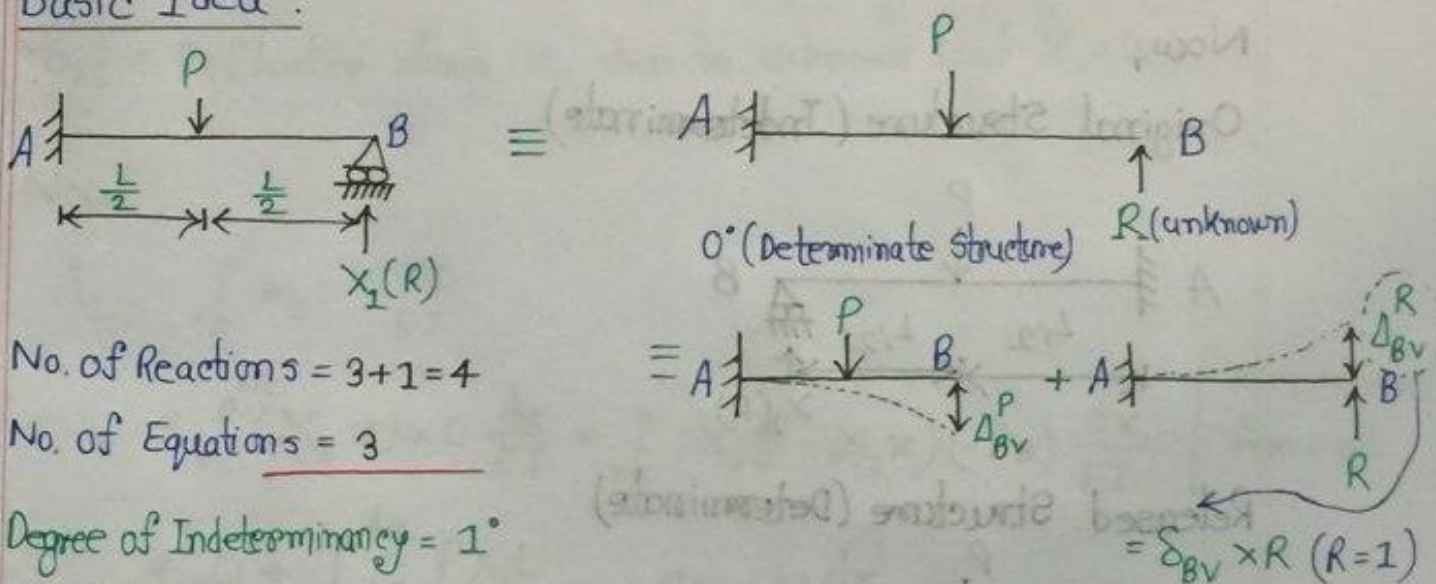


"Method of Consistent Deformation or Deflection Supervision
or Force or Flexibility Method"

Advantages of Flexibility Method:

- Accurate method for analysis of Indeterminate Structures
- Suitable for analysis of any structure
- Suitable for computerized approach

Basic Idea:



No. of Reactions = 3 + 1 = 4

No. of Equations = 3

Degree of Indeterminacy = 1

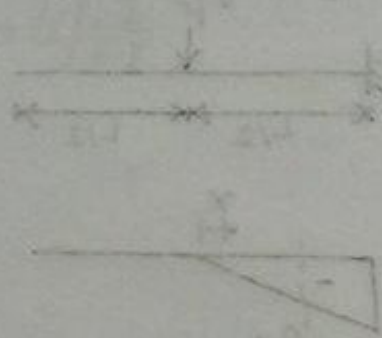
Here, Δ_{BV}^P = Vertical deflection due to External Load in Released Structure

Δ_{BV}^R = Vertical deflection due to R = 1 in Released or Determinate Structure

By unit load method,

$$\Delta_{BV}^P = \int_0^L m_0 m_1 \frac{dx}{EI}$$

$$\Delta_{BV}^R = \int_0^L m_1 m_1 \frac{dx}{EI}$$



In this example,

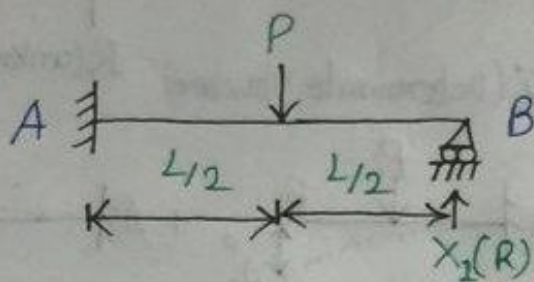
$$\Delta_{BV} = \Delta_{BV}^P + \Delta_{BV}^R$$

$$\Rightarrow 0 = \Delta_{BV}^P + \delta_{BV}^R \times R \quad [\because \text{Deflection at B (roller support) is 0}]$$

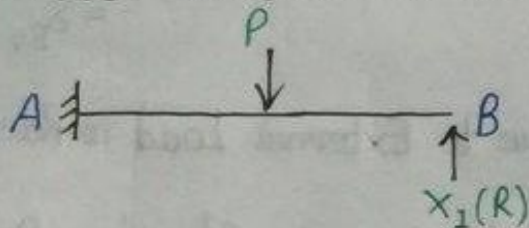
$$\therefore R = -\frac{\Delta_{BV}^P}{\delta_{BV}^R}$$

Now,

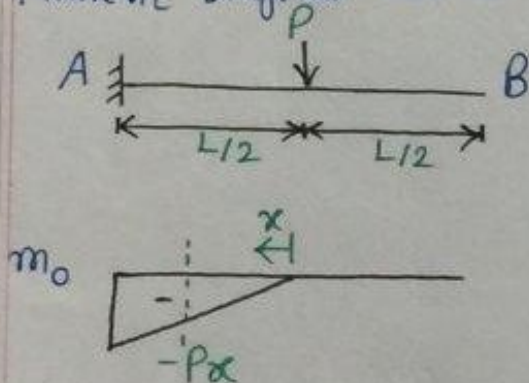
Original Structure (Indeterminate)



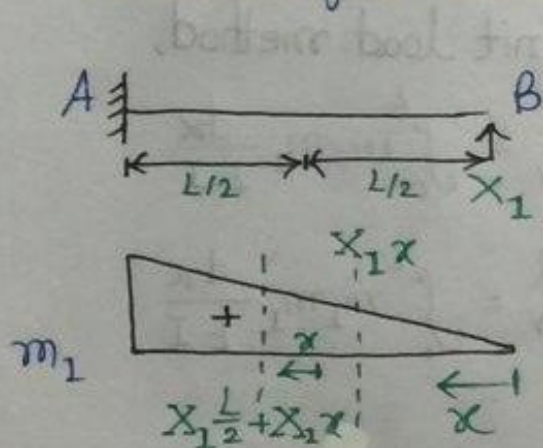
Released Structure (Determinate)



Moment Diagram Due to P



Moment Diagram Due to X_1



At B,

$$\Delta_{BV} = \Delta_{BV}^P + \delta_{BV}^R \times R$$

$$\text{or, } \Delta_1 = \Delta_{10} + \delta_{11} \times X_1$$

where,

Δ_{10} = Deflection along X_1 due to original load X_0

δ_{11} = Deflection along X_1 due to unknown load $X_1=1$

Now,

$$\Delta_{10} = \int_0^L m_1 m_0 \frac{dx}{EI}$$

$$= \int_0^{L/2} (X_1 \cdot x) \times 0 \frac{dx}{EI} + \int_0^{L/2} \left(X_1 \frac{L}{2} + X_1 x \right) (-Px) \frac{dx}{EI}$$

x is measured from right

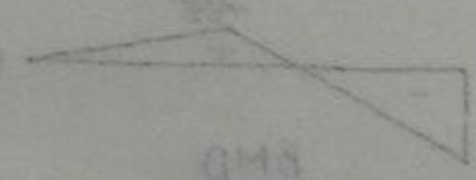
$$= 0 + \int_0^{L/2} \left(-\frac{PX_1 L}{2} x - PX_1 x^2 \right) \frac{dx}{EI}$$

$$= \left[-\frac{PL}{2} \cdot \frac{x^2}{2} - P \cdot \frac{x^3}{3} \right]_0^{L/2} \frac{1}{EI} \quad [\because X_1=1]$$

$$= \left[-\frac{PL}{4} \cdot \left(\frac{L}{2}\right)^2 - \frac{P}{3} \cdot \left(\frac{L}{2}\right)^3 + 0 + 0 \right] \frac{1}{EI}$$

$$= \left[-\frac{PL^3}{16} - \frac{PL^3}{24} \right] \frac{1}{EI}$$

$$= -\frac{5PL^3}{48EI}$$



$$\delta_{11} = \int_0^L m_1 m_1 \frac{dx}{EI}$$

$$= \int_0^L (X_1 \cdot x) (X_1 \cdot x) \frac{dx}{EI}$$

$$= \int_0^L X_1^2 x^2 \frac{dx}{EI}$$

$$= \left[\frac{x^3}{3} \right]_0^L \frac{1}{EI}$$

$$= \frac{L^3}{3EI}$$

$$[\because X_1 = 1]$$

Now, $X_1 = - \frac{\Delta_{10}}{\delta_{11}}$

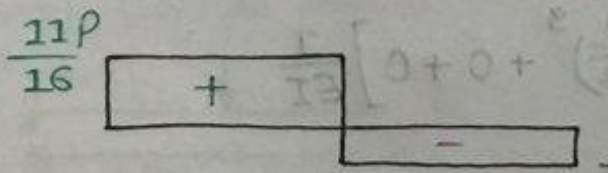
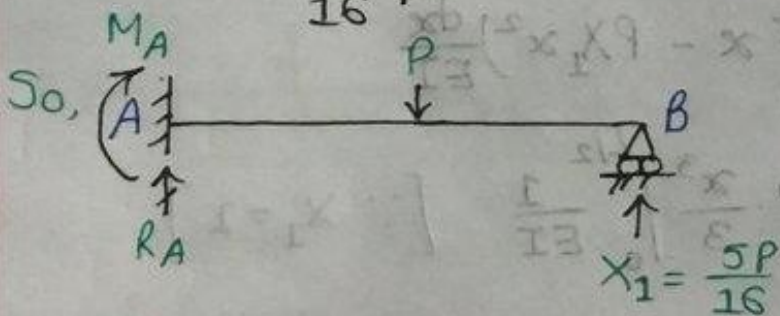
$$= - \frac{\left(- \frac{5PL^3}{48EI} \right)}{\frac{L^3}{3EI}}$$

$$= \frac{5}{16} P$$

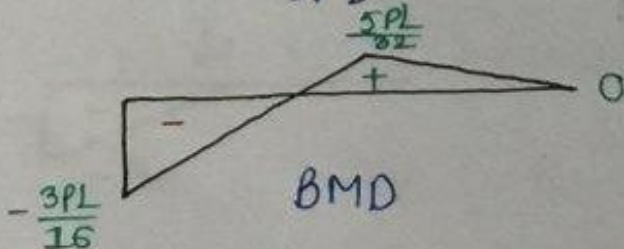
$$R_A = P - \frac{5P}{16} = \frac{11P}{16}$$

$$M_A = \frac{5P}{16} \times L - P \cdot \frac{L}{2}$$

$$= - \frac{3PL}{16}$$



SFD



BMD

Solution Steps:

- ① Find Degree of Indeterminacy = D°
- ② Select Redundant Forces equal to a number of D° and release the structure
- ② Find equations.

General Equation,

$$(\Delta_i) = (0) = (\Delta_{i0}) + (\delta_{ij})(X_j) \quad \text{where } i=j=D^\circ$$

Find Δ & δ terms by unit load method

Example: For 1°

$$(\Delta_1) = (\Delta_{10}) + (\delta_{11})(X_1)$$

For 2°

$$\begin{pmatrix} \Delta_1 \\ \Delta_2 \end{pmatrix} = \begin{pmatrix} \Delta_{10} \\ \Delta_{20} \end{pmatrix} + \begin{pmatrix} \delta_{11} & \delta_{12} \\ \delta_{21} & \delta_{22} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}$$

Remember: $\delta_{12} = \delta_{21}$; $\delta_{13} = \delta_{31} \dots \dots \dots$

For a Beam or Frame (Bending Members):

- ③ Draw m_0 diagram (Bending Moment diagram of Determinate structure for external load)
- ④ Draw m_1, m_2, m_3, \dots diagrams
(m_i diagram is the Bending Moment diagram of Determinate structure due to $X_i = 1$)
- ⑤ Find $\Delta_{i0} = \int m_0 m_i \frac{dx}{EI}$
- ⑥ Find $\delta_{ij} = \int m_i m_j \frac{dx}{EI}$
- ⑦ Solve for X_1, X_2, X_3 etc
- ⑧ Draw SFD, BMD for actual structure

For a Truss (Axial Members):

- ③ Find n_0 forces due to external loads
- ④ Find n_1, n_2, n_3, \dots etc forces due to $X_1 = 1, X_2 = 1, X_3 = 1, \dots$ etc loads.

⑤ Find $\Delta_{i_0} = \sum n_0 n_i \frac{L}{AE}$

⑥ Find $\delta_{ij} = \sum n_i n_j \frac{L}{AE}$

⑦ Solve for X_1, X_2, X_3, \dots etc

⑧ Find Bar Forces in actual truss

Summary of Solution Steps: With No Support Settlement

PART - 1 (Common for all structures)

Degree of Indeterminacy,

For Beams = No. of Reactions - No. of Eqⁿs - No. of Internal Hinges

For Frames = No. of Reactions + 3 × No. of Members - 3 × No. of Joints
- No. of Internal Hinges

For Trusses = No. of Bars + No. of Reactions - 2 × No. of Joints

General Equation,

$$(\Delta_i) = (0) = (\Delta_{i_0}) + (\delta_{ij})(X_j) \text{ for } i = j = \text{No. of Indeterminacy}$$

PART-2:

(a) For Beam & Frame (Bending Only)

$$\Delta_{io} = \int_0^L \frac{m_o m_i}{EI} dx \quad \dots \dots \dots (A1)$$

$$\delta_{ij} = \int_0^L \frac{m_i m_j}{EI} dx = \delta_{ji} \quad \dots \dots \dots (A2)$$

(b) For Truss (Axial Only)

$$\Delta_{io} = \sum \frac{n_o n_i L}{AE} + \sum n_i \alpha (\Delta T) L + \sum n_i (dL) \quad \dots \dots \dots (B1)$$

External Load Temperature Change Misfit

$$\delta_{ij} = \sum \frac{n_i n_j L}{AE} = \delta_{ji} \quad \dots \dots \dots (B2)$$

(c) For Beam & Frame (Bending & Axial)

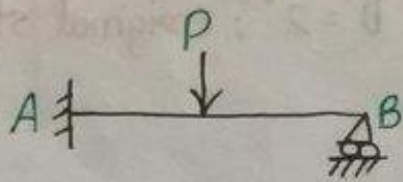
$$\Delta_{io} = A_1 + B_1$$

$$\delta_{ij} = A_2 + B_2$$

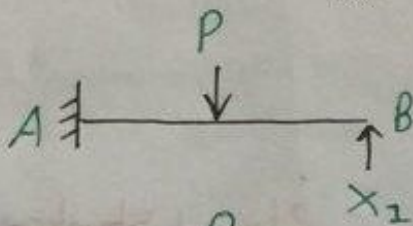
- **Misfit of truss** means the use of short or long members due to construction difficulties.

"Different Forms of Released (Primary) Structures & Redundants"

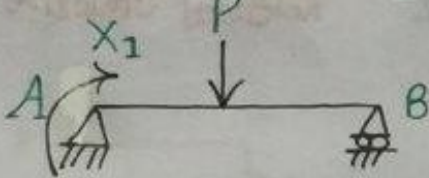
①



$D^{\circ} = 1^{\circ}$; original structure

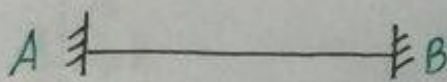


Released structure - 1

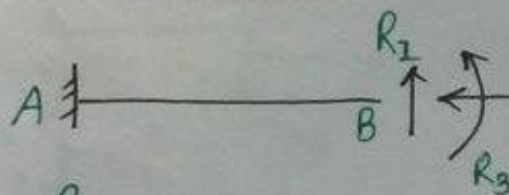


Released structure - 2

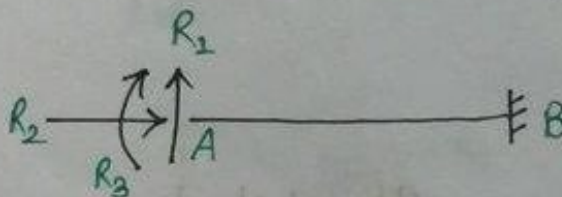
②



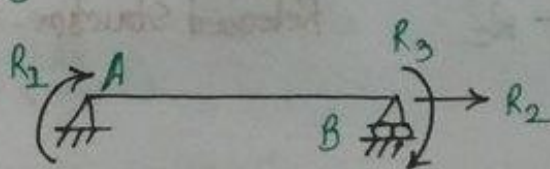
$D^{\circ} = 3^{\circ}$; original structure



