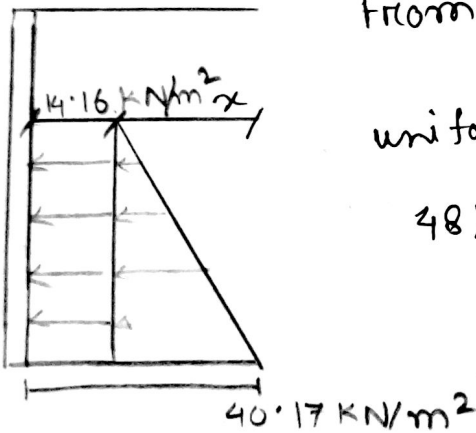




- ⊗ Triangular load finite
- ⊗ Sloping " infinite

□ Uniform load: uniform load ~~22222~~ convert it to equivalent height.

But eqn height ~~or~~ ~~22222~~, from example of previous class



uniformly distributed load  $48 \text{ KN/m}^2$

$$48 \times K_a = 48 \times 0.295 \text{ (for 2nd layer)}$$

$$= 14.16$$

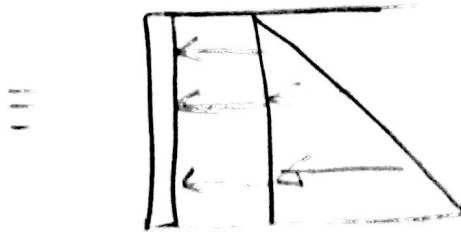
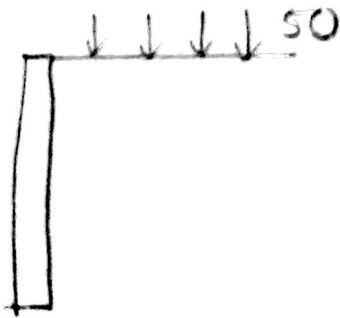
so str throughout

so 14.16 str for structure. Triangular variation for soil.

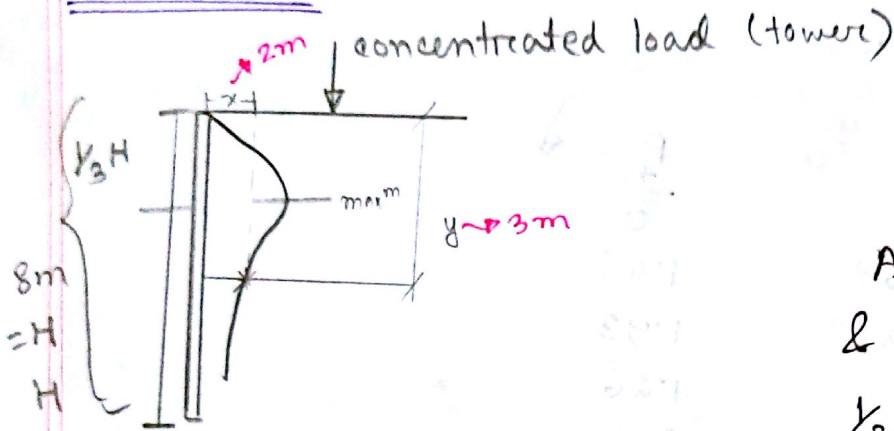
$\alpha$  only soil, no only A.E.P no surcharge

$$\therefore K_a \times \gamma_2 \times 5 = 0.295 \times 18 \times 5 = 26.55$$

$$\therefore 26.55 + 14.16 = 40.71 \text{ KN/m}^2$$



Point load :



As considering wall rigid so  $\sigma_{max}$  soil at A.F.P at rest & concentrated load.  $\frac{1}{3}H$  at  $\sigma_{max}$  pressure.

Exam  $\rightarrow$  only concentrated load  $\rightarrow$   $\sigma_{max}$  no soil considered  $\rightarrow$  particular point at pressure  $(x, y)$