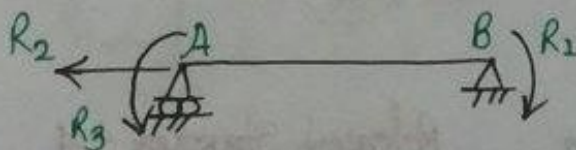
Released structure - 1



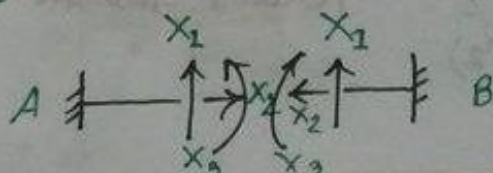
Released structure - 2



Released structure - 3

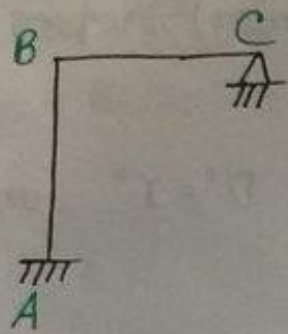


Released structure - 4

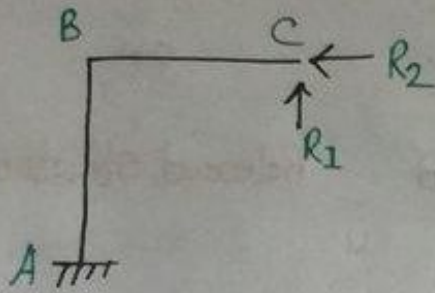


Released structure - 5

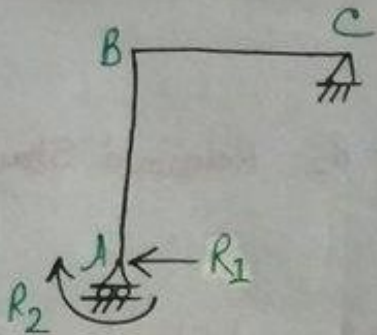
3



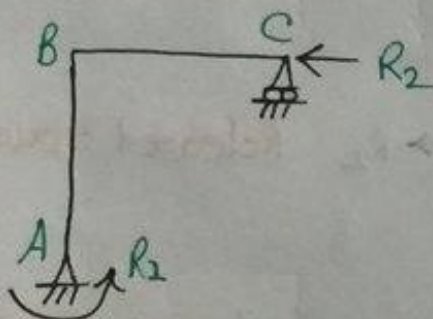
$\theta = 2^\circ$; original structure



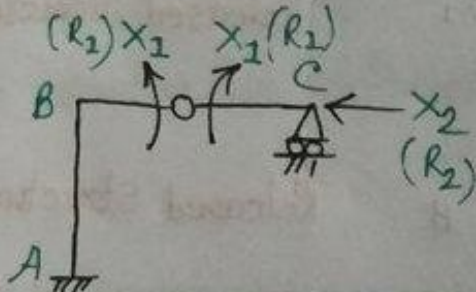
Released structure - 1



Released structure - 2

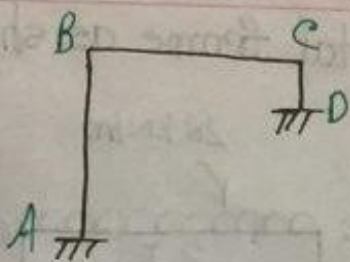


Released structure - 3

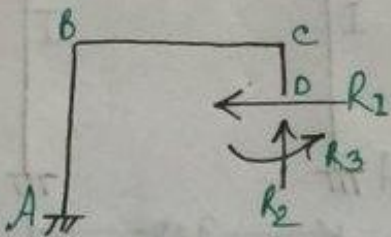


Released structure - 4

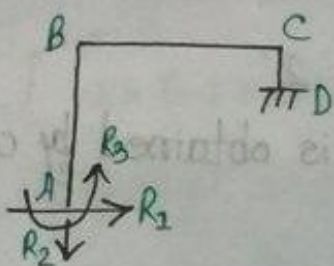
4



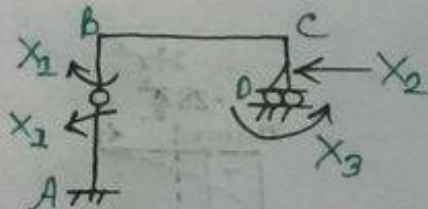
$D^0 = 3^0$; original structure



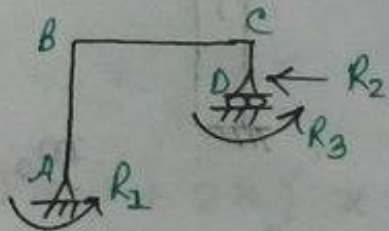
Released Structure - 1



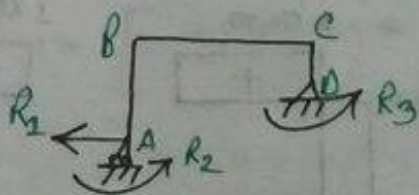
Released Structure - 2



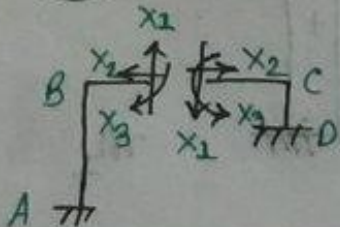
Released Structure - 3



Released Structure - 4



Released structure - 5



Released Structure - 6

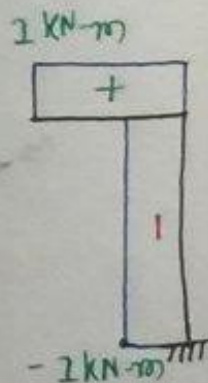
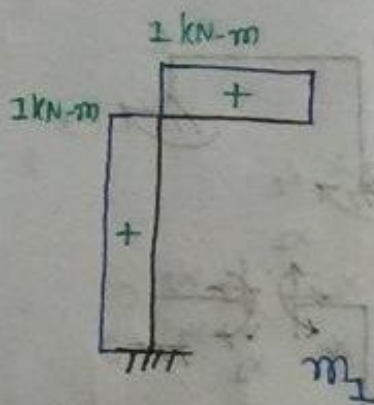
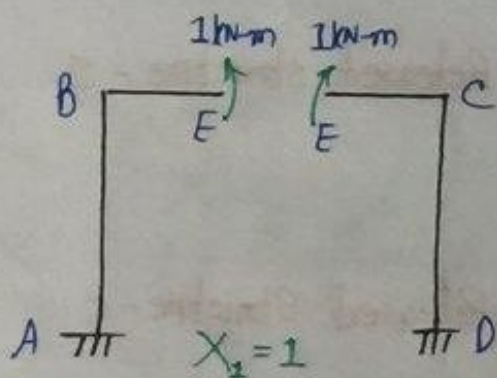
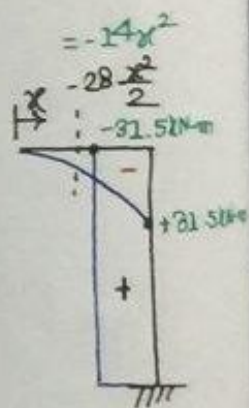
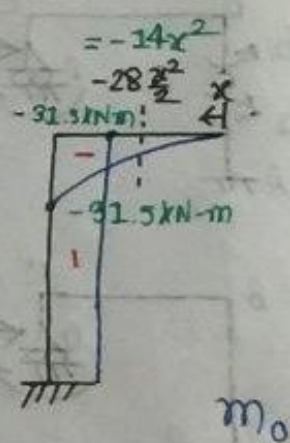
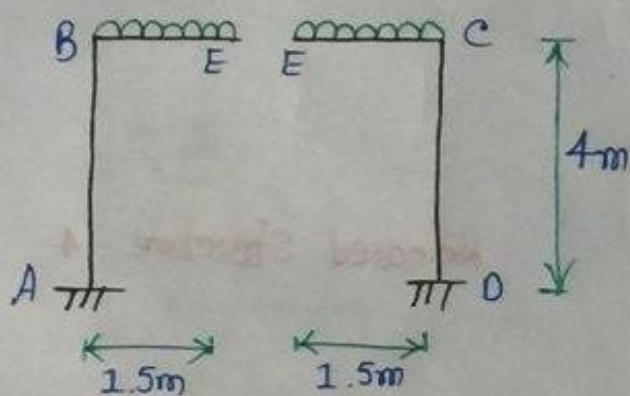
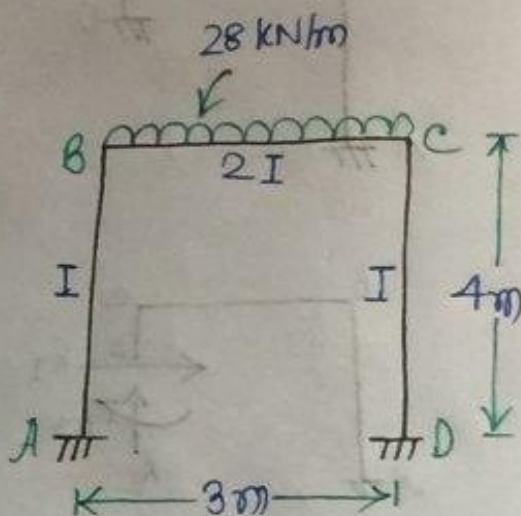
FRAME-1: Analyze the portal frame as shown by the force method.

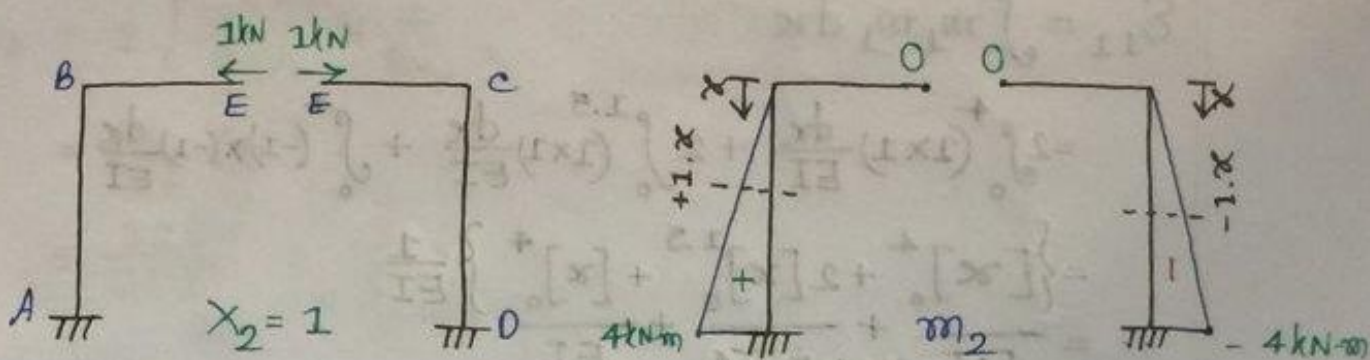
Solⁿ: Due to symmetry of the frame and loading, the shear force at the middle point of BC is zero.

Here, $D^{\circ} = (3+3) - 3$
 $= 3^{\circ}$

but due to symmetry, $D^{\circ} = 3 - 1 = 2^{\circ}$

The basic determinate structure is obtained by applying a cut at the middle of BC.





Here,

$$\Delta_{10} = \int m_1 m_0 \frac{dx}{EI}$$

$$= 2 \int_0^{1.5} 1 \times (-14x^2) \frac{dx}{EI} + \int_0^4 1 \times (-31.5) \frac{dx}{EI} + \int_0^4 (-1) \times (31.5) \frac{dx}{EI}$$

$$= 2 \times \left[\left(\frac{-14x^3}{3 \times 2EI} \right) \right]_0^{1.5} + 2 \times \left[-\frac{31.5x}{EI} \right]_0^4$$

$$= 2 \times \left[\frac{-14(1.5)^3}{3 \times 2EI} \right] + 2 \times \left[\frac{-31.5 \times 4}{EI} \right]$$

$$= -\frac{267.75}{EI}$$

$$\Delta_{20} = \int m_2 m_0 \frac{dx}{EI}$$

$$= 0 + 0 + 2 \times \int_0^4 x \times (-31.5) \frac{dx}{EI}$$

$$= 2 \times \left[-\frac{31.5x^2}{2EI} \right]_0^4$$

$$= 2 \times \left[\frac{-31.5 \times (4)^2}{2EI} \right]$$

$$= -\frac{504}{EI}$$

$$\delta_{11} = \int m_1 m_1 dx$$

$$= \int_0^4 (1 \times 1) \frac{dx}{EI} + 2 \int_0^{1.5} (1 \times 1) \frac{dx}{EI} + \int_0^4 (-1) \times (-1) \frac{dx}{EI}$$

$$= \frac{[x]_0^4}{EI} + \frac{2[x]_0^{1.5}}{2EI} + \frac{[x]_0^4}{EI}$$

$$= \frac{4}{EI} + \frac{2 \times 1.5}{2EI} + \frac{4}{EI}$$

$$= \frac{9.5}{EI}$$

$$\delta_{12} = \delta_{21} = \int m_1 m_2 dx$$

$$= \int_0^4 1 \times (x) \frac{dx}{EI} + 0 + 0 + \int_0^4 (-1) \times (x) \frac{dx}{EI}$$

$$= 2 \times \int_0^4 x \frac{dx}{EI}$$

$$= 2 \times \left[\frac{x^2}{2} \right]_0^4 \times \frac{1}{EI}$$

$$= 2 \times \frac{(4)^2}{2} \times \frac{1}{EI}$$

$$= \frac{16}{EI}$$

$$\delta_{22} = \int m_2 m_2 \frac{dx}{EI}$$

$$= \int_0^4 (x \times x) \frac{dx}{EI} + 0 + 0 + \int_0^4 (-x) \times (-x) \frac{dx}{EI}$$

$$= 2 \int_0^4 x^2 \frac{dx}{EI}$$

$$\begin{aligned}\delta_{22} &= 2 \left[\frac{x^3}{3} \right]_0^4 \times \frac{1}{EI} \\ &= \frac{2}{3EI} \times (4)^3 \\ &= \frac{128}{3EI}\end{aligned}$$

Now,

$$\begin{pmatrix} \Delta_1 \\ \Delta_2 \end{pmatrix} = \begin{pmatrix} \Delta_{10} \\ \Delta_{20} \end{pmatrix} + \begin{pmatrix} \delta_{11} & \delta_{12} \\ \delta_{21} & \delta_{22} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}$$

or,

$$\Delta_1 = \Delta_{10} + \delta_{11} X_1 + \delta_{12} X_2$$

$$\Rightarrow 0 = -\frac{267.75}{EI} + \frac{9.5}{EI} X_1 + \frac{16}{EI} X_2$$

$$\therefore 9.5 X_1 + 16 X_2 = 267.75 \quad \text{①}$$

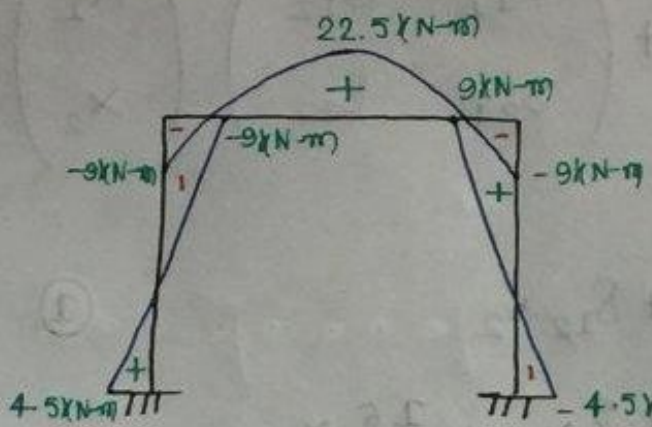
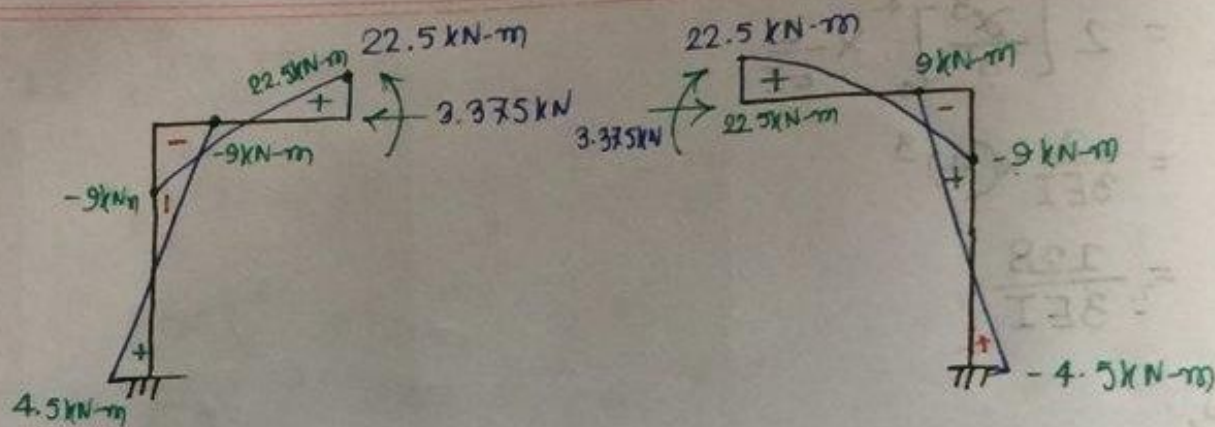
$$\Delta_2 = \Delta_{20} + \delta_{21} X_1 + \delta_{22} X_2$$

$$\Rightarrow 0 = -\frac{504}{EI} + \frac{16}{EI} X_1 + \frac{128}{3EI} X_2$$

$$\Rightarrow 16 X_1 + \frac{128}{3} X_2 = 504 \quad \text{②}$$

By solving eqⁿ ① & ② we get,

$$X_1 = 22.5 \text{ kN} \quad \& \quad X_2 = 3.375 \text{ kN} \quad (\text{Ans:})$$



Final BMD

$$\Rightarrow 0 = -\frac{204}{EI} + \frac{16}{EI} X_1 + \frac{159}{3EI} X_2$$

$$\Rightarrow 16 X_1 + 159 X_2 = 204$$

By solving eqn (1) & (2) we get

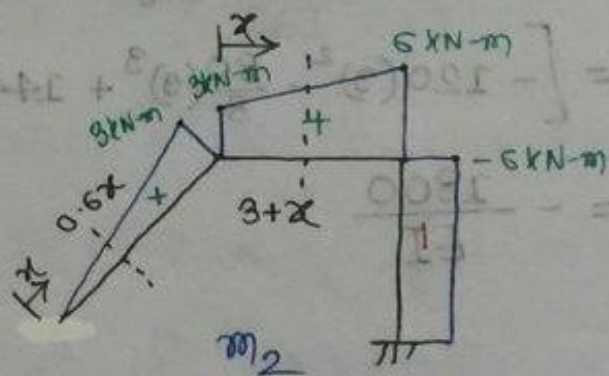
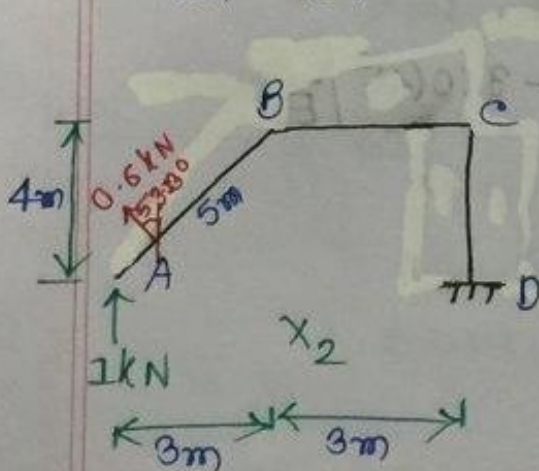
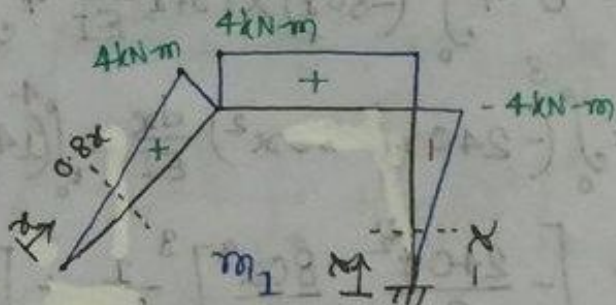
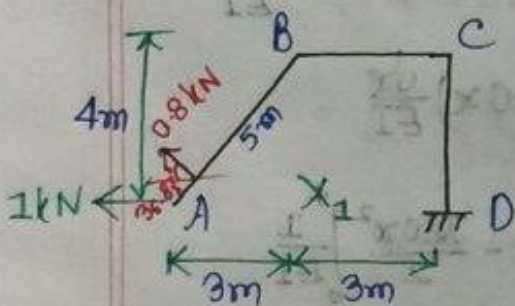
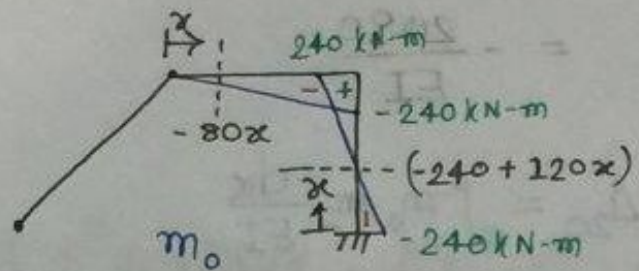
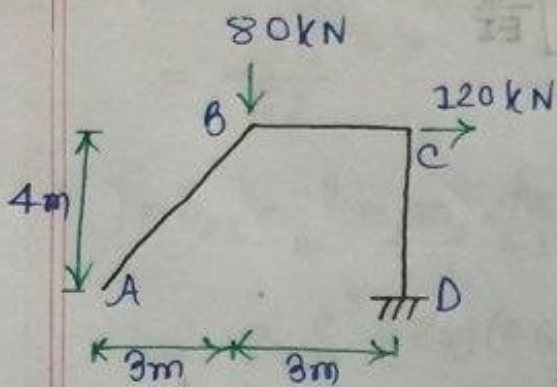
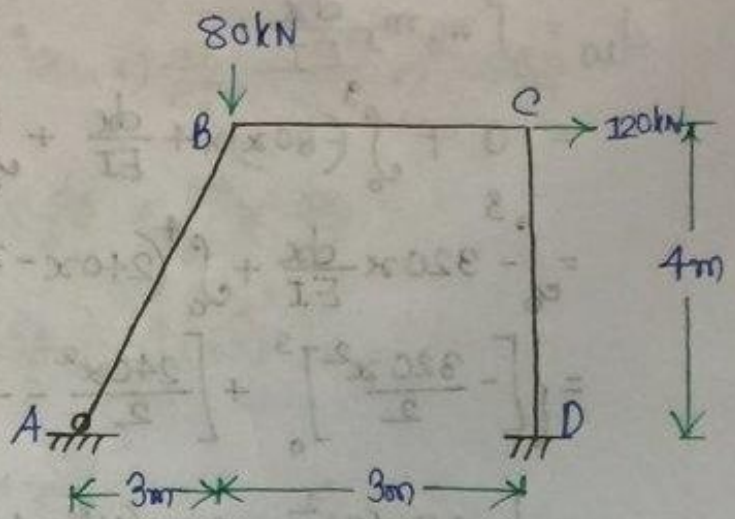
$$X_1 = 22.5 \text{ kN} \cdot \text{m}$$

FRAME-2: Analyze the inclined leg portal frame as shown by the force method.

Solⁿ: Here,

$$D^{\circ} = (2+3) + (3 \times 3) - (4 \times 3) = 2^{\circ}$$

Release the Hinge support



Here,

$$\begin{aligned}\Delta_{10} &= \int m_0 m_1 \frac{dx}{EI} \\ &= 0 + \int_0^3 (-80x) \times 4 \frac{dx}{EI} + \int_0^4 (-240 + 120x) \times (-x) \frac{dx}{EI} \\ &= \int_0^3 -320x \frac{dx}{EI} + \int_0^4 (240x - 120x^2) \frac{dx}{EI} \\ &= \left\{ \left[-\frac{320x^2}{2} \right]_0^3 + \left[\frac{240x^2}{2} - \frac{120x^3}{3} \right]_0^4 \right\} \frac{1}{EI} \\ &= \left[-160(3)^2 + 120(4)^2 - 40(4)^3 \right] \frac{1}{EI} \\ &= -\frac{2080}{EI}\end{aligned}$$

$$\begin{aligned}\Delta_{20} &= \int m_0 m_2 \frac{dx}{EI} \\ &= 0 + \int_0^3 (-80x) \times (3+x) \frac{dx}{EI} + \int_0^4 (-240 + 120x) \times (-6) \frac{dx}{EI} \\ &= \int_0^3 (-240x - 80x^2) \frac{dx}{EI} + \int_0^4 (1440 - 720x) \frac{dx}{EI} \\ &= \left[-\frac{240x^2}{2} - \frac{80x^3}{3} \right]_0^3 \frac{1}{EI} + \left[1440x - \frac{720x^2}{2} \right]_0^4 \frac{1}{EI} \\ &= \left[-120(3)^2 - \frac{80}{3}(3)^3 + 1440(4) - 360(4)^2 \right] \frac{1}{EI} \\ &= -\frac{1800}{EI}\end{aligned}$$

$$\delta_{11} = \int m_1 m_1 \frac{dx}{EI}$$

$$= \int_0^5 (0.8x)(0.8x) \frac{dx}{EI} + \int_0^3 (4 \times 4) \frac{dx}{EI} + \int_0^4 (-x)(-x) \frac{dx}{EI}$$

$$= \int_0^5 0.64x^2 \frac{dx}{EI} + \int_0^3 16 \frac{dx}{EI} + \int_0^4 x^2 \frac{dx}{EI}$$

$$= \left[\frac{0.64x^3}{3} \right]_0^5 \frac{1}{EI} + \left[\frac{16x}{EI} \right]_0^3 + \left[\frac{x^3}{3EI} \right]_0^4$$

$$= \frac{0.64(5)^3}{3EI} + \frac{16(3)}{EI} + \frac{(4)^3}{3EI}$$

$$= \frac{96}{EI}$$

$$\delta_{12} = \delta_{21} = \int m_1 m_2 \frac{dx}{EI}$$

$$= \int_0^5 (0.8x)(0.6x) \frac{dx}{EI} + \int_0^3 4(3+x) \frac{dx}{EI} + \int_0^4 (-x)(-6) \frac{dx}{EI}$$

$$= \int_0^5 0.48x^2 \frac{dx}{EI} + \int_0^3 (12+4x) \frac{dx}{EI} + \int_0^4 6x \frac{dx}{EI}$$

$$= \left[\frac{0.48x^3}{3EI} \right]_0^5 + \left[\frac{12x + \frac{4x^2}{2}}{EI} \right]_0^3 + \left[\frac{6x^2}{2EI} \right]_0^4$$

$$= \frac{0.48(5)^3}{3EI} + \frac{12(3) + 2(3)^2}{EI} + \frac{6(4)^2}{2EI}$$

$$= \frac{122}{EI}$$

$$\begin{aligned}
\delta_{22} &= \int m_2 m_2 \frac{dx}{EI} \\
&= \int_0^5 (0.6x)(0.6x) \frac{dx}{EI} + \int_0^3 (3+x)(3+x) \frac{dx}{EI} + \int_0^4 (-6)(-6) \frac{dx}{EI} \\
&= \int_0^5 0.36x^2 \frac{dx}{EI} + \int_0^3 (9+6x+x^2) \frac{dx}{EI} + \int_0^4 36 \frac{dx}{EI} \\
&= \left[\frac{0.36x^3}{3EI} \right]_0^5 + \left[\frac{9x + \frac{6x^2}{2} + \frac{x^3}{3}}{EI} \right]_0^3 + \left[\frac{36x}{EI} \right]_0^4 \\
&= \frac{0.36(5)^3}{3EI} + \frac{9(3) + 3(3)^2 + \frac{(3)^3}{3}}{EI} + \frac{36(4)}{EI} \\
&= \frac{222}{EI}
\end{aligned}$$

Now,

$$\Delta_1 = \Delta_{10} + \delta_{11} X_1 + \delta_{12} X_2$$

$$\Rightarrow 0 = -\frac{2080}{EI} + \frac{96}{EI} X_1 + \frac{122}{EI} X_2$$

$$\Rightarrow 96 X_1 + 122 X_2 = 2080 \quad \text{①}$$

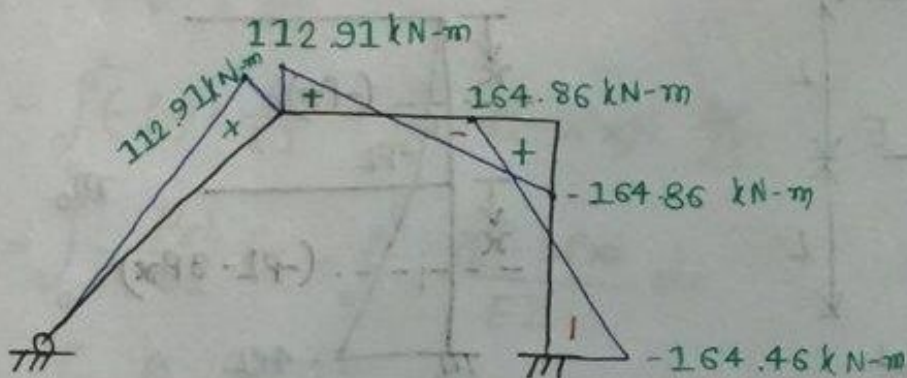
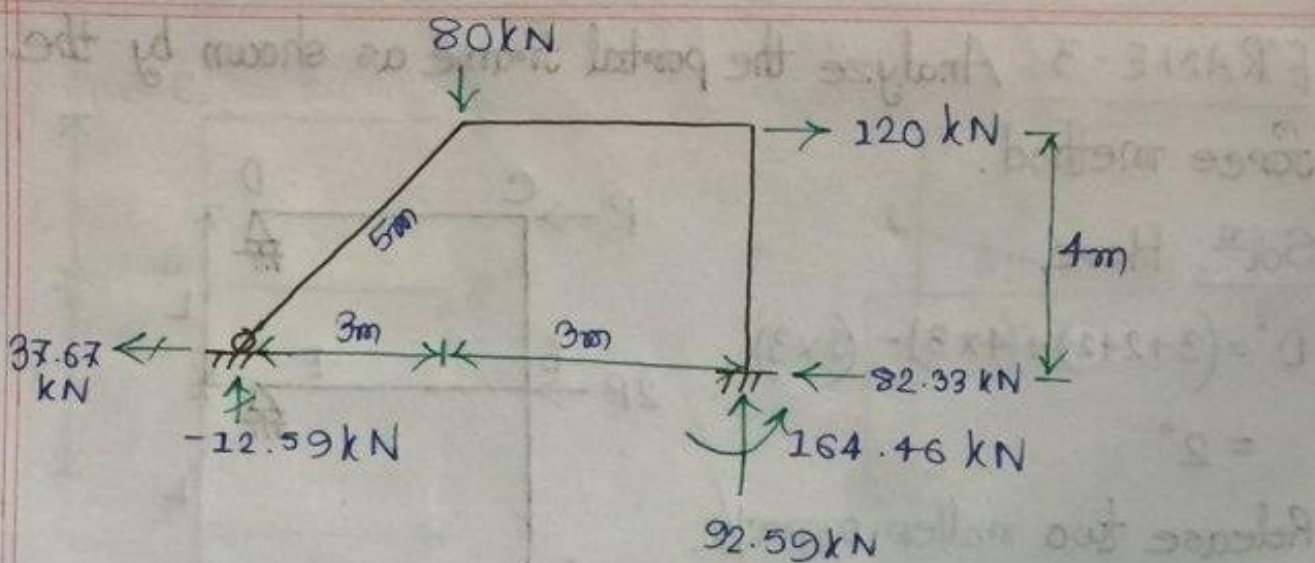
$$\Delta_2 = \Delta_{20} + \delta_{21} X_1 + \delta_{22} X_2$$

$$\Rightarrow 0 = -\frac{1800}{EI} + \frac{1}{EI} X_1 + \frac{222}{EI} X_2$$

$$\Rightarrow X_1 + 222 X_2 = 1800 \quad \text{②}$$

By solving eqⁿ ① & ② we get,

$$X_1 = 37.67 \text{ kN} \quad \& \quad X_2 = -12.59 \text{ kN} \quad (\text{Ans.})$$



Final BMD

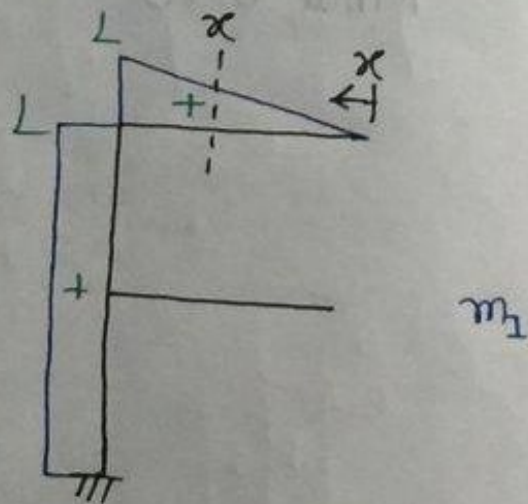
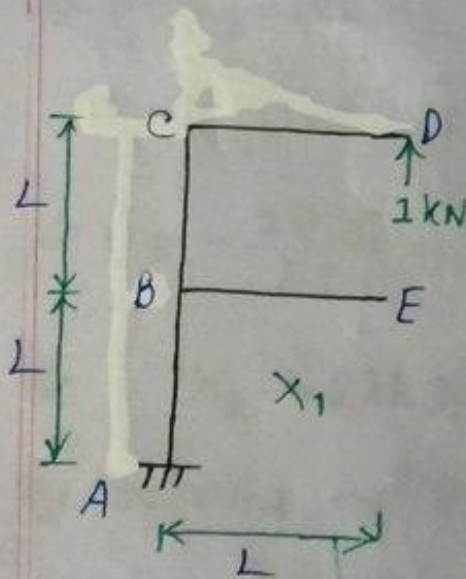
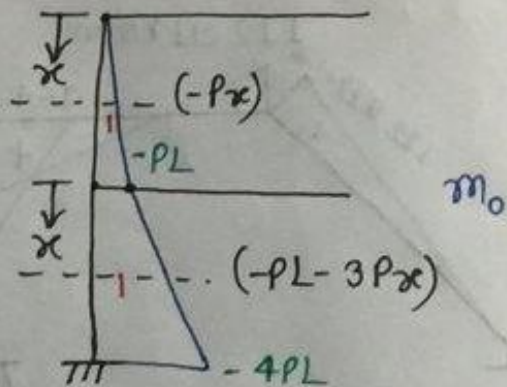
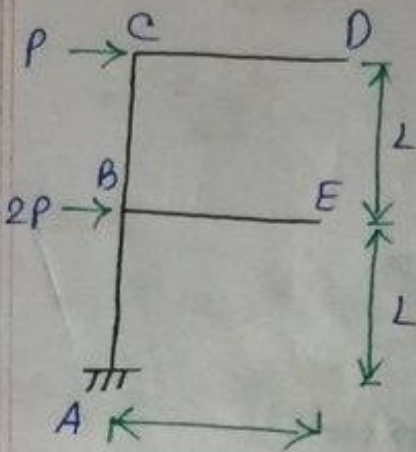
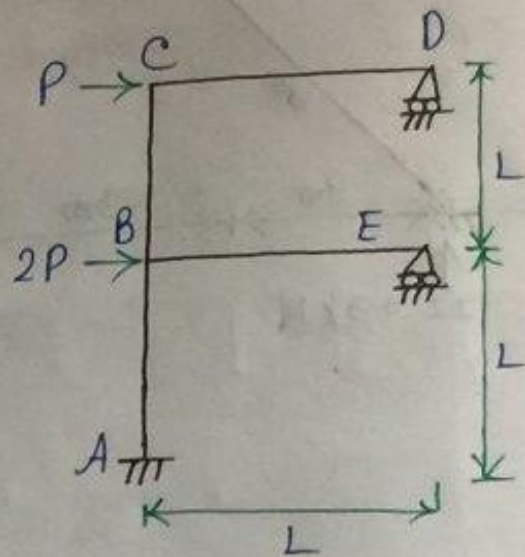
FRAME-3: Analyze the portal frame as shown by the force method.

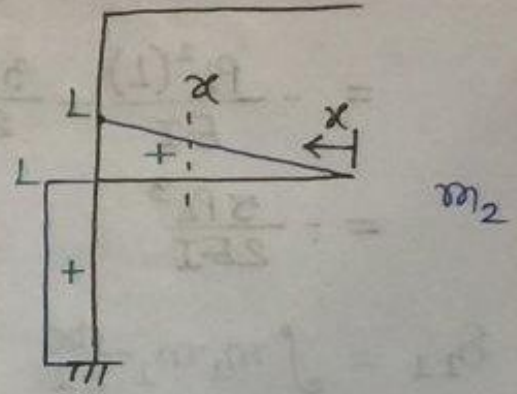
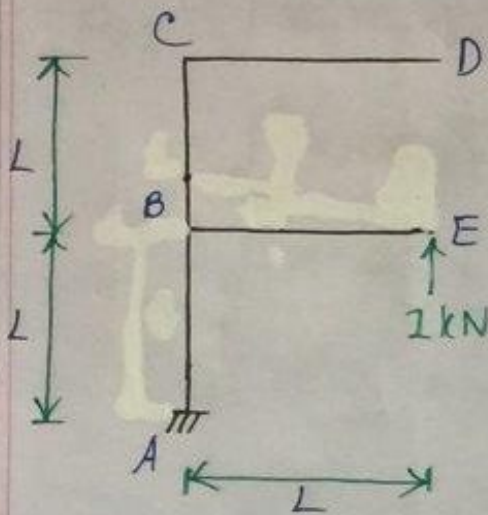
Solⁿ: Here,

$$D^{\circ} = (3+1+1) + (4 \times 3) - (5 \times 3)$$

$$= 2^{\circ}$$

Release two roller supports.





Here,

$$\Delta_{10} = \int m_0 m_1 \frac{dx}{EI}$$

$$= \int_0^L (-Px)L \frac{dx}{EI} + \int_0^L (-PL - 3Px)L \frac{dx}{EI}$$

$$= \int_0^L -\frac{PxL}{EI} dx + \int_0^L \frac{-PL^2 - 3P\alpha L}{EI} dx$$

$$= \left[-\frac{PL}{EI} \cdot \frac{x^2}{2} \right]_0^L + \left[\frac{-PL^2 x - \frac{3PLx^2}{2}}{EI} \right]_0^L$$

$$= -\frac{PL(L)^2}{2EI} + \frac{-PL^2(L) - \frac{3PL}{2}(L)^2}{EI}$$

$$= -\frac{3PL^3}{EI}$$

$$\Delta_{20} = \int m_0 m_2 \frac{dx}{EI}$$

$$= 0 + \int_0^L (-PL - 3Px)L \frac{dx}{EI}$$

$$= \int_0^L (-PL^2 - 3PLx) \frac{dx}{EI}$$

$$\Delta_{20} = \left[-\frac{PL^2x}{EI} - \frac{3PLx^2}{2EI} \right]_0^L$$

$$= -\frac{PL^2(L)}{EI} - \frac{3PL(L)^2}{2EI}$$

$$= -\frac{5PL^3}{2EI}$$

$$\delta_{11} = \int m_1 m_1 \frac{dx}{EI}$$

$$= \int_0^L (x)(x) \frac{dx}{EI} + \int_0^{2L} (L)(L) \frac{dx}{EI}$$

$$= \int_0^L x^2 \frac{dx}{EI} + \int_0^{2L} L^2 \frac{dx}{EI}$$

$$= \left\{ \left[\frac{x^3}{3} \right]_0^L + \left[L^2 x \right]_0^{2L} \right\} \frac{1}{EI}$$

$$= \frac{(L)^3}{3EI} + \frac{L^2(2L)}{EI}$$

$$= \frac{7L^3}{3EI}$$

$$\delta_{12} = \delta_{21} = \int m_1 m_2 \frac{dx}{EI}$$

$$= 0 + 0 + \int_0^L (L)(L) \frac{dx}{EI}$$

$$= \left[L^2 x \right]_0^L \frac{1}{EI}$$

$$= \frac{L^2(L)}{EI}$$

$$= \frac{L^3}{EI}$$

$$\begin{aligned}
 \delta_{22} &= \int m_2 m_2 \frac{dx}{EI} \\
 &= \int_0^L (x)(x) \frac{dx}{EI} + \int_0^L (L)(L) \frac{dx}{EI} \\
 &= \int_0^L x^2 \frac{dx}{EI} + \int_0^L L^2 \frac{dx}{EI} \\
 &= \left\{ \left[\frac{x^3}{3} \right]_0^L + \left[L^2 x \right]_0^L \right\} \frac{1}{EI} \\
 &= \frac{(L)^3}{3EI} + \frac{L^2(L)}{EI} \\
 &= \frac{4L^3}{3EI}
 \end{aligned}$$

Now,

$$\begin{aligned}
 \Delta_1 &= \Delta_{10} + \delta_{11} X_1 + \delta_{12} X_2 \\
 \Rightarrow 0 &= -\frac{3PL^3}{EI} + \frac{7L^3}{3EI} X_1 + \frac{L^3}{EI} X_2
 \end{aligned}$$

$$\therefore 7X_1 + 3X_2 = 9P \quad \text{①}$$

$$\Delta_2 = \Delta_{20} + \delta_{21} X_1 + \delta_{22} X_2$$

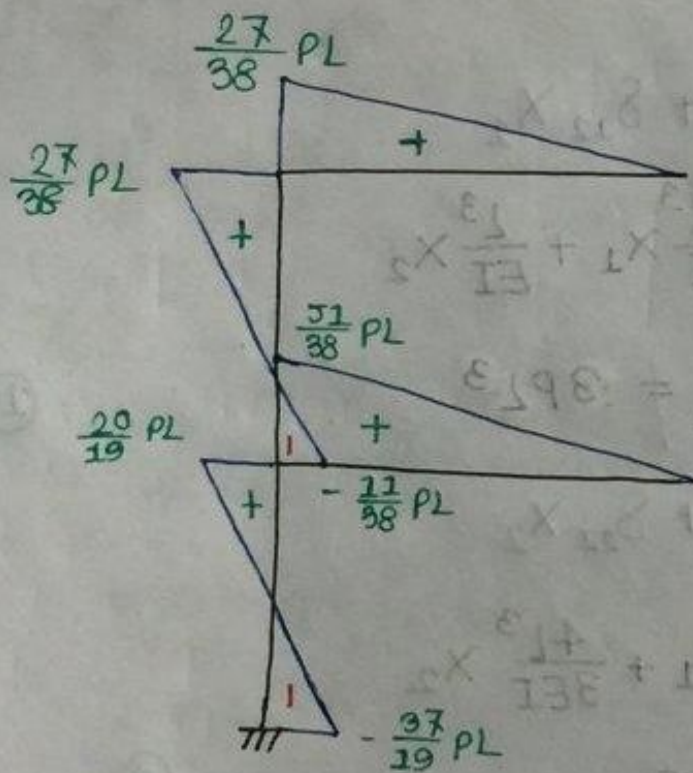
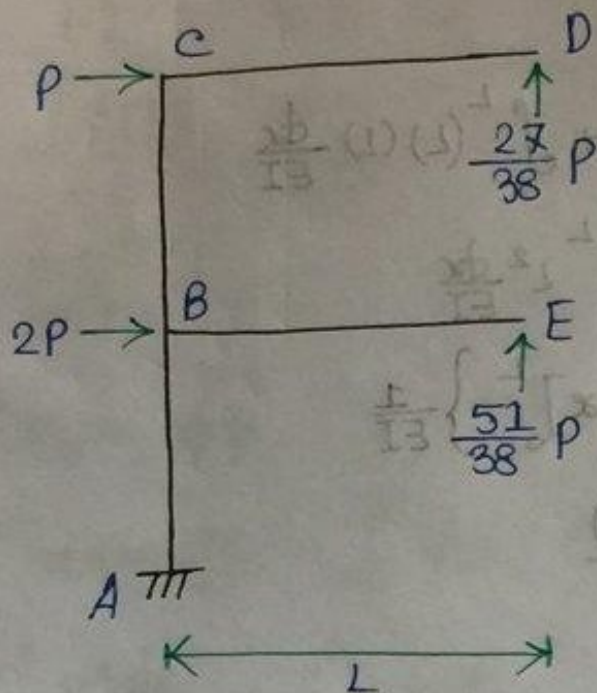
$$\Rightarrow 0 = -\frac{5PL^3}{2EI} + \frac{L^3}{EI} X_1 + \frac{4L^3}{3EI} X_2$$

$$\therefore 6X_1 + 8X_2 = 15P \quad \text{②}$$

By solving eqⁿ ① & ② we get,

$$X_1 = \frac{27}{38} P \quad \& \quad X_2 = \frac{51}{38} P$$

(Ans:)