$x = mH$

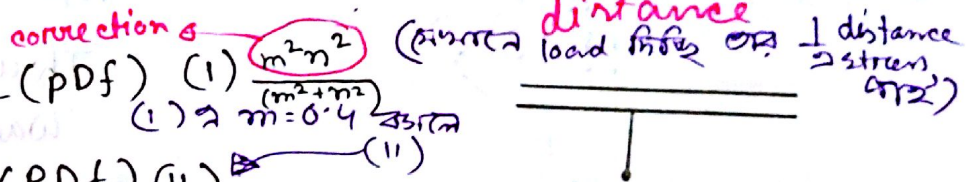
$\therefore m = \frac{x}{H} = 0.25$

$y = nH$

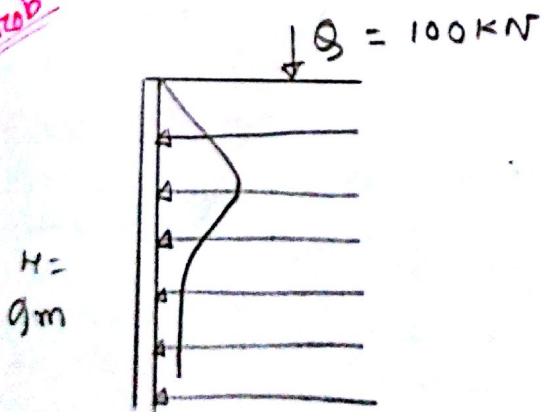
$n = \frac{y}{H} = 0.375$

$\otimes$  Dist<sup>n</sup> will happen at a perpendicular distance

$m > 0.4 \approx \text{eqn (PDF) (I)}$   
 $m \leq 0.4 = \text{eqn (PDF) (II)}$



Prob:



9m (is uniformly  $\sigma_{max}$ , But not less than 6)

$\therefore \frac{9}{6} = 1.5$

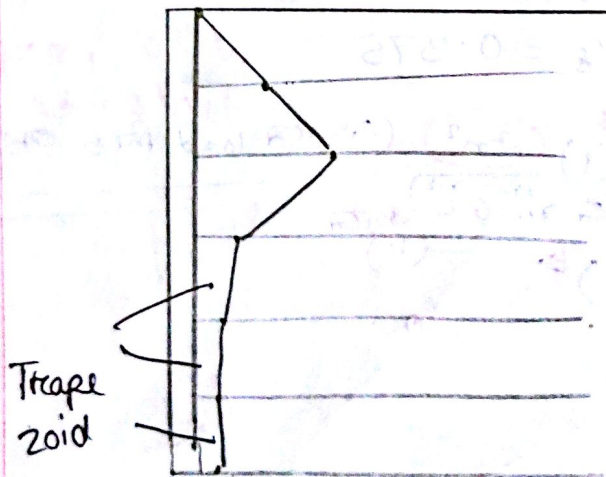
Step 1:  $m = \frac{x}{9} = 0.22$

$\therefore m < 0.4$

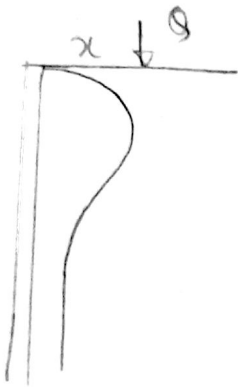
$\therefore P_a = \frac{0.28Q}{H^2} \cdot \frac{n^2}{(0.16+n^2)^3}$   
 $= \frac{0.28 \times 100}{9^2} \times \frac{n^2}{(0.16+n^2)^3}$

$$= \frac{0.346n^2}{(0.16+n^2)^3}$$

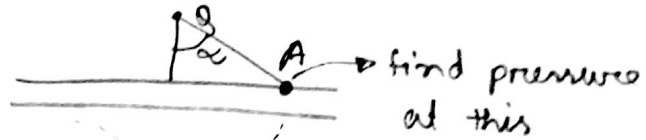
<u>Depth</u>	<u><math>n = \frac{y}{H}</math></u>	<u><math>\frac{P}{h} = \psi</math></u>
0	0	0
1.5	0.167	1.45
3	0.33	1.93
4.5	0.5	1.26
6	0.667	0.7
7.5	0.833	0.39
9	1	0.22



Total area  $\psi$  total  
Thrust acting on the  
Wall.

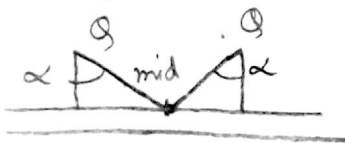


Plan of retaining wall



then ~~use~~ <sup>এটি</sup> co-ordinate কে  $\cos^2(1+\alpha)$  দিয়ে multiply করতে হবে  
not sure

thrust বস করতে বসলে total লোকোড  $\cos^2(1+\alpha)$  দিয়ে multiply.



mid point এ বসলে যে কোন প্রকারে ডান  $\cos^2(1+\alpha)$  দিয়ে গুণ করে ২ দিয়ে গুণ