Final BMD

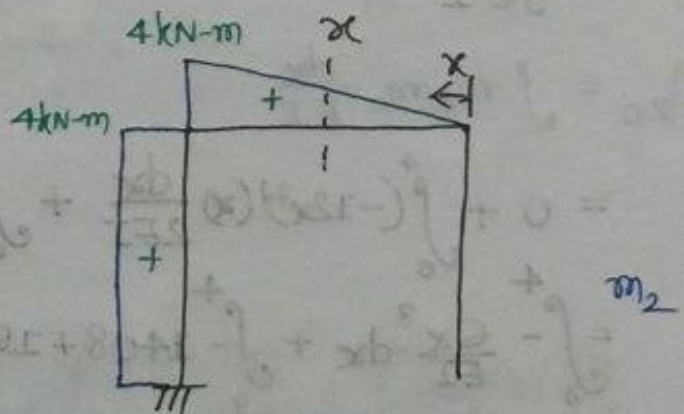
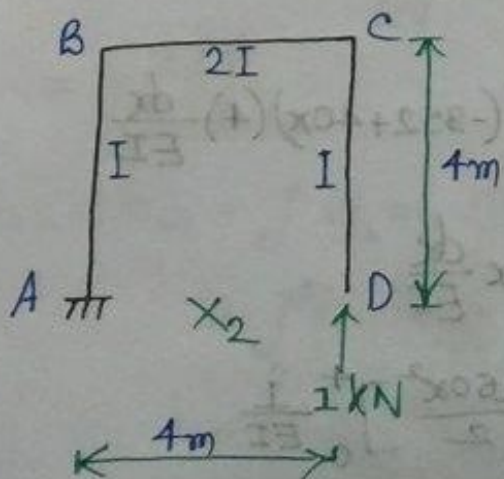
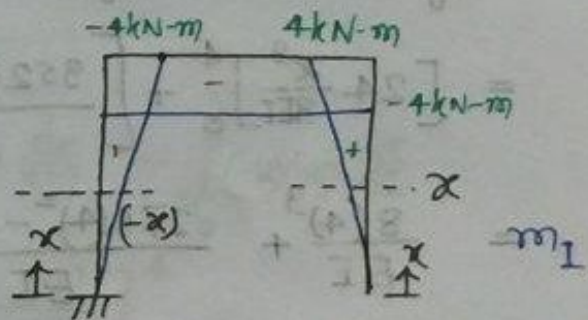
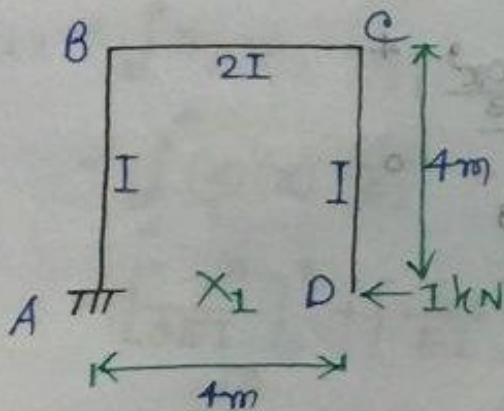
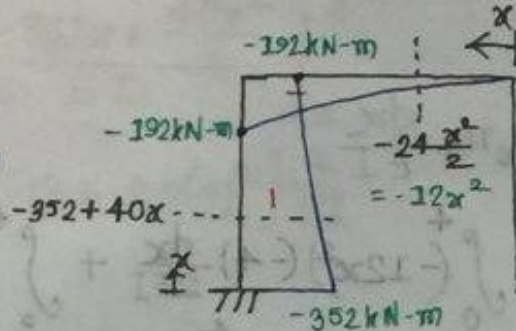
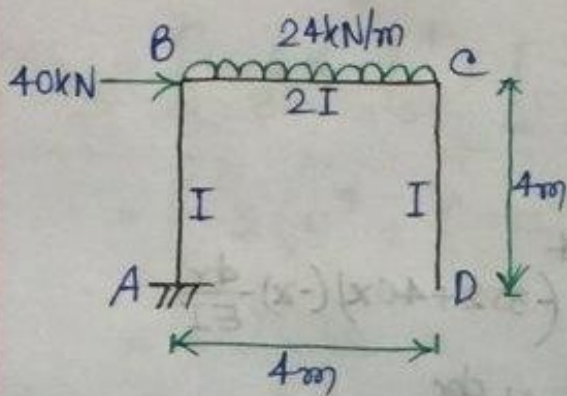
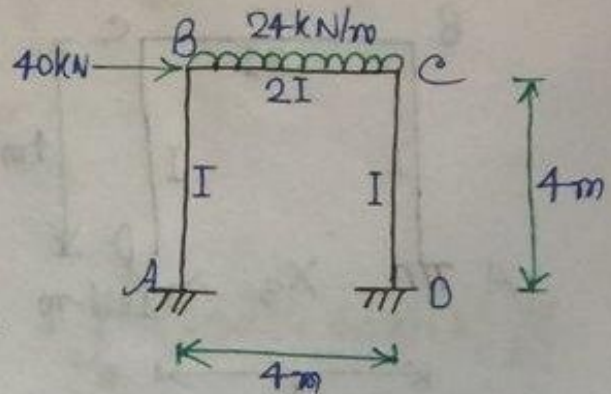
FRAME-4: Analyze the portal frame as shown by the force method.

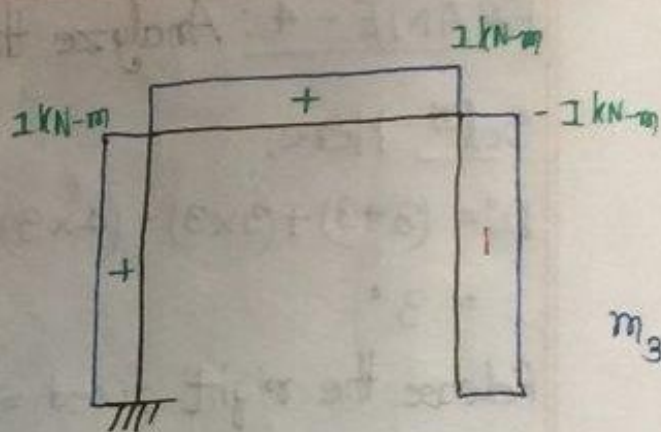
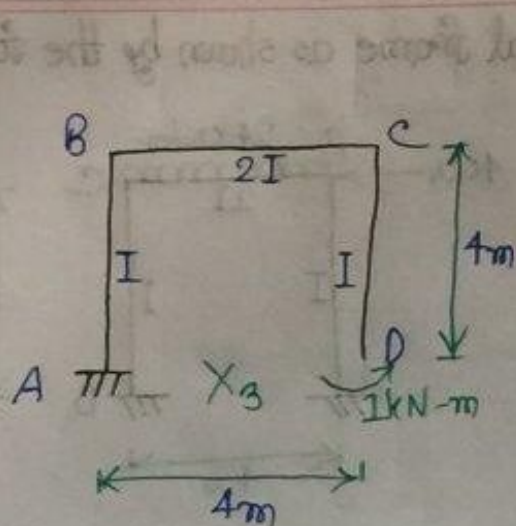
Solⁿ: Here,

$$D^{\circ} = (3+3) + (3 \times 3) - (4 \times 3)$$

$$= 3^{\circ}$$

Release the right fixed support.





Now,

$$\begin{aligned}
 \Delta_{10} &= \int m_0 m_3 \frac{dx}{EI} \\
 &= 0 + \int_0^4 (-12x^2)(-1) \frac{dx}{2EI} + \int_0^4 (-352 + 40x)(-x) \frac{dx}{EI} \\
 &= \int_0^4 48x^2 \frac{dx}{2EI} + \int_0^4 (352x - 40x^2) \frac{dx}{EI} \\
 &= \left[24 \frac{x^3}{3EI} \right]_0^4 + \left[\frac{352 \frac{x^2}{2} - \frac{40x^3}{3}}{EI} \right]_0^4 \\
 &= \frac{8(4)^3}{EI} + \frac{176(4)^2 - \frac{40}{3}(4)^3}{EI} \\
 &= \frac{7424}{3EI}
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{20} &= \int m_0 m_2 \frac{dx}{EI} \\
 &= 0 + \int_0^4 (-12x^2)(x) \frac{dx}{2EI} + \int_0^4 (-352 + 40x)(4) \frac{dx}{EI} \\
 &= \int_0^4 -\frac{6x^3}{EI} dx + \int_0^4 -1408 + 160x \frac{dx}{EI} \\
 &= \left[-\frac{6x^4}{4EI} \right]_0^4 + \left[-1408x + \frac{160x^2}{2} \right]_0^4 \frac{1}{EI}
 \end{aligned}$$

$$\Delta_{20} = -\frac{6(4)^4}{4EI} - \frac{1408(4)}{EI} + \frac{80(4)^2}{EI}$$

$$= -\frac{4736}{EI}$$

$$\Delta_{30} = \int m_0 m_3 \frac{dx}{EI}$$

$$= 0 + \int_0^4 (-12x^2)(1) \frac{dx}{2EI} + \int_0^4 (-352 + 40x)(1) \frac{dx}{EI}$$

$$= \left[-\frac{6x^3}{3EI} \right]_0^4 + \left[\frac{-352x + \frac{40x^2}{2}}{EI} \right]_0^4$$

$$= \left[-2(4)^3 + (-352)(4) + 20(4)^2 \right] \frac{1}{EI}$$

$$= -\frac{1216}{EI}$$

$$\delta_{11} = \int m_1 m_1 \frac{dx}{EI}$$

$$= \int_0^4 (x)(x) \frac{dx}{EI} + \int_0^4 (4)(4) \frac{dx}{2EI} + \int_0^4 (-x)(-x) \frac{dx}{EI}$$

$$= \left[\frac{x^3}{3EI} \right]_0^4 + \left[\frac{8x}{EI} \right]_0^4 + \left[\frac{x^3}{3EI} \right]_0^4$$

$$= \frac{\frac{(4)^3}{3} + 8(4) + \frac{(4)^3}{3}}{EI}$$

$$= \frac{224}{3EI}$$

$$\delta_{12} = \delta_{21} = \int m_1 m_2 \frac{dx}{EI}$$

$$= \int_0^4 (+x)0 \frac{dx}{EI} + \int_0^4 (-4)(x) \frac{dx}{2EI} + \int_0^4 (-x)(4) \frac{dx}{EI}$$

$$= 0 + \int_0^4 (-2x) \frac{dx}{EI} + \int_0^4 (-4x) \frac{dx}{EI}$$

$$\delta_{12} = \delta_{21} = \left[-\frac{2x^2}{2EI} \right]_0^4 + \left[\frac{-4x^2}{2EI} \right]_0^4$$

$$= -\frac{(4)^2}{EI} - \frac{2(4)^2}{EI}$$

$$= -\frac{48}{EI}$$

$$\delta_{13} = \delta_{31} = \int m_1 m_3 \frac{dx}{EI}$$

$$= \int_0^4 (+x)(-1) \frac{dx}{EI} + \int_0^4 (-4)(1) \frac{dx}{2EI} + \int_0^4 (-x)(1) \frac{dx}{EI}$$

$$= 2 \int_0^4 (-x) \frac{dx}{EI} + \int_0^4 (-2) \frac{dx}{EI}$$

$$= 2 \left[-\frac{x^2}{2EI} \right]_0^4 + \left[\frac{-2x}{EI} \right]_0^4$$

$$= -\frac{(4)^2}{EI} - \frac{2(4)}{EI}$$

$$= -\frac{24}{EI}$$

$$\delta_{22} = \int m_2 m_2 \frac{dx}{EI}$$

$$= 0 + \int_0^4 (x)(x) \frac{dx}{2EI} + \int_0^4 (4)(4) \frac{dx}{EI}$$

$$= \int_0^4 \frac{x^2}{2EI} dx + \int_0^4 16 \frac{dx}{EI}$$

$$= \left[\frac{x^3}{3 \times 2EI} \right]_0^4 + \left[\frac{16x}{EI} \right]_0^4$$

$$= \frac{(4)^3}{6EI} + \frac{16 \times 4}{EI}$$

$$= \frac{224}{3EI}$$

$$\delta_{23} = \delta_{32} = \int m_2 m_3 \frac{dx}{EI}$$

$$= 0 + \int_0^4 (x)(1) \frac{dx}{2EI} + \int_0^4 (4)(1) \frac{dx}{EI}$$

$$= \left[\frac{x^2}{2 \times 2EI} \right]_0^4 + \left[\frac{4x}{EI} \right]_0^4$$

$$= \frac{(4)^2}{4EI} + \frac{4 \times 4}{EI}$$

$$= \frac{20}{EI}$$

$$\delta_{33} = \int m_3 m_3 \frac{dx}{EI}$$

$$= \int_0^4 (-1)(-1) \frac{dx}{EI} + \int_0^4 (1)(1) \frac{dx}{2EI} + \int_0^4 (1)(1) \frac{dx}{EI}$$

$$= 2.5 \left[\frac{x}{EI} \right]_0^4$$

$$= \frac{2.5(4)}{EI}$$

$$= \frac{10}{EI}$$

Now,

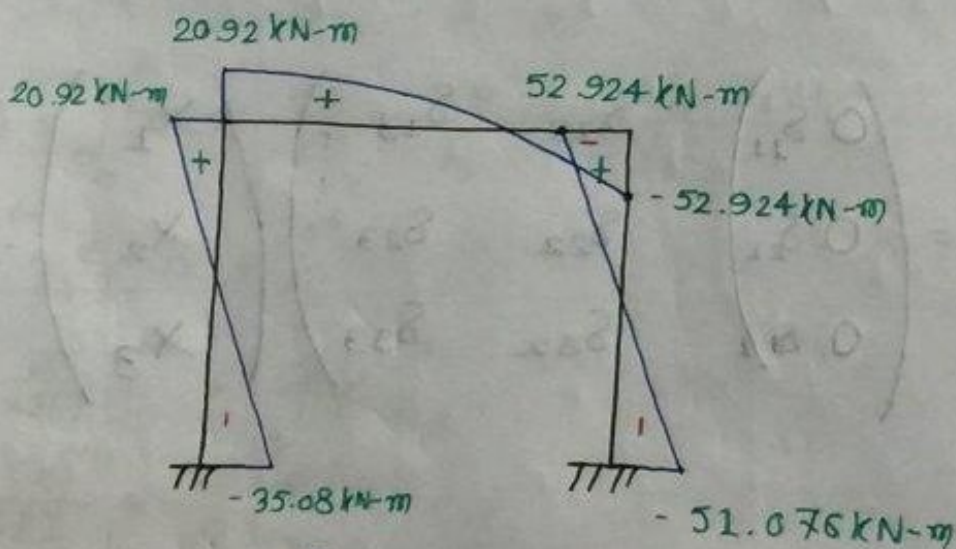
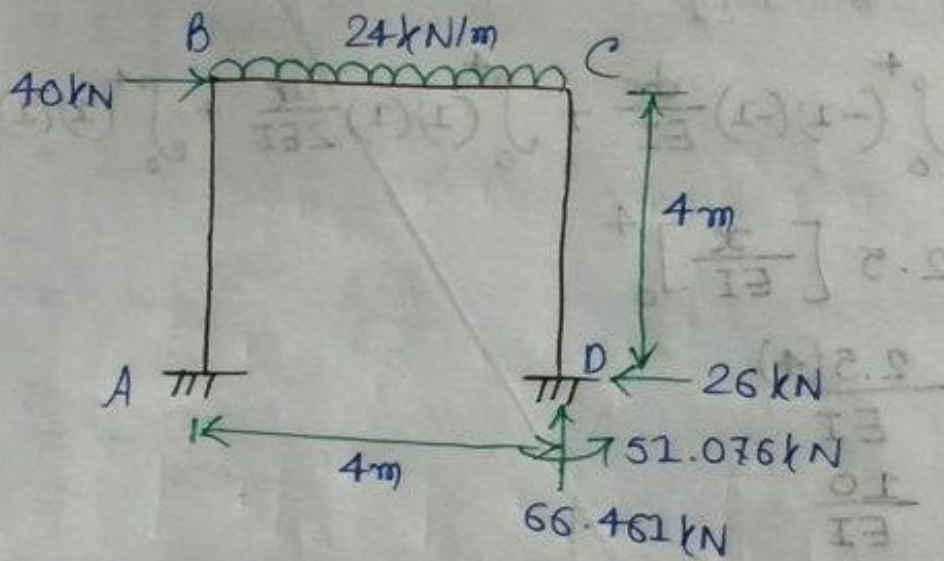
$$\begin{pmatrix} \Delta_1 \\ \Delta_2 \\ \Delta_3 \end{pmatrix} = \begin{pmatrix} \delta_{11} & \delta_{12} & \delta_{13} \\ \delta_{21} & \delta_{22} & \delta_{23} \\ \delta_{31} & \delta_{32} & \delta_{33} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix} + \begin{pmatrix} \Delta_{10} \\ \Delta_{20} \\ \Delta_{30} \end{pmatrix}$$

or,

$$\begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \frac{224}{3EI} & -\frac{48}{EI} & -\frac{24}{EI} \\ -\frac{48}{EI} & \frac{224}{3EI} & \frac{20}{EI} \\ -\frac{24}{EI} & \frac{20}{EI} & \frac{10}{EI} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix} = \begin{pmatrix} \frac{7424}{3EI} \\ -\frac{4736}{EI} \\ -\frac{1216}{EI} \end{pmatrix}$$

By solving the matrix, we get,

$$X_1 = 26 \text{ kN}; \quad X_2 = 66.461 \text{ kN}; \quad X_3 = 51.076 \text{ kN}$$



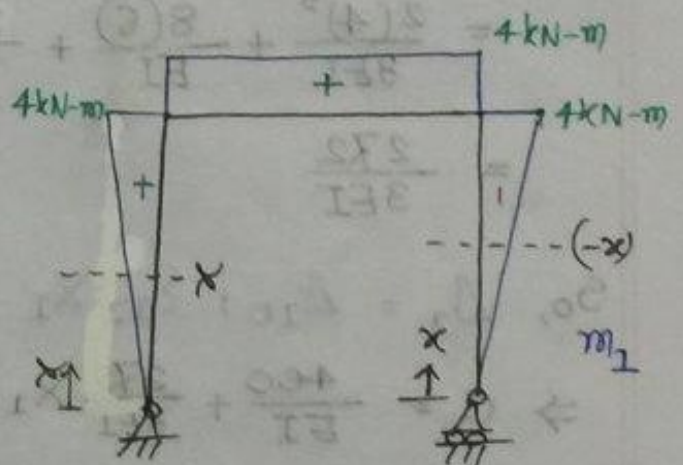
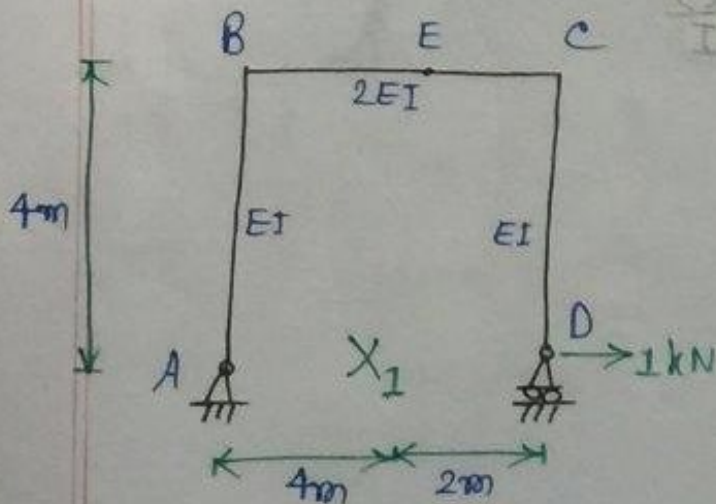
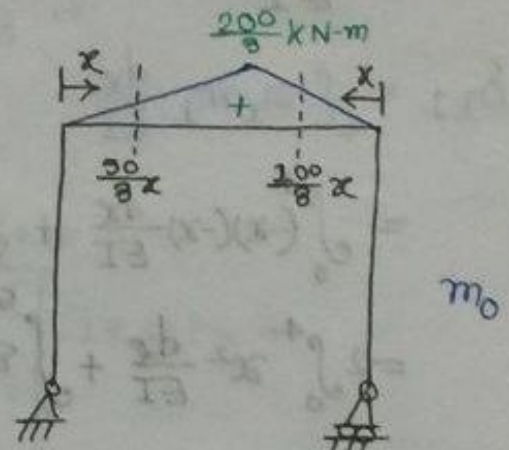
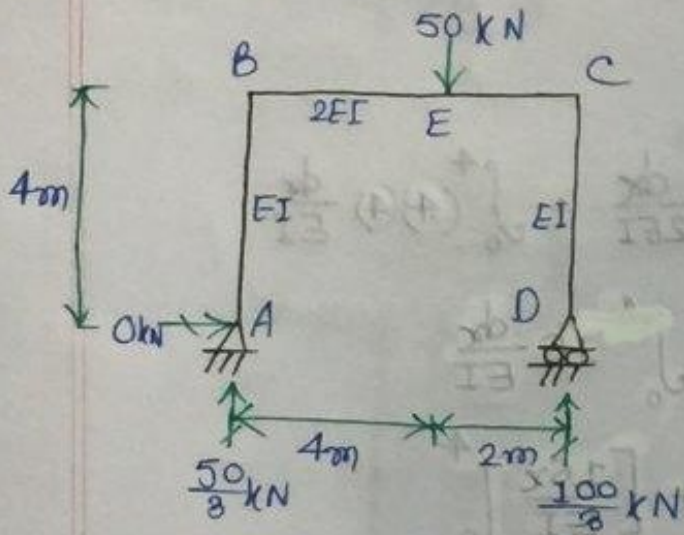
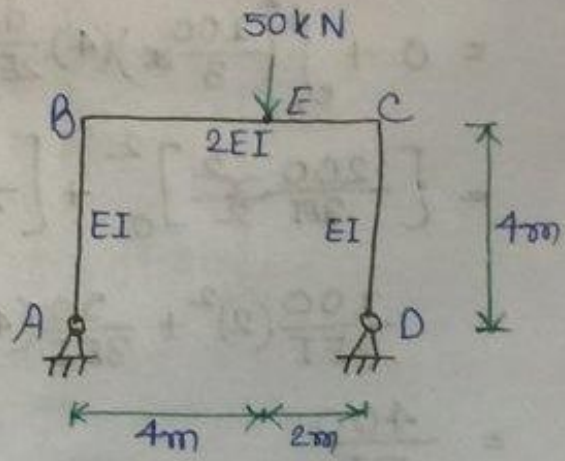
Final BMD

FRAME-5: It is required to determine the horizontal reaction component for the frame. The EI value for the beam is twice the value for the columns.

Solⁿ: Here,

$$D^{\circ} = (2+2) + (3 \times 3) - (4 \times 3) = 1^{\circ}$$

Release horizontal reaction from the right support.



Now,

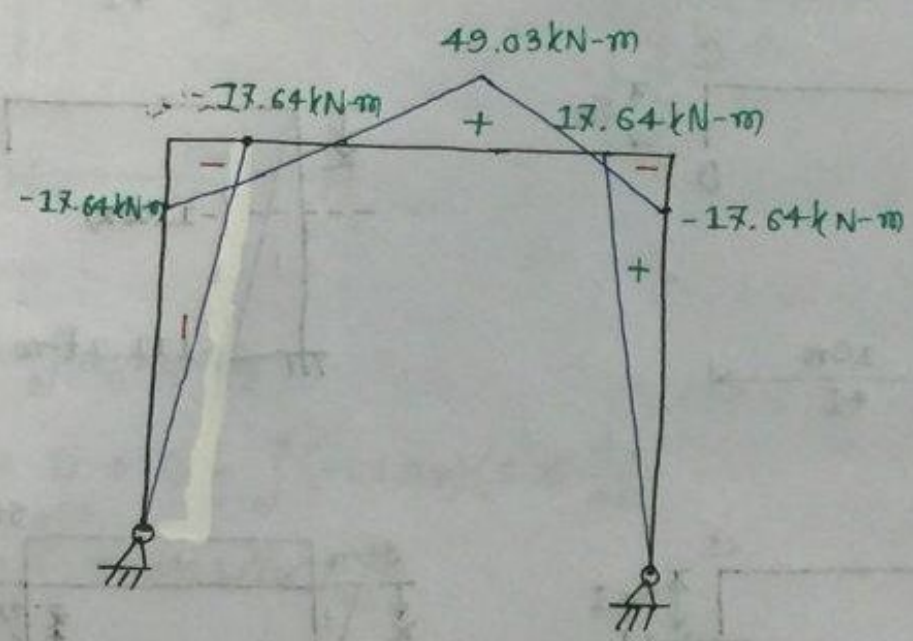
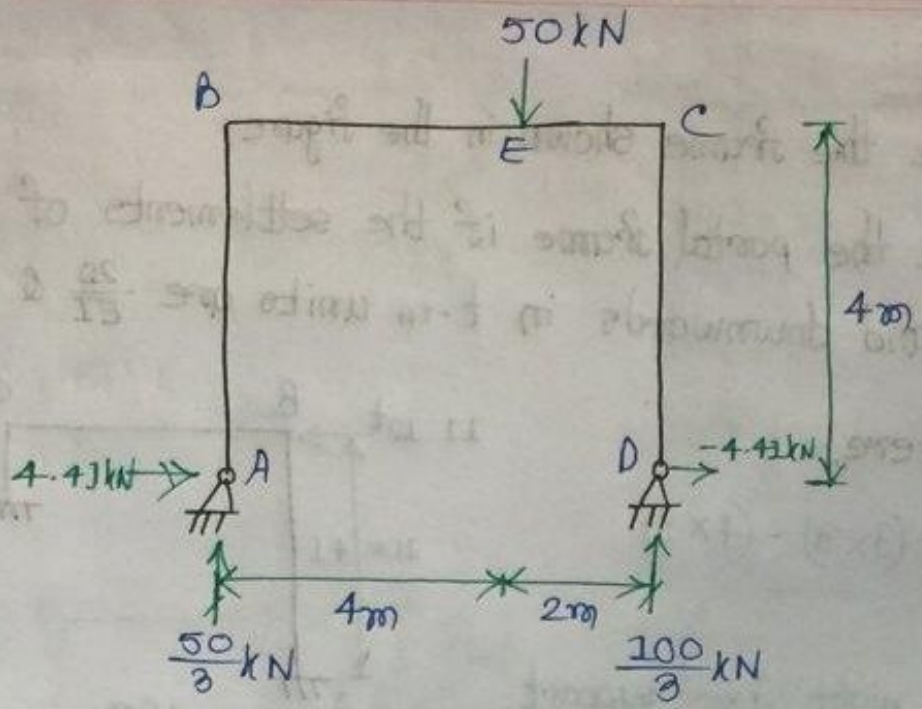
$$\begin{aligned}\Delta_{10} &= \int m_0 m_1 \frac{dx}{EI} \\ &= 0 + \int_0^2 \left(\frac{100}{3}x\right)(4) \frac{dx}{2EI} + \int_0^4 \left(\frac{50}{3}x\right)(4) \frac{dx}{2EI} + 0 \\ &= \left[\frac{200}{3EI} \frac{x^2}{2} \right]_0^2 + \left[\frac{100x^2}{3EI \times 2} \right]_0^4 \\ &= \frac{100}{3EI} (2)^2 + \frac{50}{3EI} (4)^2 \\ &= \frac{400}{EI}\end{aligned}$$

$$\begin{aligned}\delta_{11} &= \int m_1 m_1 \frac{dx}{EI} \\ &= \int_0^4 (-x)(-x) \frac{dx}{EI} + \int_0^6 (4)(4) \frac{dx}{2EI} + \int_0^4 (x)(x) \frac{dx}{EI} \\ &= 2 \int_0^4 x^2 \frac{dx}{EI} + \int_0^6 8 \frac{dx}{EI} \\ &= 2 \left[\frac{x^3}{3EI} \right]_0^4 + \left[\frac{8x}{EI} \right]_0^6 \\ &= \frac{2(4)^3}{3EI} + \frac{8(6)}{EI} + \\ &= \frac{272}{3EI}\end{aligned}$$

$$\text{So, } \Delta_1 = \Delta_{10} + \delta_{11} X_1$$

$$\Rightarrow 0 = \frac{400}{EI} + \frac{272}{3EI} X_1$$

$$\therefore X_1 = -4.41 \text{ kN (Ans.)}$$



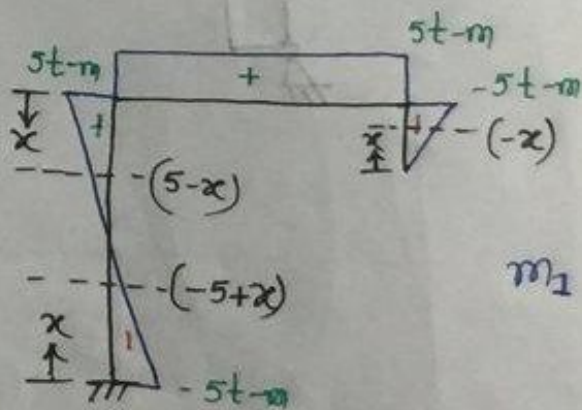
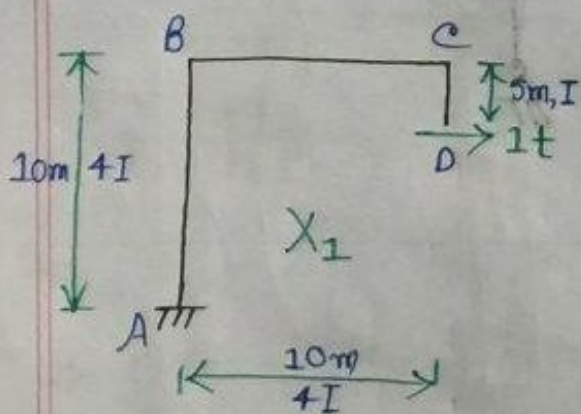
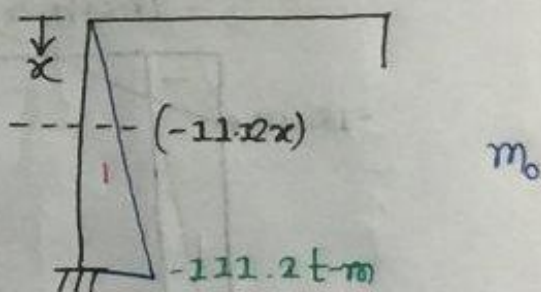
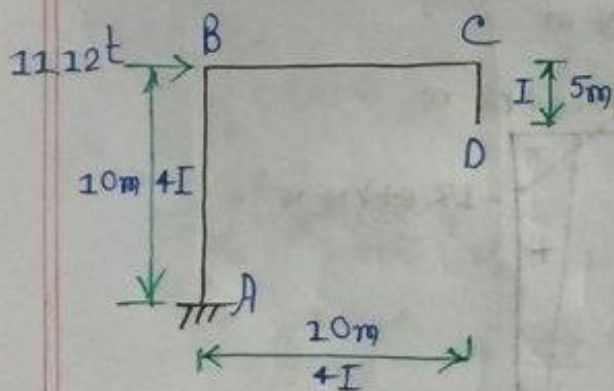
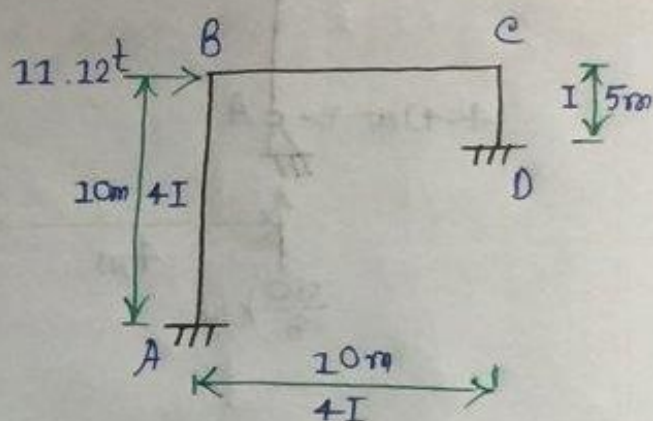
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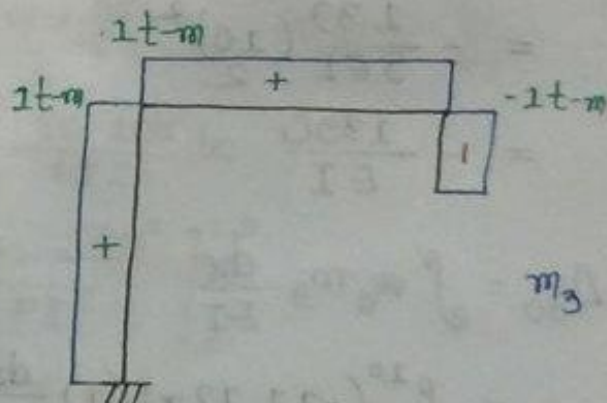
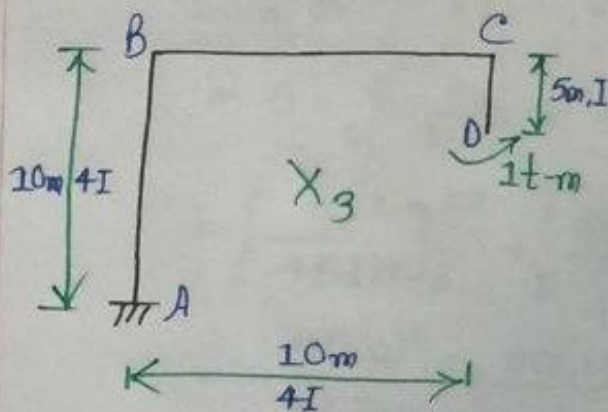
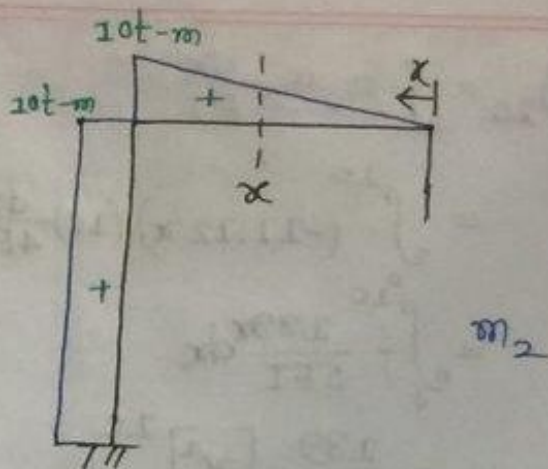
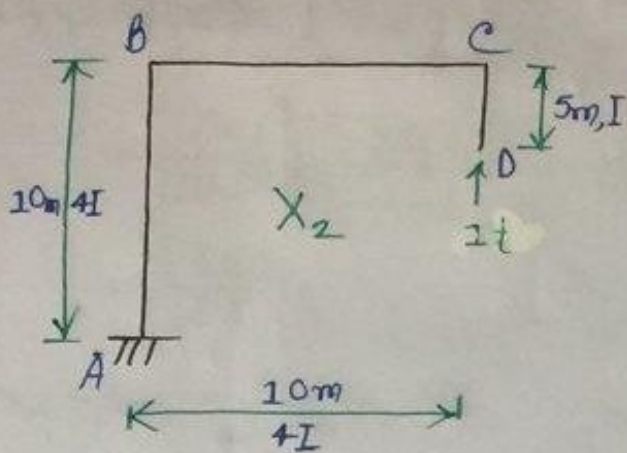
- (a) Analyze the frame shown in the figure.
 (b) Analyze the portal frame if the settlements of support D to the right and downwards in t-m units are $\frac{20}{EI}$ & $\frac{50}{EI}$ respectively.

Solⁿ: (a) Here,

$$D^{\circ} = (3+3) + (3 \times 3) - (4 \times 3) = 3^{\circ}$$

Release the right fixed support.





Now,

$$\Delta_{10} = \int m_0 m_1 \frac{dx}{EI}$$

$$= 0 + 0 + \int (-11.2x)(5-x) \frac{dx}{4EI}$$

$$= \int_0^{10} (-56x + 11.2x^2) \frac{dx}{4EI}$$

$$= \frac{1}{4EI} \left[-\frac{56x^2}{2} + \frac{11.2x^3}{3} \right]_0^{10}$$

$$= \frac{1}{4EI} \left[-\frac{56(10)^2}{2} + \frac{11.2(10)^3}{3} \right]$$

$$= \frac{695}{3EI}$$

$$\begin{aligned}
 \Delta_{20} &= \int m_0 m_2 \frac{dx}{EI} \\
 &= \int_0^{10} (-11.12x)(10) \frac{dx}{4EI} \\
 &= \int_0^{10} -\frac{139x}{5EI} dx \\
 &= -\frac{139}{5EI} \left[\frac{x^2}{2} \right]_0^{10} \\
 &= -\frac{139}{5EI} \left(\frac{10}{2} \right)^2 \\
 &= -\frac{1390}{EI}
 \end{aligned}$$

$$\begin{aligned}
 \Delta_{30} &= \int m_0 m_3 \frac{dx}{EI} \\
 &= \int_0^{10} (-11.12x)(1) \frac{dx}{4EI} \\
 &= \frac{1}{4EI} \left[-11.12 \frac{x^2}{2} \right]_0^{10} \\
 &= \frac{1}{4EI} \left[-\frac{11.12(10)^2}{2} \right] \\
 &= -\frac{139}{EI}
 \end{aligned}$$

$$\begin{aligned}
 \delta_{11} &= \int m_1 m_1 \frac{dx}{EI} \\
 &= \int_0^5 (-x)(-x) \frac{dx}{EI} + \int_0^{10} (5)(5) \frac{dx}{4EI} + \int_0^{10} (5-x)^2 \frac{dx}{4EI} \\
 &= \int_0^5 \frac{x^2}{EI} dx + \int_0^{10} \frac{25}{4EI} dx + \int_0^{10} \frac{25 - 10x + x^2}{4EI} dx
 \end{aligned}$$

$$\begin{aligned}
 \delta_{11} &= \left[\frac{x^3}{3EI} \right]_0^5 + \left[\frac{25x}{4EI} \right]_0^{10} + \left[\frac{25x - \frac{10x^2}{2} + \frac{x^3}{3}}{4EI} \right]_0^{10} \\
 &= \frac{(5)^3}{3EI} + \frac{25(10)}{4EI} + \frac{25(10) - 5(10)^2 + \frac{(10)^3}{3}}{4EI} \\
 &= \frac{125}{EI}
 \end{aligned}$$

$$\begin{aligned}
 \delta_{12} = \delta_{21} &= \int m_1 m_2 \frac{dx}{EI} \\
 &= \int_0^5 (-x) \cdot 0 \frac{dx}{EI} + \int_0^{10} (5) x \frac{dx}{4EI} + \int_0^{10} (5-x)(10) \frac{dx}{4EI} \\
 &= 0 + \int_0^{10} \frac{5x}{4EI} dx + \int_0^{10} \frac{50-10x}{4EI} dx \\
 &= \left[\frac{5x^2}{4EI \times 2} \right]_0^{10} + \left[\frac{50x - \frac{10x^2}{2}}{4EI} \right]_0^{10} \\
 &= \frac{5(10)^2}{4EI \times 2} + \frac{50(10) - 5(10)^2}{4EI} \\
 &= \frac{62.5}{EI}
 \end{aligned}$$

$$\begin{aligned}
 \delta_{13} = \delta_{31} &= \int m_1 m_3 \frac{dx}{EI} \\
 &= \int_0^5 (-x)(-1) \frac{dx}{EI} + \int_0^{10} (5)(1) \frac{dx}{4EI} + \int_0^{10} (5-x)(1) \frac{dx}{4EI} \\
 &= \left[\frac{x^2}{2EI} \right]_0^5 + \left[\frac{5x}{4EI} \right]_0^{10} + \left[\frac{5x - \frac{x^2}{2}}{4EI} \right]_0^{10} \\
 &= \frac{(5)^2}{2EI} + \frac{5(10)}{4EI} + \frac{5(10) - \frac{(10)^2}{2}}{4EI} \\
 &= \frac{25}{EI}
 \end{aligned}$$

$$\begin{aligned}
\delta_{22} &= \int m_2 m_2 \frac{dx}{EI} \\
&= 0 + \int_0^{10} (x)(x) \frac{dx}{4EI} + \int_0^{10} (10)(10) \frac{dx}{4EI} \\
&= \left[\frac{x^3}{3 \times 4EI} \right]_0^{10} + \left[\frac{100x}{4EI} \right]_0^{10} \\
&= \frac{(10)^3}{3EI} + \frac{100(10)}{4EI} \\
&= \frac{1000}{3EI}
\end{aligned}$$

$$\begin{aligned}
\delta_{23} = \delta_{32} &= \int m_2 m_3 \frac{dx}{EI} \\
&= 0 + \int_0^{10} (x)(1) \frac{dx}{4EI} + \int_0^{10} (10)(1) \frac{dx}{4EI} \\
&= \left[\frac{x^2}{2 \times 4EI} \right]_0^{10} + \left[\frac{10x}{4EI} \right]_0^{10} \\
&= \frac{(10)^2}{8EI} + \frac{10(10)}{4EI} \\
&= \frac{37.5}{EI}
\end{aligned}$$

$$\begin{aligned}
\delta_{33} &= \int m_3 m_3 \frac{dx}{EI} \\
&= \int_0^5 (-1)(-1) \frac{dx}{EI} + \int_0^{10} (1)(1) \frac{dx}{4EI} + \int_0^{10} (1)(1) \frac{dx}{4EI} \\
&= \left[\frac{x}{EI} \right]_0^5 + 2 \times \left[\frac{x}{4EI} \right]_0^{10} \\
&= \frac{5}{EI} + 2 \times \frac{10}{4EI} = \frac{10}{EI}
\end{aligned}$$

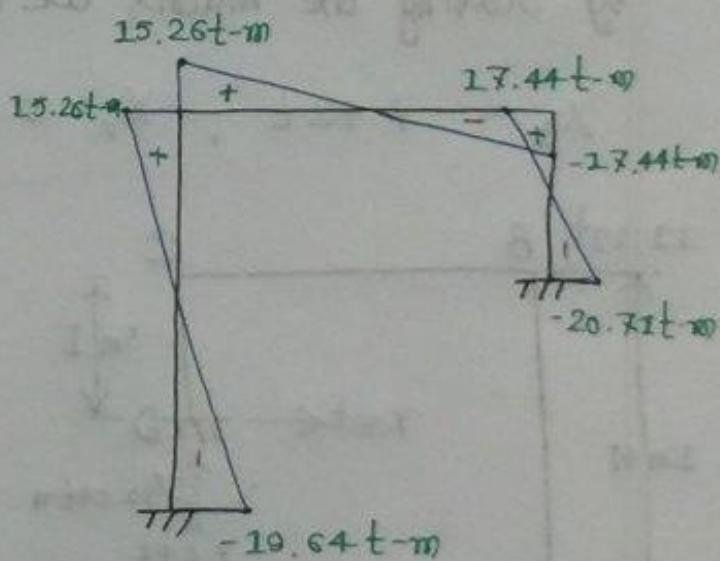
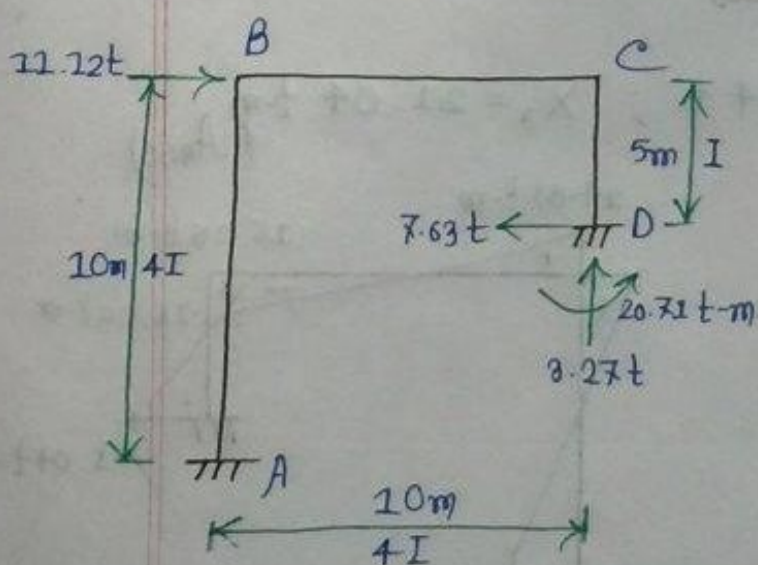
(a) For, No Support Settlements,

$$\begin{pmatrix} \Delta_1 \\ \Delta_2 \\ \Delta_3 \end{pmatrix} = \begin{pmatrix} \Delta_{10} \\ \Delta_{20} \\ \Delta_{30} \end{pmatrix} + \begin{pmatrix} \delta_{11} & \delta_{12} & \delta_{13} \\ \delta_{21} & \delta_{22} & \delta_{23} \\ \delta_{31} & \delta_{32} & \delta_{33} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix}$$

$$\Rightarrow \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \frac{695}{3EI} \\ -\frac{1990}{EI} \\ -\frac{139}{EI} \end{pmatrix} + \begin{pmatrix} \frac{125}{EI} & \frac{62.5}{EI} & \frac{25}{EI} \\ \frac{62.5}{EI} & \frac{1000}{3EI} & \frac{37.5}{EI} \\ \frac{25}{EI} & \frac{37.5}{EI} & \frac{10}{EI} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix}$$