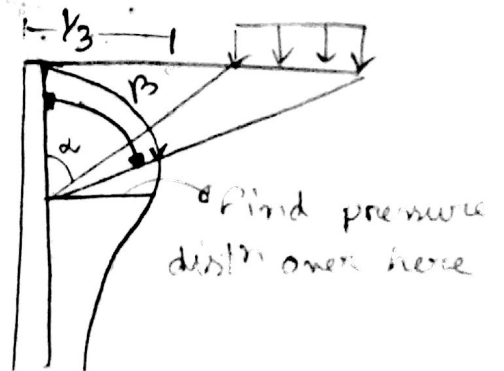
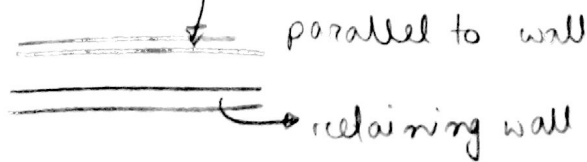
Line load:

For  $m > 0.4$

$$P_m = \frac{4q}{\pi} \frac{m^2 n}{(m^2 + n^2)^2}$$

$m = 0.4 \Rightarrow \dots$

Strip load:



For all loads strip, ramp,  $\Delta$  max<sup>m</sup> dist<sup>n</sup> at  $1/3$   
 $\beta$  &  $\alpha$  in radian.

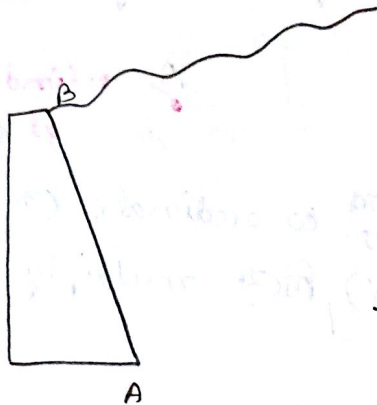
\* Exam  $\rightarrow$  point & line ২: ৩) formula (৩) গাণিতিক

সি,

Calman's

▣ Coulomb's Graphical Method: (consider active & cohesionless soil)

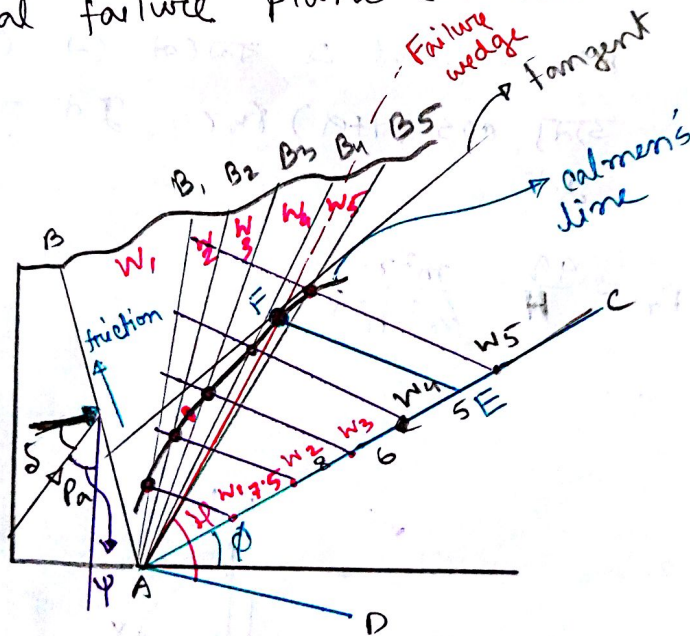
cohesionless soil विना (Graphical method when surcharge load not smooth)



असतल failure surface  $45^\circ + \phi/2$   
 एका रेटर line, एका रेटर line  
 करा.

This is a theory extension of Coulomb's (wedge) theory.

several failure plane consider करा,



$c = 0$   
 $\phi = \phi$   
 $\gamma = \gamma$

Backfill रतल  
 wall तऱु ळरतऱु गऱरतऱु  
 soil.

From A in the direction of backfill draw a line of  $\phi$  angle

BAB<sub>1</sub> → fail करतल (Rankine's रतल) it will move down & friction up.



Reaction & friction resultant A.E.P ( $P_a$ ).

$P_a$  & reaction angle  $\delta$ , angle of wall friction.

draw vertical line  $P_a$  at angle  $\psi$ .

$$\psi > \phi,$$

again A point in opposite dirn of Backfill draw a line with angle  $\psi$ .