By solving the matrix, we get,

$$X_1 = -7.63 t ; X_2 = 3.27 t ; X_3 = 20.71 t \cdot m \text{ (Ans.)}$$



Final BMD

(b) With support settlements, $\Delta_1 = \frac{20}{EI}$ (same direction to X_1)

& $\Delta_2 = -\frac{50}{EI}$ (opposite direction to X_2)

Hence,

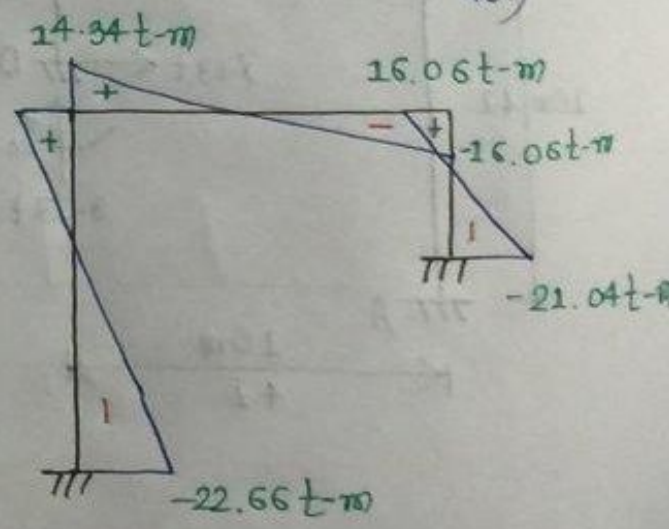
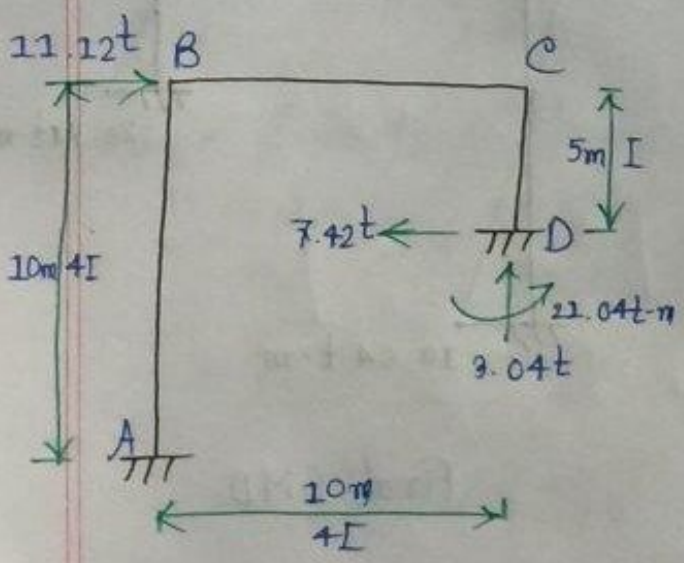
$$\begin{pmatrix} \Delta_1 \\ \Delta_2 \\ \Delta_3 \end{pmatrix} = \begin{pmatrix} \Delta_{10} \\ \Delta_{20} \\ \Delta_{30} \end{pmatrix} + \begin{pmatrix} \delta_{11} & \delta_{12} & \delta_{13} \\ \delta_{21} & \delta_{22} & \delta_{23} \\ \delta_{31} & \delta_{32} & \delta_{33} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix}$$

or,

$$\begin{pmatrix} \frac{20}{EI} \\ -\frac{50}{EI} \\ 0 \end{pmatrix} = \begin{pmatrix} \frac{695}{3EI} \\ -\frac{1390}{EI} \\ -\frac{139}{EI} \end{pmatrix} + \begin{pmatrix} \frac{125}{EI} & \frac{62.5}{EI} & \frac{25}{EI} \\ \frac{62.5}{EI} & \frac{1000}{3EI} & \frac{37.5}{EI} \\ \frac{25}{EI} & \frac{37.5}{EI} & \frac{10}{EI} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \\ X_3 \end{pmatrix}$$

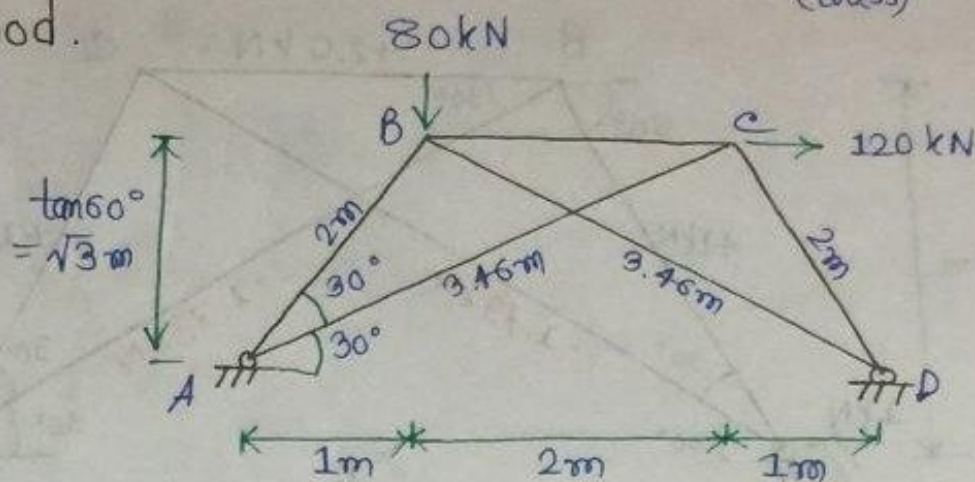
By solving the matrix we get,

$$X_1 = -7.42t, \quad X_2 = 3.04t, \quad X_3 = 21.04t \cdot m \quad (\text{Ans.})$$



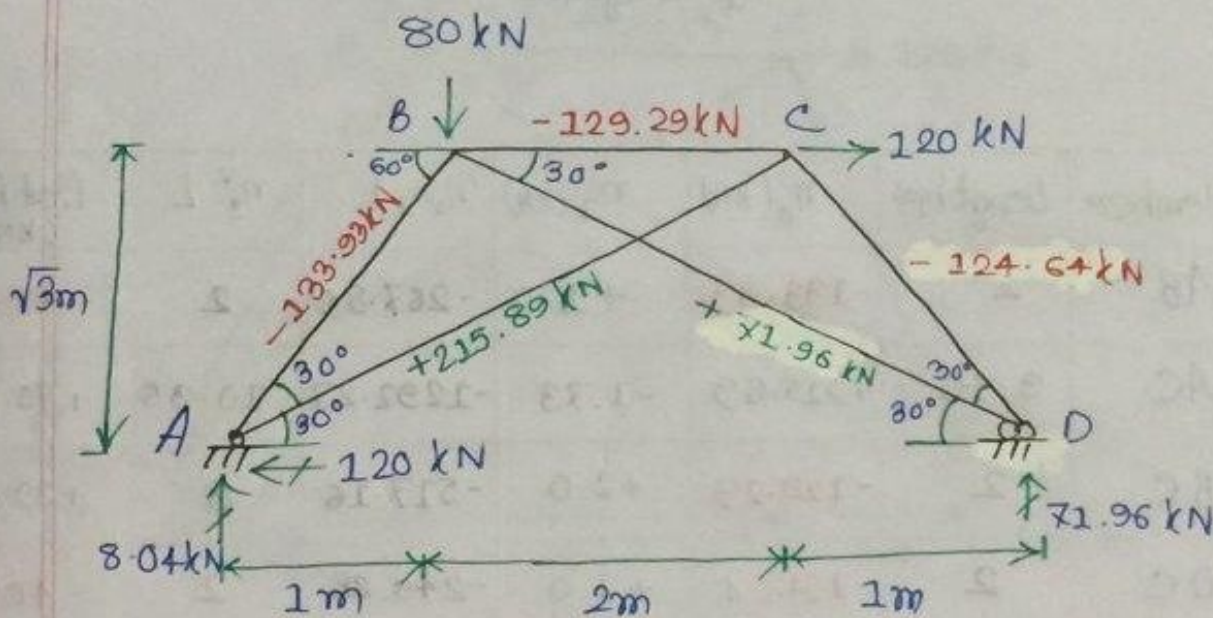
Final BMD

TRUSS-1: Analyze the indeterminate pin-jointed frame by the force method. (truss)

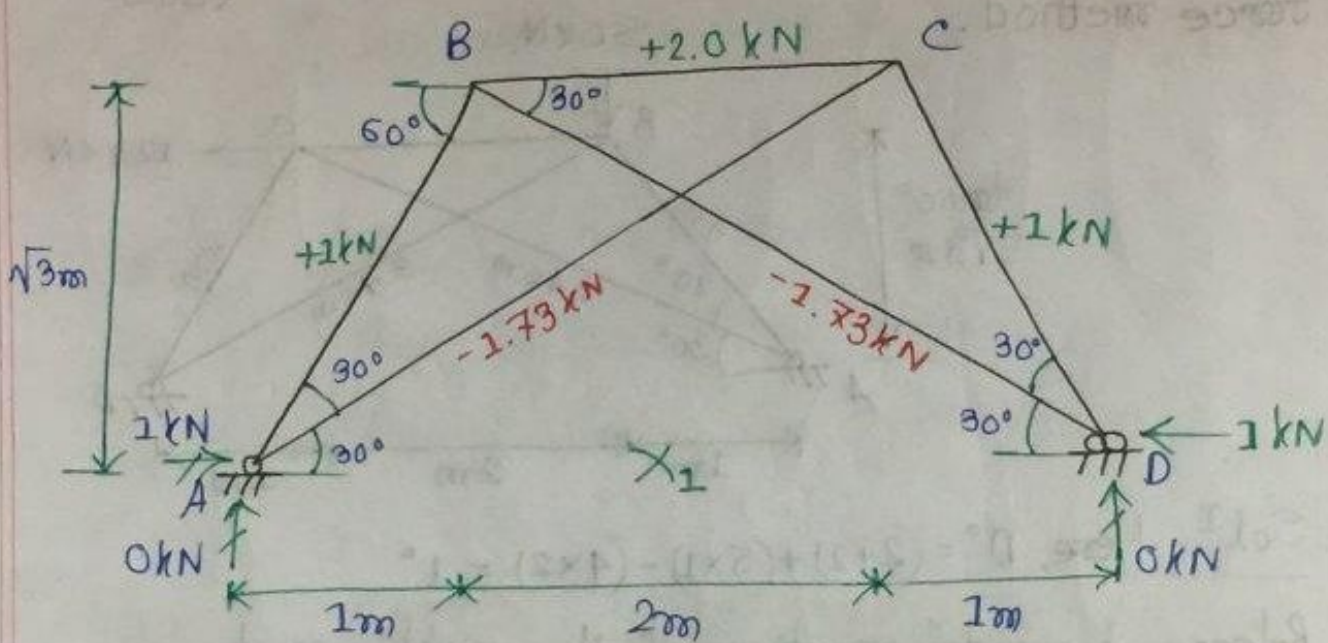


Solⁿ: Here, $D^{\circ} = (2+2) + (5 \times 1) - (4 \times 2) = 1^{\circ}$

Release horizontal reaction of the right support.



N_0 -diagram



n_1 -diagram

Member	Length(m)	n_0 (kN)	n_1 (kN)	$n_0 n_1 L$	$n_1^2 L$	Final force (kN)
AB	2	-133.93	+1.0	-267.86	2	-49.66
AC	3.46	+215.89	-1.73	-1292.27	10.36	+70.1
BC	2	-129.29	+2.0	-517.16	8	+39.25
DC	2	-124.64	+1.0	-249.28	2	-40.37
DB	3.46	+71.96	-1.73	-430.74	10.36	-73.83
				-2757.28	32.72	(Using formula)

Note: Final force, $n = n_0 + \sum n_i X_i$

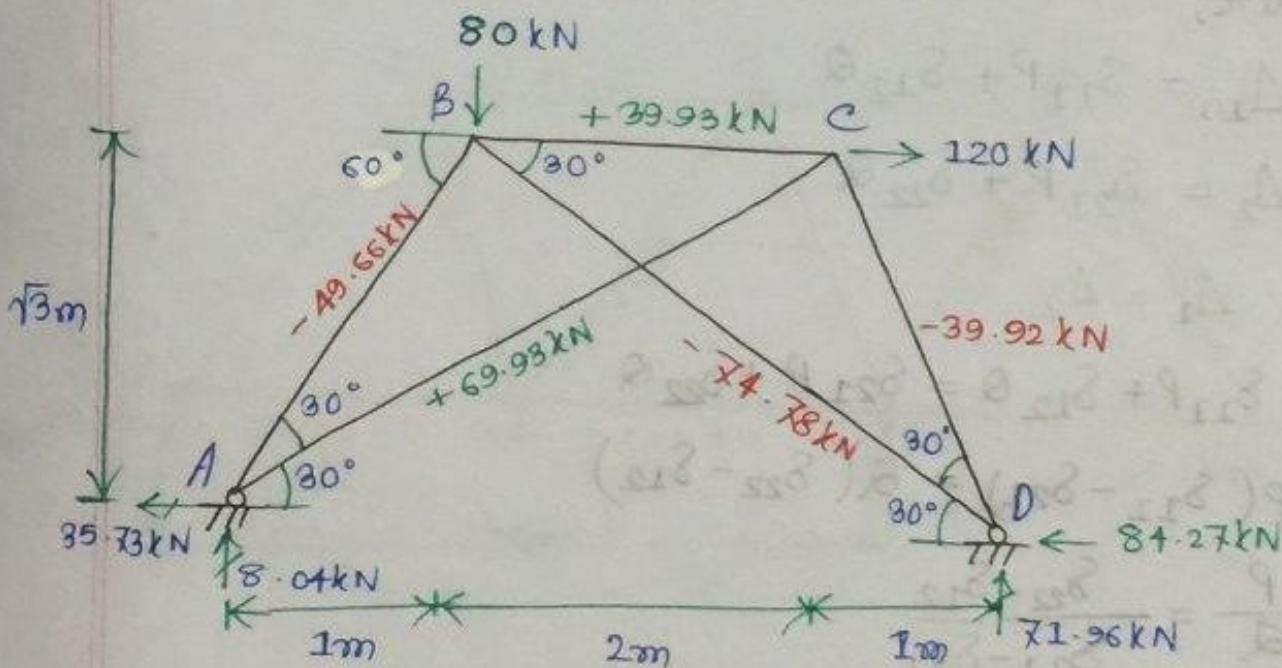
Now,

$$\Delta_1 = \Delta_{10} + \delta_{11} X_1$$

$$\Rightarrow \Delta_1 = \sum \frac{n_0 n_1 L}{AE} + \sum \frac{n_1 n_1 L}{AE} X_1$$

$$\Rightarrow 0 = -\frac{2757.28}{AE} + \frac{32.72}{AE} X_1$$

$$\therefore X_1 = 84.27 \text{ kN (Ans.)}$$



Final Bar Forces (Using Force Analysis)

TRUSS-2: For the pin jointed truss with loads P and Q as shown in figure, determine the ratio $\frac{P}{Q}$ so that the joint E and F have the same vertical displacement. $\frac{1}{AE}$ is constant for all members.

Solⁿ: Here,

$$D^{\circ} = (2+1) + (11 \times 1) - (7 \times 2) \\ = 0^{\circ}$$

But due to vertical displacement, we have,

$$\Delta_1 = \delta_{11}P + \delta_{12}Q$$

$$\Delta_2 = \delta_{21}P + \delta_{22}Q$$

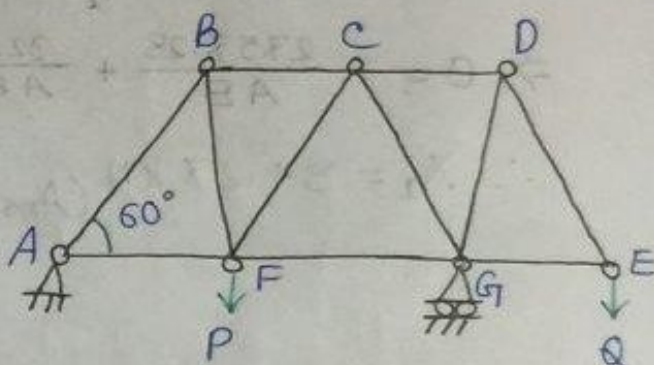
Now, $\Delta_1 = \Delta_2$

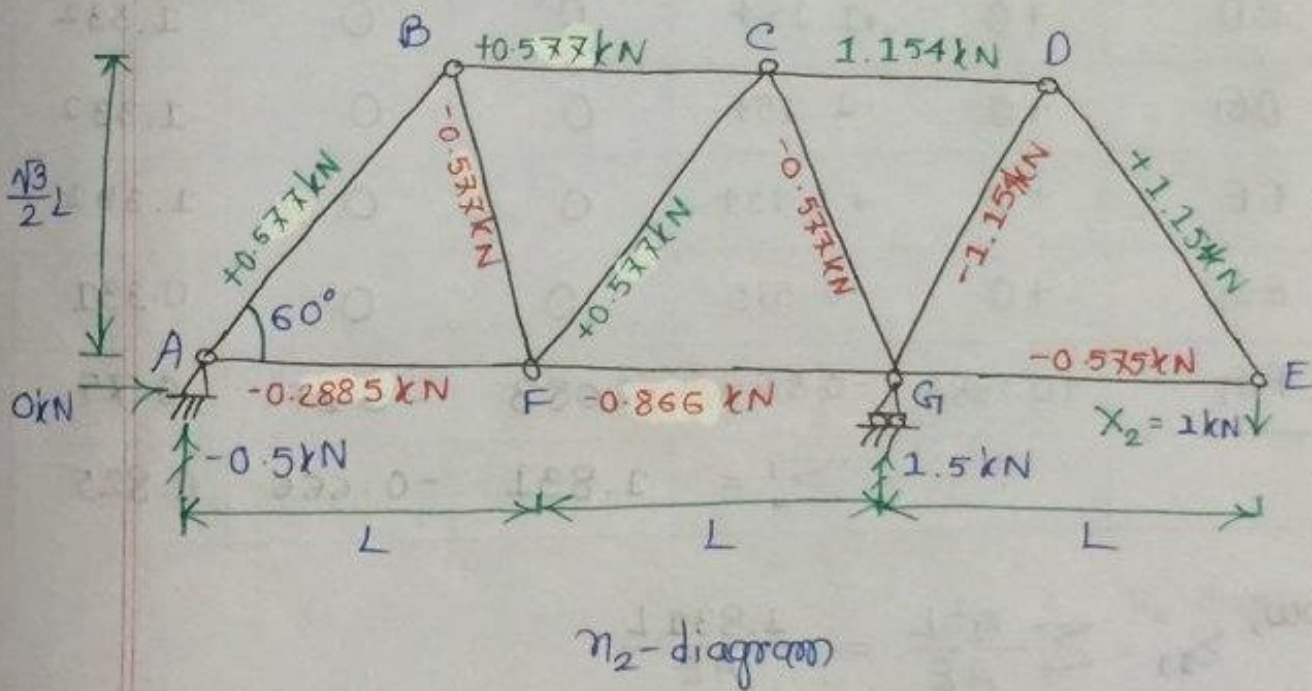
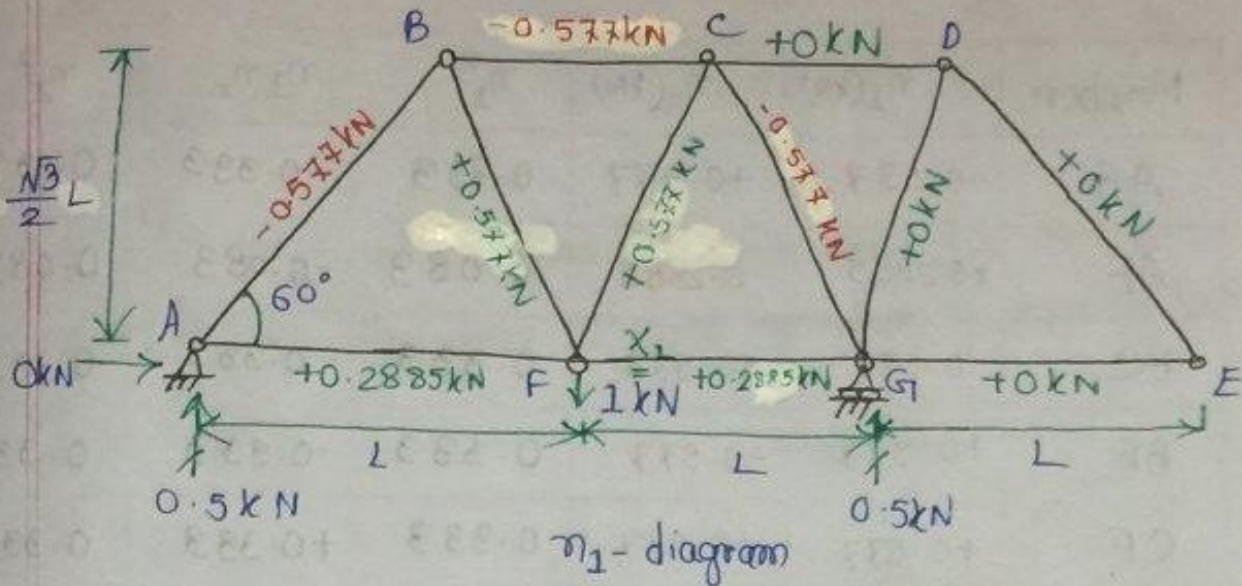
$$\text{So, } \delta_{11}P + \delta_{12}Q = \delta_{21}P + \delta_{22}Q$$

$$\Rightarrow P(\delta_{11} - \delta_{21}) = Q(\delta_{22} - \delta_{12})$$

$$\therefore \frac{P}{Q} = \frac{\delta_{22} - \delta_{12}}{\delta_{11} - \delta_{21}}$$

where, δ_{11} & δ_{21} are the displacements of points F & E respectively due to a unit vertical load at joint F . Similarly, δ_{12} & δ_{22} are the displacements of points F & E respectively due to a unit vertical load at joint E