BAB, draw division cover  $\psi$ , per division draw scale  $\psi$  (area) draw  $\psi$ , draw area, draw  $\perp$  unit width  $\psi$ , so volm & then multiply by  $\gamma$ , so find weight

suppose  $W_1 = 1000 \text{ KN}$ , wt of ABB,

go to weight scale, suppose  $100 \text{ KN} = 1 \text{ cm}$

$$\therefore 1000 \text{ KN} = 10 \text{ cm}$$

$$W_2 = \text{wt of } AB_1B_2 = 750$$

$$W_3 = 800$$

$$W_4 = 600$$

$$W_5 = 500$$

from  $W_1, W_2, W_3, W_4, W_5$  draw parallel to line AD

AD is called reference line.

draw lines failure surface  $\psi$  (point  $\psi$  draw  $\psi$  area) draw smooth curve. draw calmen's lines.

draw a tangent from max<sup>m</sup> curvature,  
 " parallel to AC.

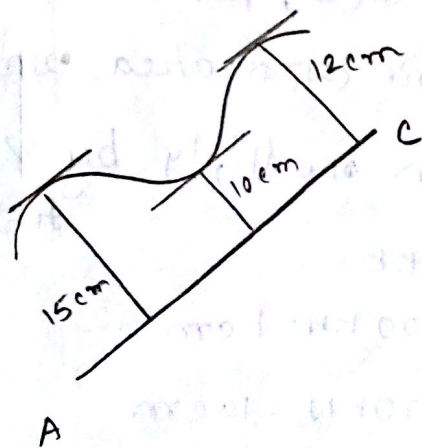
Tangent point F.

F point is || to AD, and AC can be cut.

FE = 12cm distance

scale is 100 kN = 1cm

$\therefore 12\text{cm} = 12 \times 100 = 1200 \text{ kN}$  (active pressure, thrust)



guyana failure

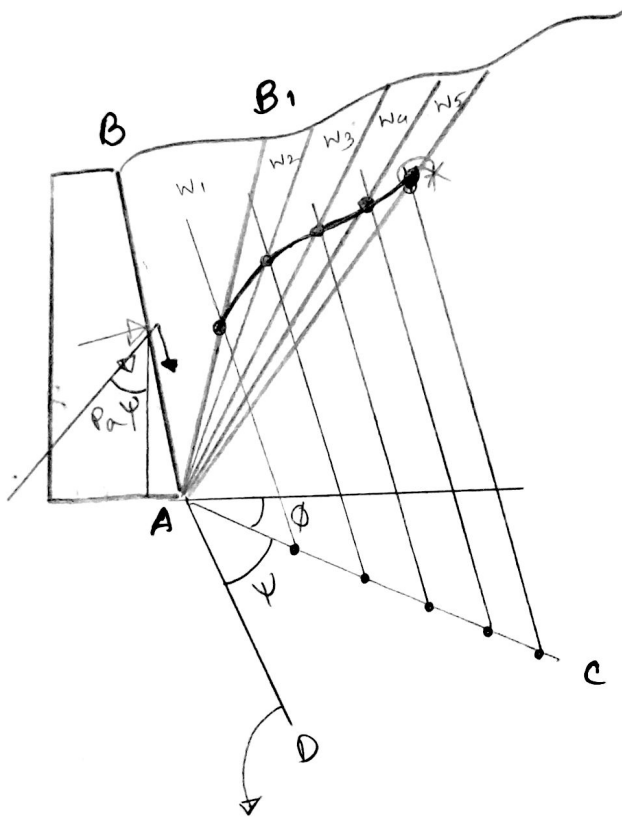
15cm is 3m, cause

active earth pressure is

definition of max pressure

A fail is 1200

Active Earth Pressure:



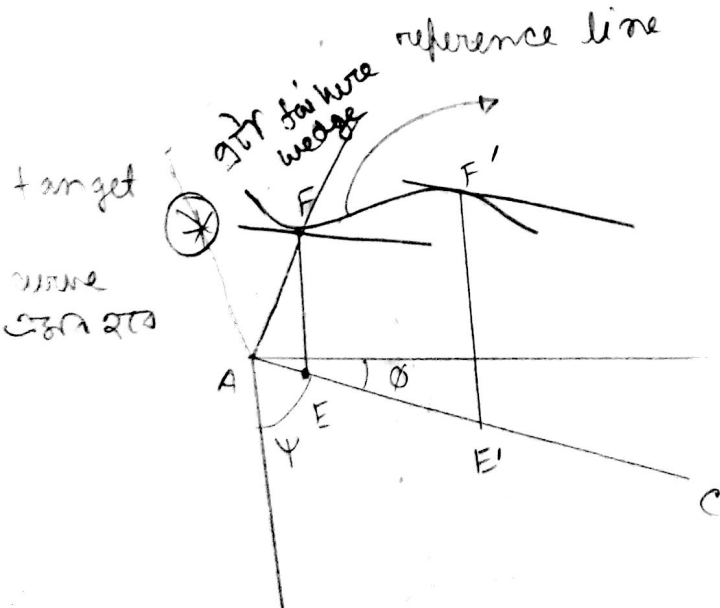
$c = 0$   
 $\phi = \phi$   
 $\psi = \psi$

Draw a line in opposite direction of Backfill //

inward & upward movement

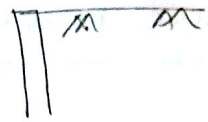
$\psi$  angle of pressure and vertical

$EF = 12 \text{ cm} \rightarrow$   $\rightarrow$  failure zone  
 $F'E' = 15 \text{ cm}$  failure

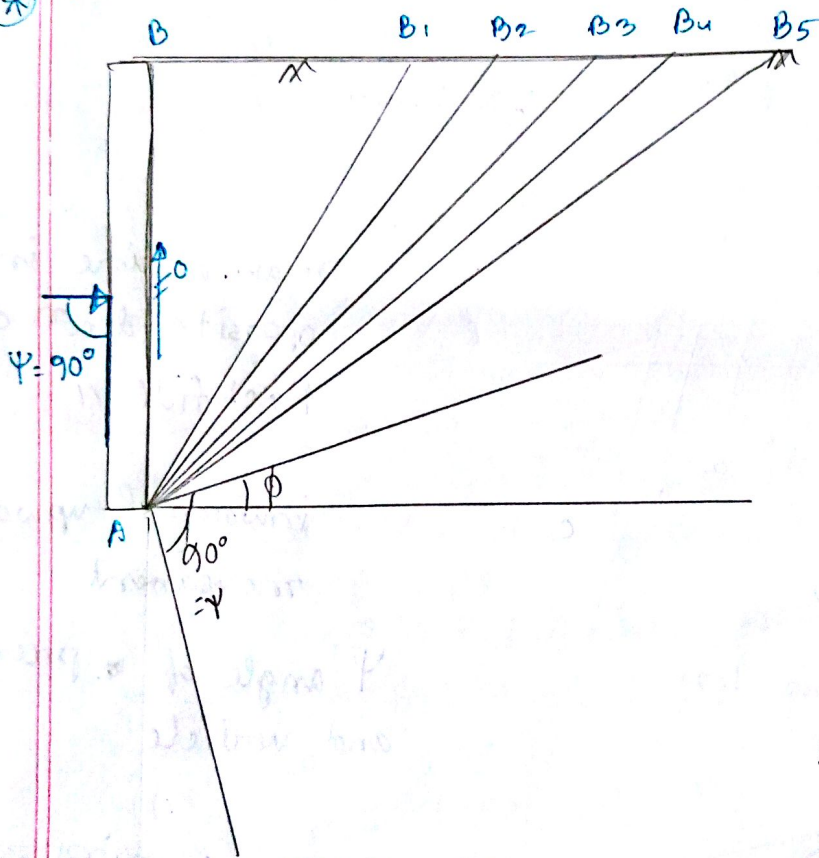


□ smooth & vertical wall, Ground plane.

[You indicate the failure wedge]  
Solve in calmen's method



⊛ Prob Prev. year (smooth wall)