Member	η_1 (kN)	η_2 (kN)	η_1^2	$\eta_1 \eta_2$	η_2^2
AB	-0.577	+0.577	0.333	-0.333	0.333
AF	+0.2885	-0.2885	0.083	-0.083	0.083
BC	-0.577	+0.577	0.333	-0.333	0.333
BF	+0.577	-0.577	0.333	-0.333	0.333
CF	+0.577	+0.577	0.333	+0.333	0.333
CG	-0.577	-0.577	0.333	+0.333	0.333
CD	+0	+1.154	0	0	1.332
DG	+0	-1.154	0	0	1.332
DE	+0	+1.154	0	0	1.332
EG	+0	-0.575	0	0	0.331
FG	+0.2885	-0.866	0.083	-0.25	0.75
		$\Sigma =$	1.831	-0.666	6.825

$$\text{Now, } \delta_{11} = \sum \frac{\eta_1^2 L}{AE} = \frac{1.831 L}{AE}$$

$$\delta_{12} = \delta_{21} = \sum \frac{\eta_1 \eta_2 L}{AE} = -\frac{0.666 L}{AE}$$

$$\delta_{22} = \sum \frac{\eta_2^2 L}{AE} = \frac{6.825 L}{AE}$$

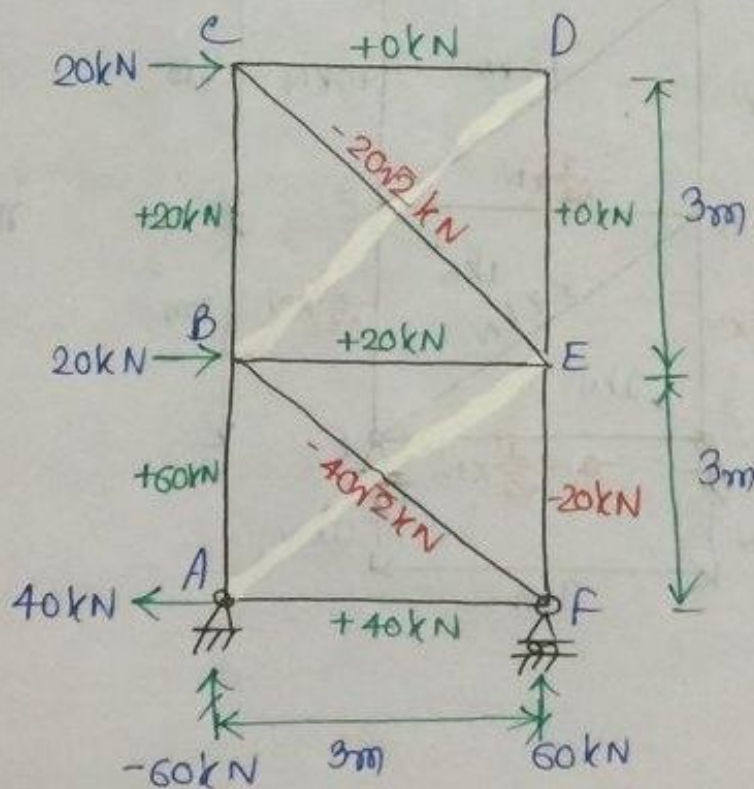
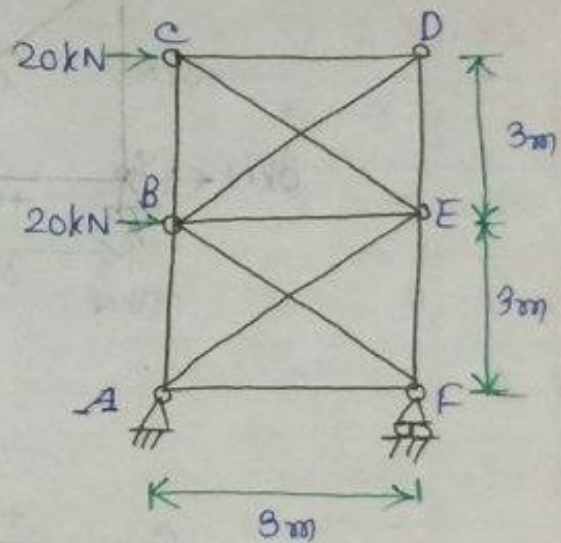
$$\text{Hence, } \frac{P}{Q} = \frac{\delta_{22} - \delta_{12}}{\delta_{11} - \delta_{21}} = \frac{\frac{5.825L}{AE} - \left(-\frac{0.666L}{AE}\right)}{\frac{1.831L}{AE} - \left(-\frac{0.666L}{AE}\right)} = 3 \quad (\text{Ans.})$$

TRUSS-3: It is required to determine the bar forces in the steel truss. The area of each member is $500 \times 10^{-6} \text{ m}^2 (500 \text{ mm}^2)$.

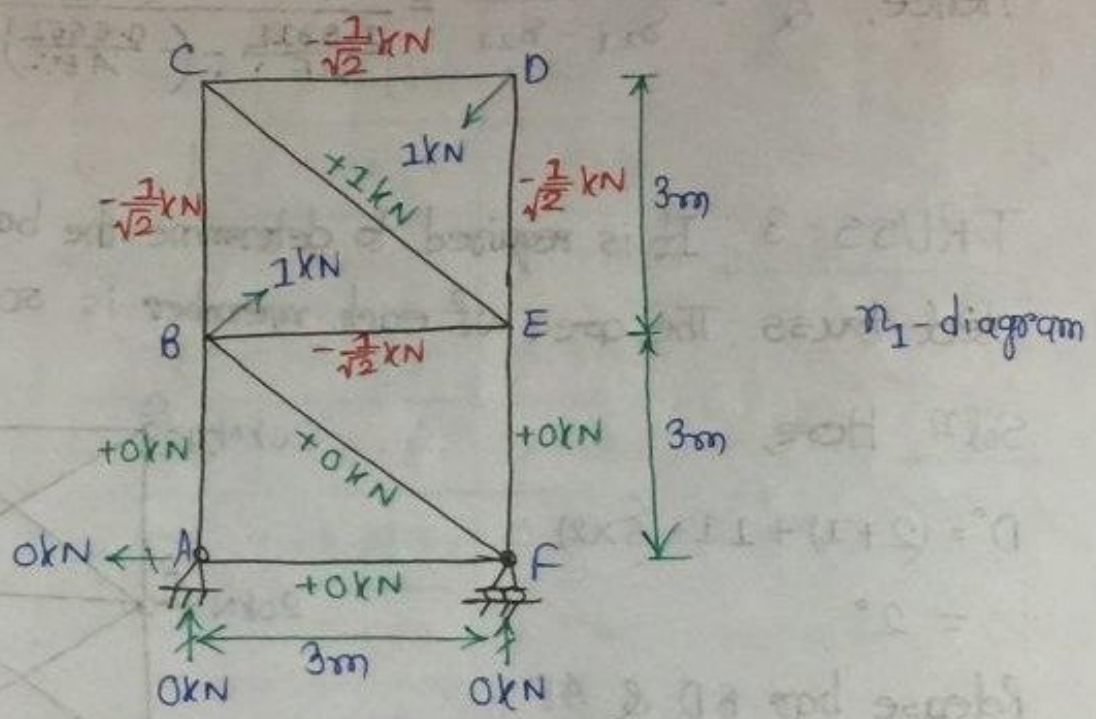
Solⁿ: Here,

$$D^{\circ} = (2+1) + 11 - (6 \times 2) = 2^{\circ}$$

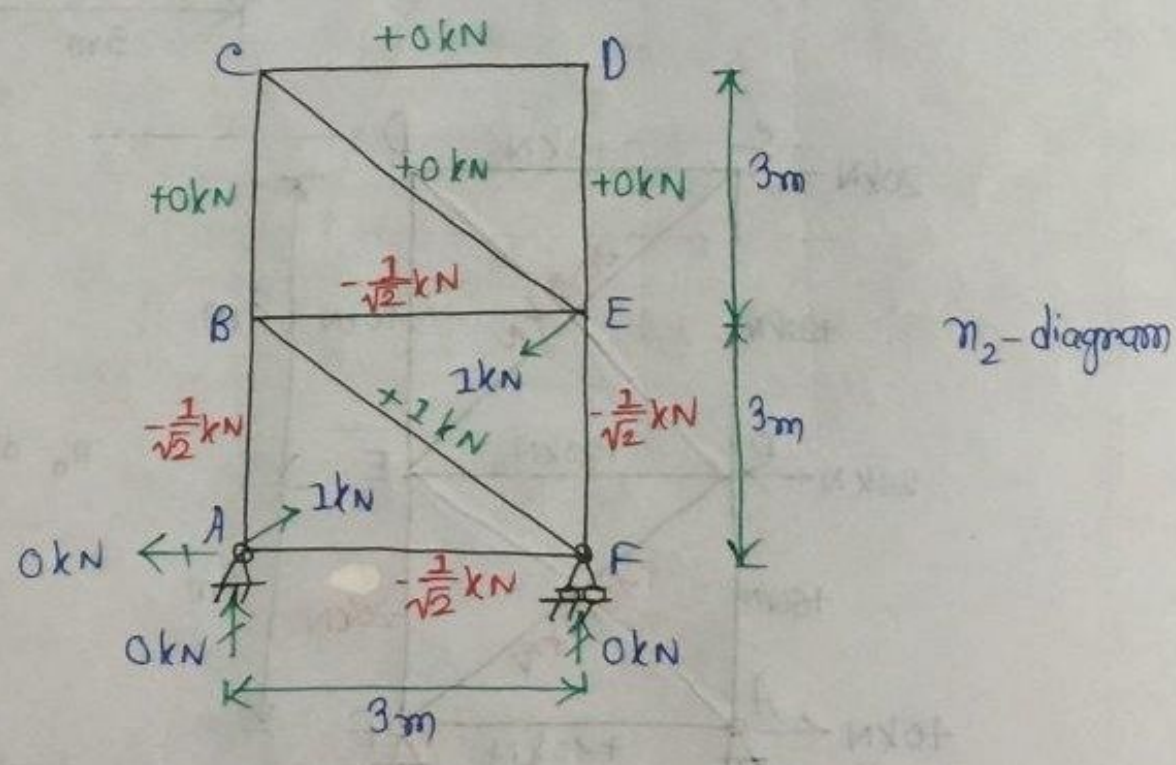
Release bar BD & AE.



n_0 - diagram



n_1 -diagram



n_2 -diagram

Member	Length (m)	n_0 (kN)	n_1 (kN)	n_2 (kN)	$n_0 n_1 L$	$n_0 n_2 L$	$n_1^2 L$	$n_2^2 L$	$n_1 n_2 L$	Force Bar Force $= n_0 + n_1 \sqrt{1} + n_2 \sqrt{2}$
AB	3	+60	+0	$-\frac{1}{\sqrt{2}}$	0	$-30\sqrt{2}$	0	0	1.5	+58.74
BC	3	+20	$-\frac{1}{\sqrt{2}}$	+0	$-30\sqrt{2}$	0	1.5	0	0	+12.2
FE	3	-20	+0	$-\frac{1}{\sqrt{2}}$	0	$30\sqrt{2}$	0	0	1.5	-41.5
ED	3	+0	$-\frac{1}{\sqrt{2}}$	+0	0	0	1.5	0	0	-7.8
AF	3	+40	+0	$-\frac{1}{\sqrt{2}}$	0	$-60\sqrt{2}$	0	0	1.5	+18.74
BE	3	+20	$-\frac{1}{\sqrt{2}}$	$-\frac{1}{\sqrt{2}}$	$-30\sqrt{2}$	$-30\sqrt{2}$	1.5	1.5	1.5	-9.06
CD	3	+0	$-\frac{1}{\sqrt{2}}$	+0	0	0	1.5	0	0	-7.8
AE	$3\sqrt{2}$	+0	+0	+1	0	0	0	0	$3\sqrt{2}$	+30.071
BF	$3\sqrt{2}$	$-40\sqrt{2}$	+0	+1	0	-240	0	0	$3\sqrt{2}$	-26.50
BD	$3\sqrt{2}$	+0	+1	+0	0	0	$3\sqrt{2}$	0	0	+11.03
CE	$3\sqrt{2}$	$-20\sqrt{2}$	+1	+0	-120	0	$3\sqrt{2}$	0	0	-17.26
				Σ	$-60\sqrt{2} - 120$	$-150\sqrt{2} - 240$	$6 + 6\sqrt{2}$	1.5	$6 + 6\sqrt{2}$	

Now,

$$\Delta_1 = \Delta_{10} + \delta_{11} X_1 + \delta_{12} X_2$$

$$\Delta_2 = \Delta_{20} + \delta_{21} X_1 + \delta_{22} X_2$$

Where, $\Delta_{10} = \sum \frac{n_0 n_1 L}{AE}$

$$\Delta_{20} = \sum \frac{n_0 n_2 L}{AE}$$

$$\delta_{11} = \sum \frac{n_1^2 L}{AE}$$

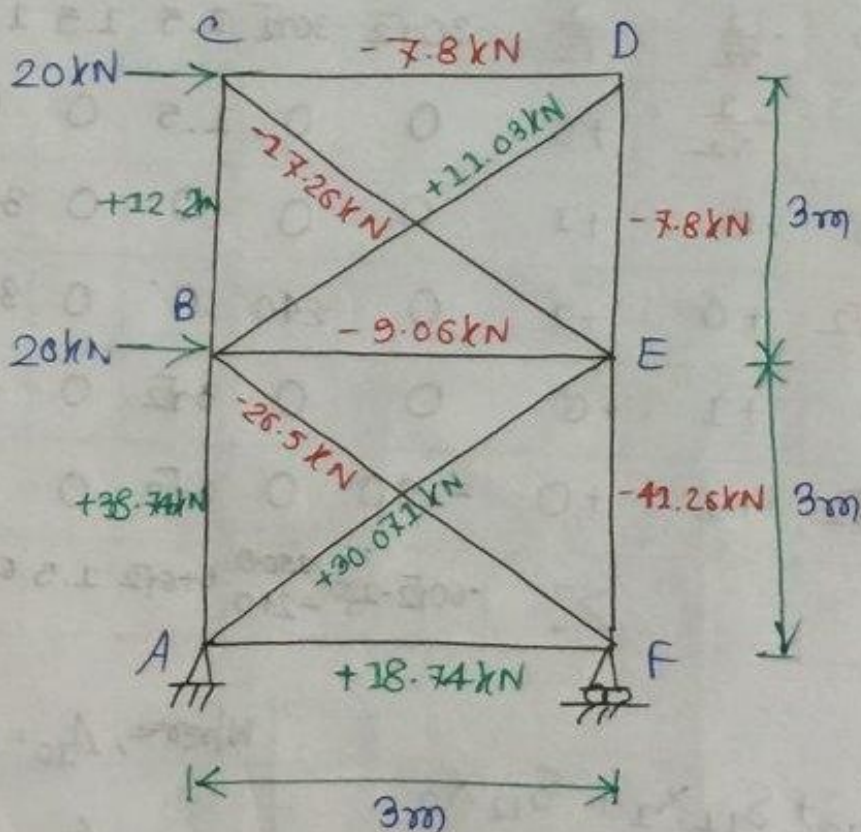
$$\delta_{12} = \delta_{21} = \sum \frac{n_1 n_2 L}{AE}$$

$$\delta_{22} = \sum \frac{n_2^2 L}{AE}$$

$$\Rightarrow \begin{pmatrix} 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \frac{-60\sqrt{2}-120}{AE} \\ \frac{-150\sqrt{2}-240}{AE} \end{pmatrix} + \begin{pmatrix} \frac{6+6\sqrt{2}}{AE} & \frac{1.5}{AE} \\ \frac{1.5}{AE} & \frac{6+6\sqrt{2}}{AE} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}$$

By solving the matrix we get,

$$X_1 = 11.028 \text{ kN} \quad \& \quad X_2 = 30.071 \text{ kN}$$



Final bar forces

TRUSS-4: Consider the given truss and supposing that there is a temperature drop of 30°C on all the outer members AB, BC, CD, DE, EF, find the forces set up in the members due to temperature drop only. Take $\alpha = 1.0 \times 10^{-5}/^\circ\text{C}$.

Solⁿ: Here, same as TRUSS-3.

Instead of External loads, due to temperature drop, the outer members AB, BC, CD, DE, EF induces bar forces in those.

Here, $D^\circ = 2^\circ$

So,

$$\begin{pmatrix} \Delta_1 \\ \Delta_2 \end{pmatrix} = \begin{pmatrix} \Delta_{10} \\ \Delta_{20} \end{pmatrix} + \begin{pmatrix} \delta_{11} & \delta_{12} \\ \delta_{21} & \delta_{22} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}$$

where, $\Delta_{i0} = \sum n_i \alpha (\Delta T) L$

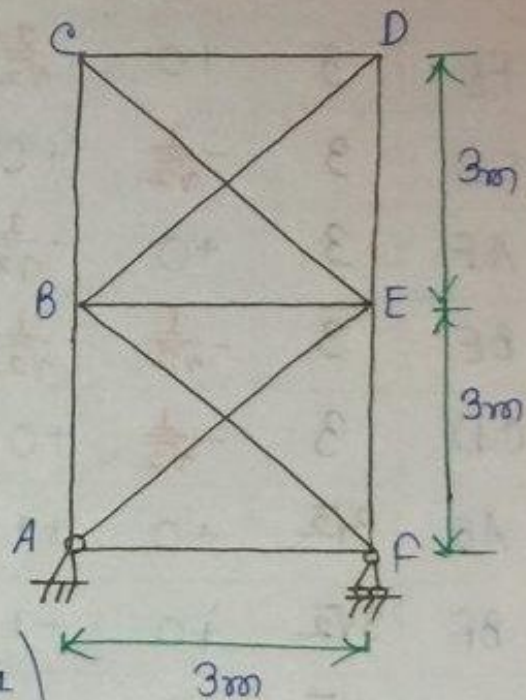
$$\delta_{ij} = \sum \frac{n_i n_j L}{AE}$$

n_1 & n_2 diagram is same as TRUSS-3.