we assume active pressure

Let  $AB_1 = 4'$

$BA = 10'$

scale 2 अंकताइ

but right angle  $\Delta$

$\therefore \text{Area} = \frac{1}{2} \times 10 \times 4$

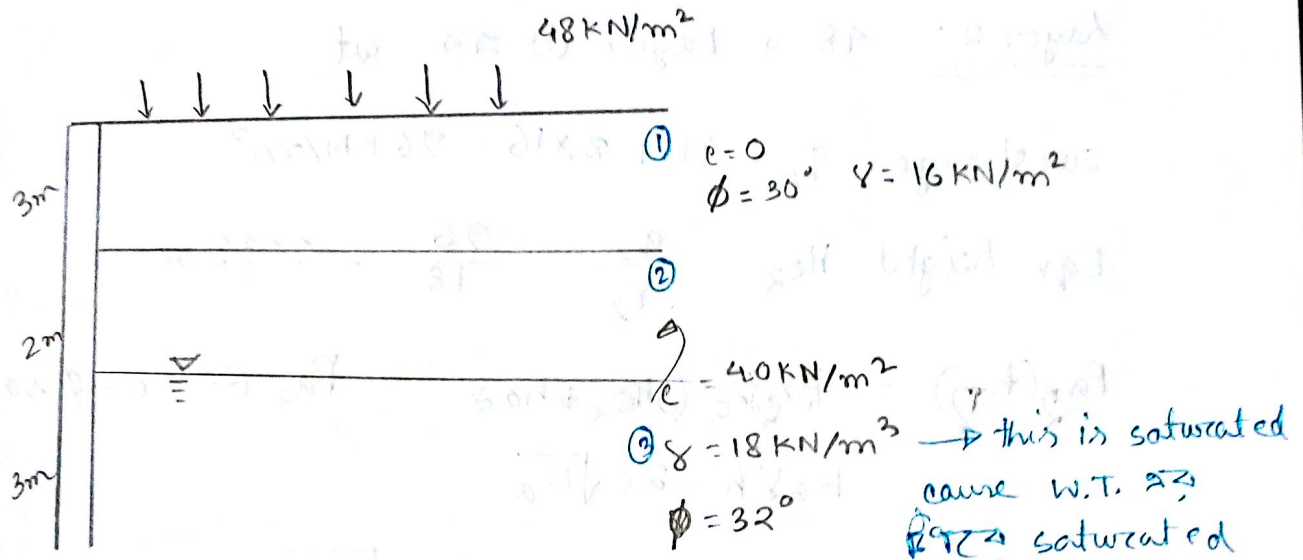
so graph (अंक) count  
अंकताइ अंक,

$\Delta \text{ area} = 20 \text{ m}^2$

$20 \times 8 = 160 \text{ kN}$   
↓  
16

Let's assume  $B_1B_2 = B_2B_3 = B_3B_4 = B_4B_5 = 4$

so अंक W same अंक, अंक truck.



Layer 1: Always see if there is surcharge

$$P_{a1}(h_1) = K_{a1} \gamma_1 (h_1) \rightarrow \text{surcharge থাকলে } h_1 \text{ গুণে } h+h_e \text{ দিয়ে বসবে হবে}$$

$$\text{Equivalent height} = \frac{q}{\gamma_1} = \frac{48}{16} = 3 \text{ m}$$

$$P_{a1}(h_1) = K_{a1} \gamma_1 (H_e + h_1)$$

$$\therefore K_{a1} = \frac{1 - \sin 30}{1 + \sin 30} = 0.333$$

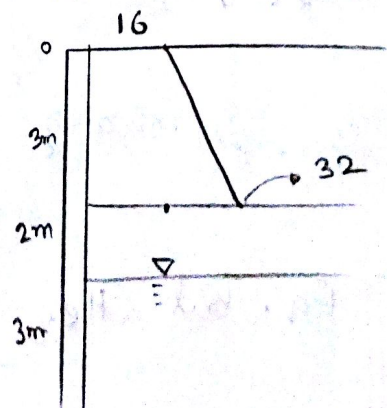
$$\therefore P_{a1}(h_1) = 0.333 \times 16 \times (3 + h_1)$$

$$= 5.33 \times (3 + h_1)$$

$$h_1 = 0 \Rightarrow P_{a1} = 16$$

$$h_1 = 3 \Rightarrow P_{a1}(3) = 31.98$$

$$= 32 \text{ kN/m}^2$$



⊗ Any F.P problem see if any surcharge

Layer 2: 48 + Layer ① ⇒ wt

$$\text{surcharge } q_2 = 48 + 3 \times 16 = 96 \text{ kN/m}^2$$

$$\text{Eqv height } H_{e2} = \frac{q_2}{\gamma_2} = \frac{96}{18} = 5.33 \text{ m}$$

$$P_{a2}(h_2) = \cancel{K_{a2} \gamma_2 (H_{e2} + h_2)} \quad P_{a2} \text{ (c-}\phi \text{ soil)}$$

$$K_a \gamma h - 2c \sqrt{K_a}$$

$$P_{a2}(h_2) = K_{a2} \gamma_2 (h_2 + H_e) - 2c \sqrt{K_{a2}}$$

$$K_{a2} = \frac{1 - \sin 32}{1 + \sin 32} = 0.31$$

$$P_{a2}(h_2) = 0.31 \times 18 (h_2 + 5.33) - 2 \times 40 \sqrt{0.31}$$

$$= 5.58 (5.33 + h_2) - 44.54$$

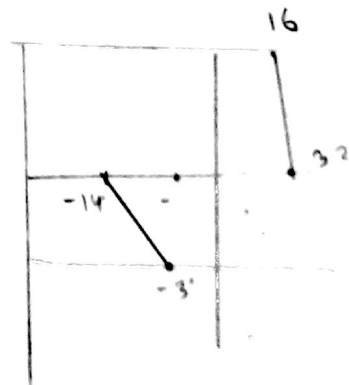
$$P_{a2}(0) = -14.8 \text{ kN/m}^2$$

$$P_{a2}(2) = \cancel{1000} - 3.6 \text{ kN/m}^2$$

⊗ : surcharge  $q_3 = 48 + 3 \times 16 + 2 \times 18$

$$= 132 \text{ kN/m}^2$$

$$\text{Eq. wt } H_{e3} = \frac{q_3}{\gamma_3} = \frac{132}{(18 - 9.81)} = 16.11 \text{ m}$$



⊛ identify layer ~~water~~ depending on soil type

⊛ then surcharge ⊛ then eqn height

$$P_{a3}(h_3) = K_{a3} \gamma_3 h_3 - 2c \sqrt{K_{a3}}$$

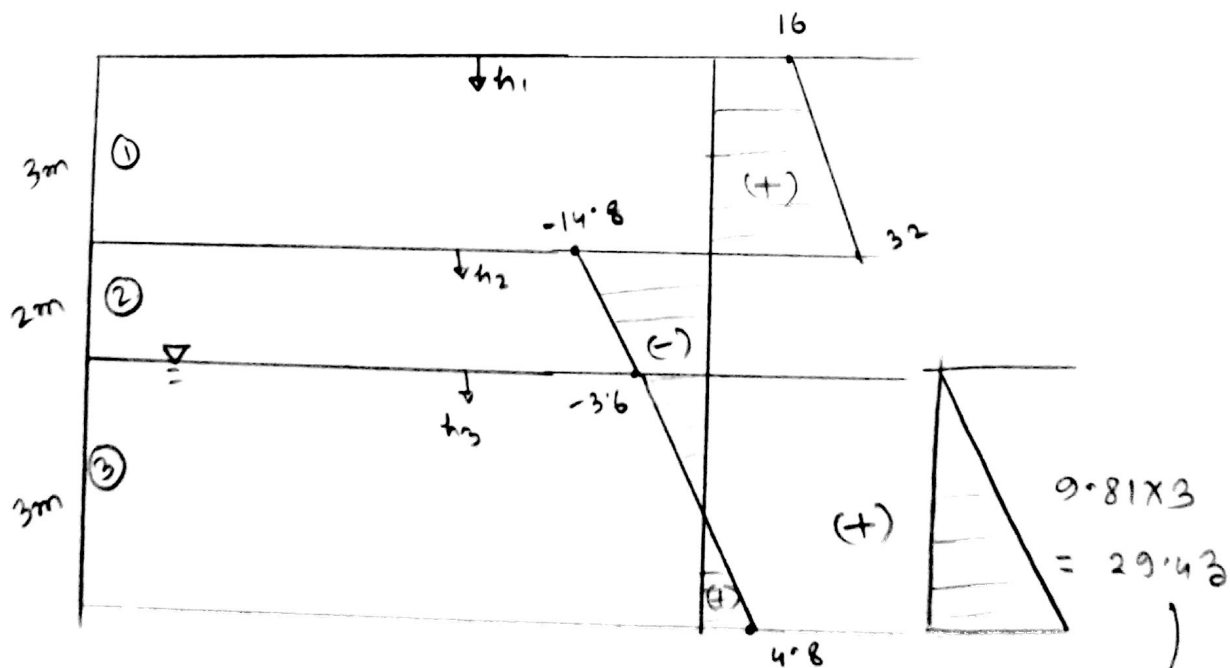
$$K_{a3} = 0.31$$

$$P_{a3}(h_3) = 0.31 \times (18 - 9.81) \left( h_3 + 16.1 \right) - 2 \times 40 \sqrt{0.31}$$

$$= 2.54 (h_3 + 16.1) - 44.54$$

$P_{a3}(0) = -3.64$  (same in layer ② & ③ cause break 2<sup>nd</sup> for  $\phi$  or  $\delta$ ,  $2c$  same, so no change)

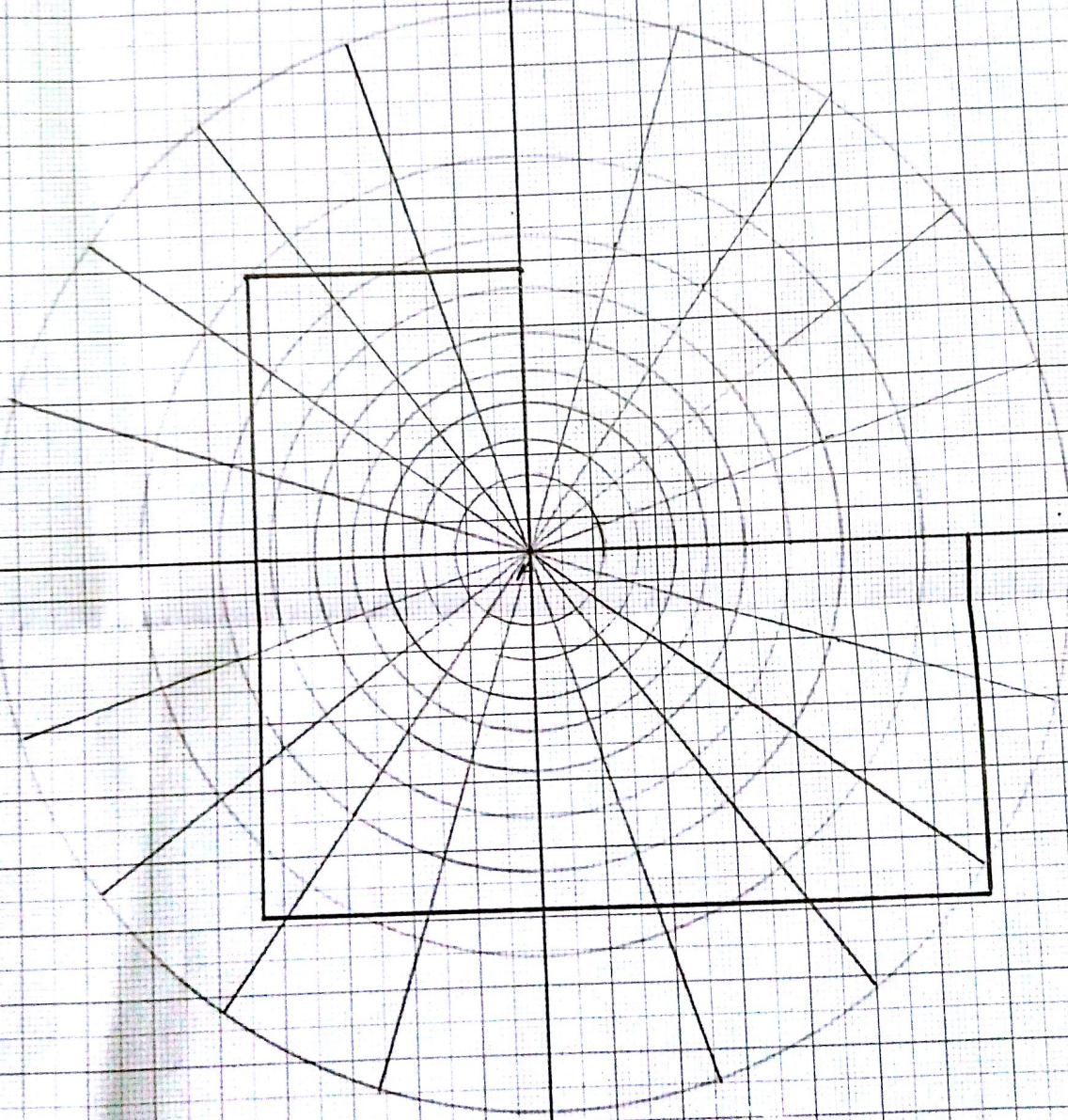
$$P_{a3}(3) = 4.8$$



Calculate the active thrust  $\rightarrow$   $\Delta$  ~~water~~

calculate the total thrust  $\rightarrow$   $\Delta$  ~~water~~ +  $H_2O$  pressure  $\Delta$

$$z = 1.75''$$
$$\text{Influence factor} = \frac{1}{200}$$



$$\sigma_z' = \frac{1}{200} \times 110 \times q$$

plotting wrong cause I took the wrong scale, but procedure for work,