Given, $\alpha = 1.0 \times 10^{-5}/^\circ\text{C}$

$$\Delta T = -30^\circ\text{C}$$

$$AE = (500 \times 10^{-6} \text{ m}^2 \times 200 \times 10^6 \text{ kPa}) = 10^5$$



-30°C

ΔT

Member	Length	n_1	n_2	$n_2 L$ $\times \alpha \Delta T$	$n_2 \alpha \Delta T L$	$n_1^2 L$	$n_1 n_2 L$	$n_2^2 L$	Final bar force $= n_1 X_1 + n_2 X_2$
AB	3	+0	$-\frac{1}{\sqrt{2}}$	0	$+6.36 \times 10^{-4}$	0	0	1.5	+5.3
BC	3	$-\frac{1}{\sqrt{2}}$	+0	$+6.36 \times 10^{-4}$	0	1.5	0	0	+8.76
FE	3	+0	$-\frac{1}{\sqrt{2}}$	0	$+6.36 \times 10^{-4}$	0	0	1.5	+5.3
ED	3	$-\frac{1}{\sqrt{2}}$	+0	$+6.36 \times 10^{-4}$	0	1.5	0	0	+8.76
AF	3	+0	$-\frac{1}{\sqrt{2}}$	-	-	0	0	1.5	+5.3
BE	3	$-\frac{1}{\sqrt{2}}$	$-\frac{1}{\sqrt{2}}$	-	-	1.5	1.5	1.5	+14.07
CD	3	$-\frac{1}{\sqrt{2}}$	+0	$+6.36 \times 10^{-4}$	0	1.5	0	0	+8.76
AE	$3\sqrt{2}$	+0	+1	-	-	0	0	$3\sqrt{2}$	-7.498
BF	$3\sqrt{2}$	+0	+1	-	-	0	0	$3\sqrt{2}$	-7.498
BD	$3\sqrt{2}$	+1	+0	-	-	$3\sqrt{2}$	0	0	-12.996
CE	$3\sqrt{2}$	+1	+0	-	-	$3\sqrt{2}$	0	0	-12.996
			Σ	1.908×10^{-3}	1.272×10^{-3}	$6+6\sqrt{2}$	1.5	$6+6\sqrt{2}$	

Now,

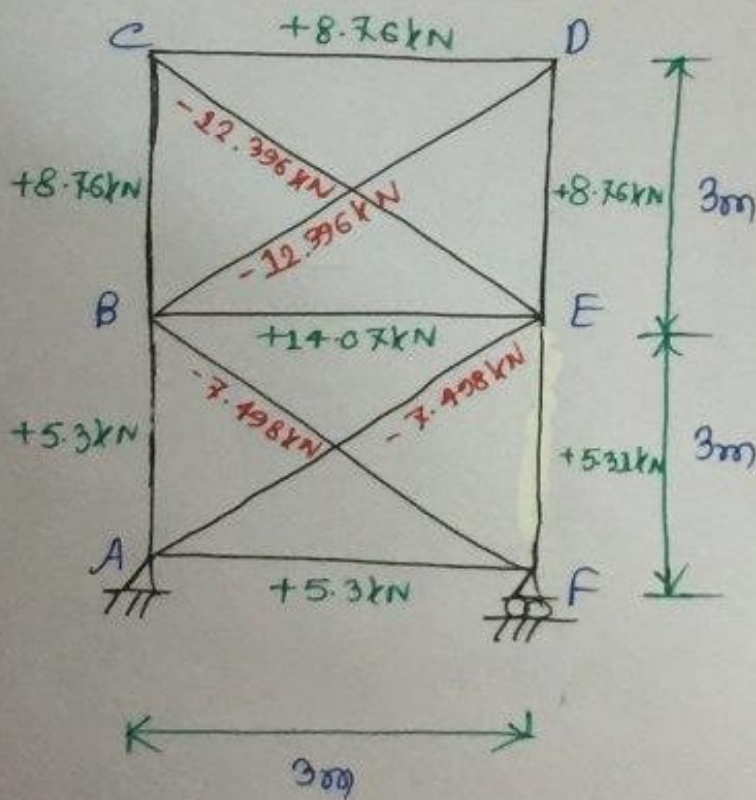
$$\begin{pmatrix} \Delta_1 \\ \Delta_2 \end{pmatrix} = \begin{pmatrix} \Delta_{10} \\ \Delta_{20} \end{pmatrix} + \begin{pmatrix} \delta_{11} & \delta_{12} \\ \delta_{21} & \delta_{22} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}$$



$$\text{or, } \begin{pmatrix} 0 \\ 0 \end{pmatrix} = \begin{pmatrix} 1.908 \times 10^{-3} \\ 1.272 \times 10^{-3} \end{pmatrix} + \begin{pmatrix} \frac{6+6\sqrt{2}}{20^5} & \frac{1.5}{20^5} \\ \frac{1.5}{20^5} & \frac{6+6\sqrt{2}}{20^5} \end{pmatrix} \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}$$

By solving the matrix, we get,

$$X_1 = -12.396 \text{ kN} \quad \& \quad X_2 = -7.498$$

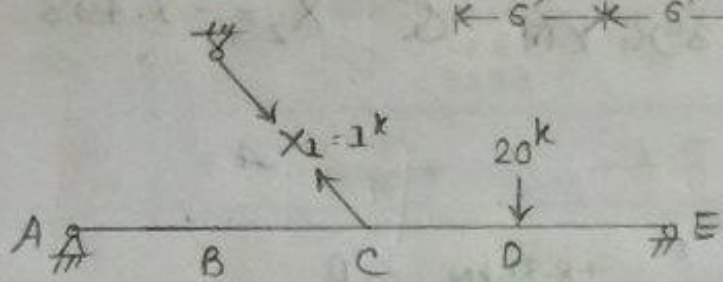
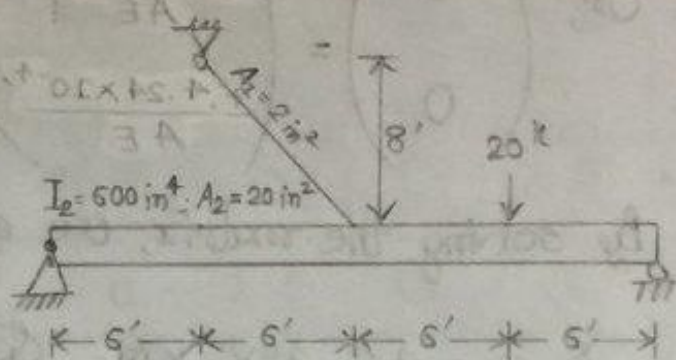


Composite Structure

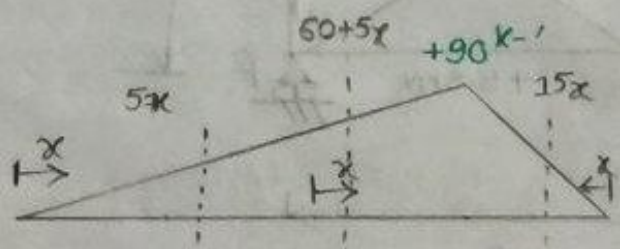
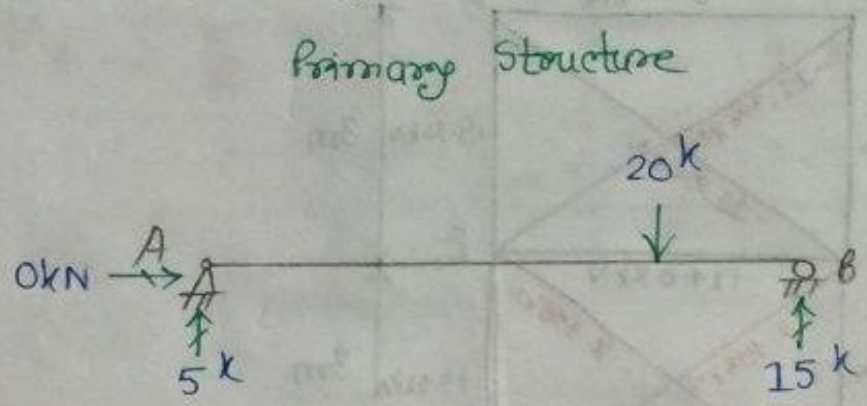
Example 9.8: Compute the force in the tie rod of this structure.

Solⁿ: Here, $D^{\circ} = (2+1+1) - 1$
 $= 1^{\circ}$

Cut the tie rod and select its bar force as **redundant**.



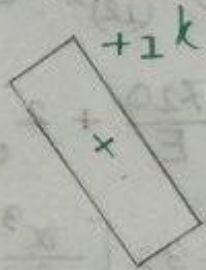
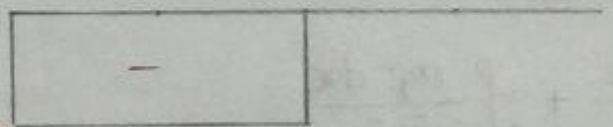
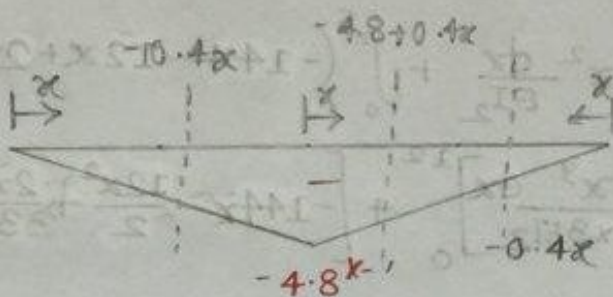
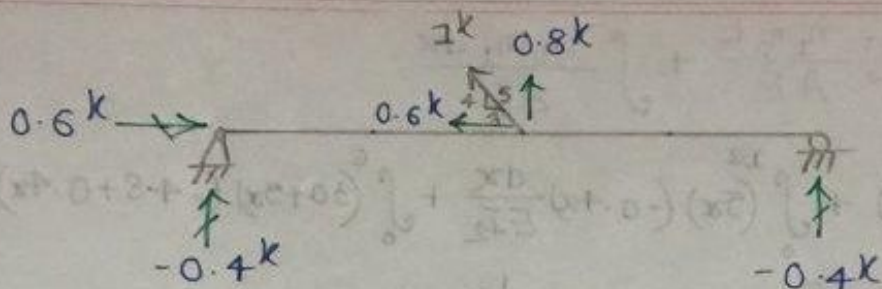
Primary Structure



m_0

n_0

+0 k



m_1 (cable)

m_1 (cable)

$$\begin{aligned}
\text{Now, } \Delta_{10} &= \sum \frac{n_1 n_0 L}{AE} + \int \frac{m_0 m_1 dx}{EI} \\
&= 0 + \int_0^{12} (5x)(-0.4x) \frac{dx}{EI_2} + \int_0^6 (60+5x)(-48+0.4x) \frac{dx}{EI_2} \\
&\quad + \int_0^6 (15x)(-0.4x) \frac{dx}{EI_2} \\
&= \int_0^{12} -2x^2 \frac{dx}{EI_2} + \int_0^6 (-288 - 0.4x + 2x^2) \frac{dx}{EI_2} + \int_0^6 (-6x^2) \frac{dx}{EI_2} \\
&= \left[-\frac{2x^3}{3EI_2} \right]_0^{12} + \left[-288x + \frac{2x^3}{3} \right]_0^6 \frac{1}{EI} + \left[-\frac{6x^3}{3EI_2} \right]_0^6 \\
&= \frac{1}{EI_2} \times \left[-\frac{2(12)^3}{3} - 288(6) + \frac{2(6)^3}{3} - 2(6)^3 \right] \\
&= -\frac{3168}{EI_2}
\end{aligned}$$

$$\begin{aligned}
\delta_{11} &= \sum \frac{n_1^2 L}{AE} + \int \frac{m_1^2 dx}{EI} \\
&= \frac{(-0.6)^2 \times 12}{\frac{20}{(12)^2} \times E} + \frac{(1)^2 \times 10}{\frac{2}{(12)^2} \times E} + 2 \int_0^{12} (-0.4x)^2 \frac{dx}{EI_2} \\
&= \frac{31.104}{E} + \frac{720}{E} + 2 \int_0^{12} 0.16x^2 \frac{dx}{EI_2} \\
&= \frac{751.104}{E} + 0.32 \left[\frac{x^3}{3} \right]_0^{12} \frac{1}{EI_2} \\
&= \frac{751.104}{E} + \frac{0.32}{3} (12)^3 \cdot \frac{1}{E \times I_2}
\end{aligned}$$

$$\Rightarrow EI_2 \delta_{11} = 751.104 I_2 + 184.32$$

$$= 751.104 \times \frac{600}{(12)^4} + 184.32$$

$$\delta_{11} = \frac{206.0533}{EI_2}$$

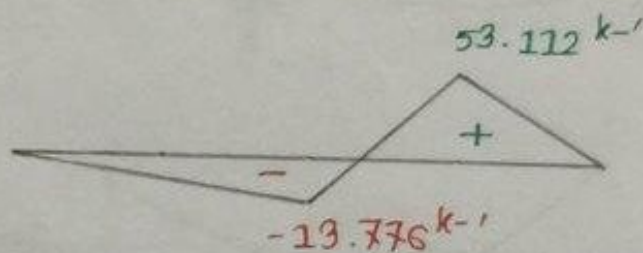
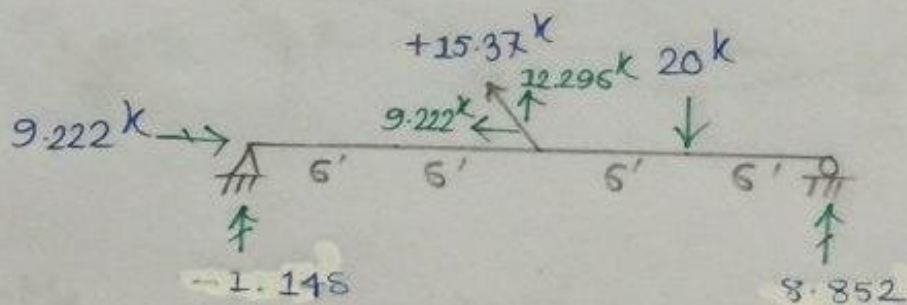
Now,

$$\Delta_1 = \Delta_{10} + \delta_{11} X_1$$

$$\Rightarrow 0 = -\frac{3168}{EI_2} + \frac{206.0533}{EI_2} X_1$$

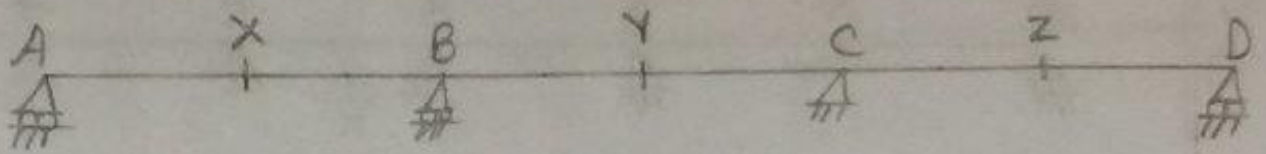
$$\therefore X_1 = +15.37 \text{ k}$$

(Ans.)

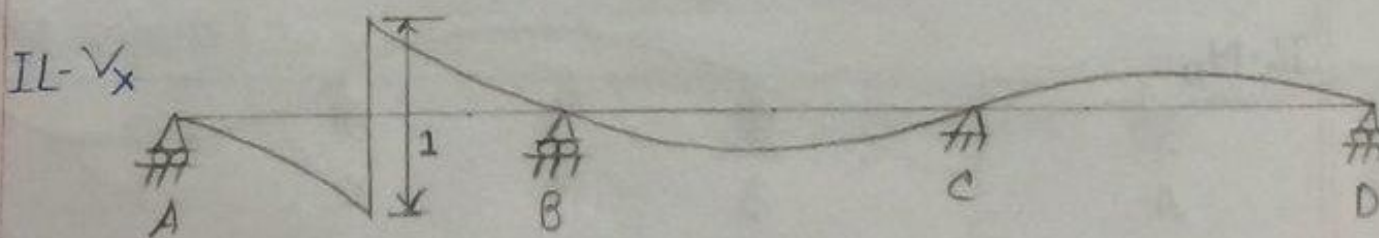
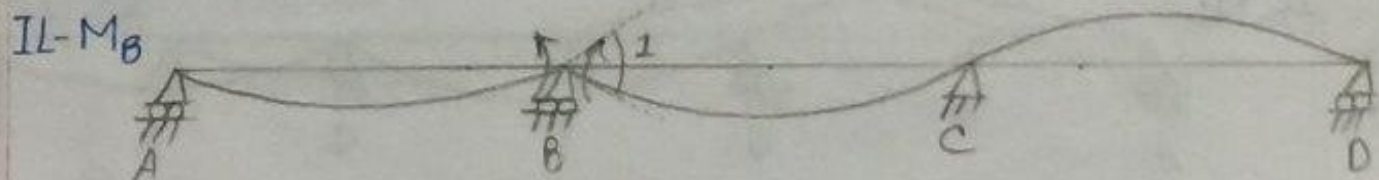
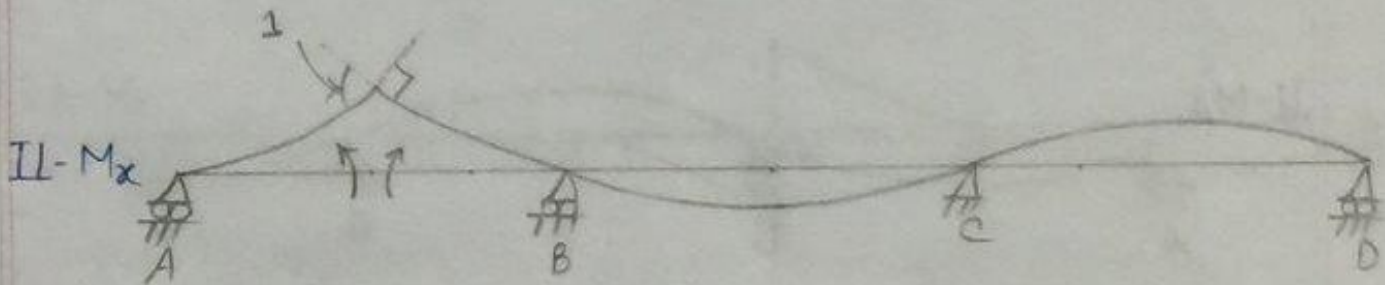
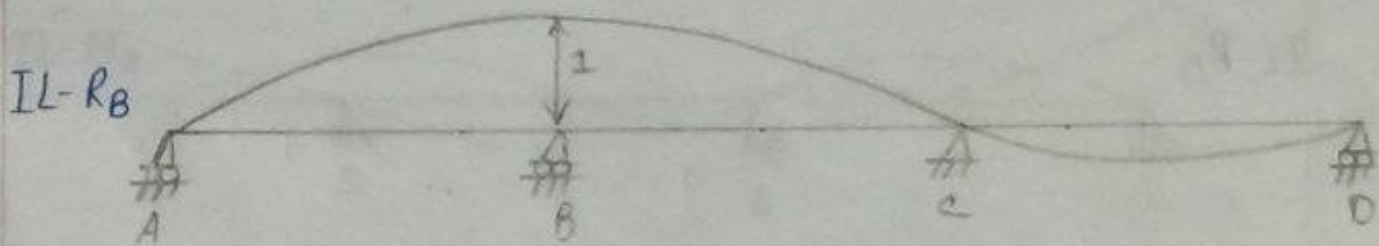
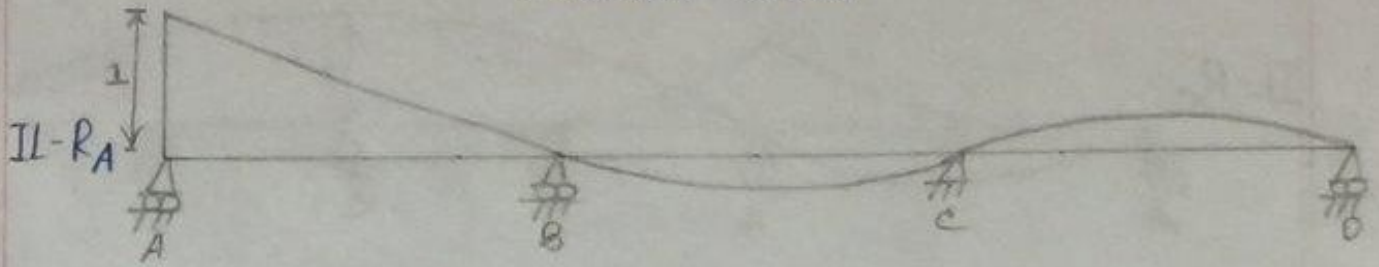


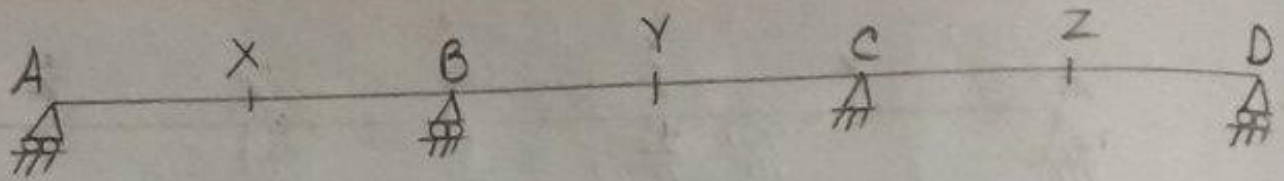
BMD

Qualitative Influence Lines for Statically Indeterminate Structures

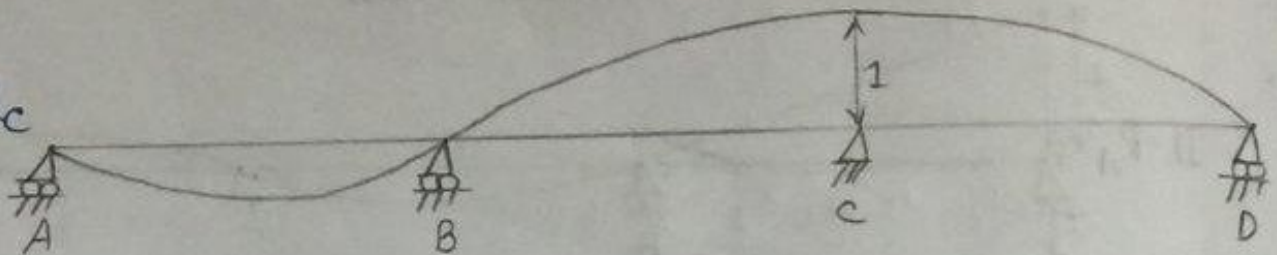


Continuous Beam

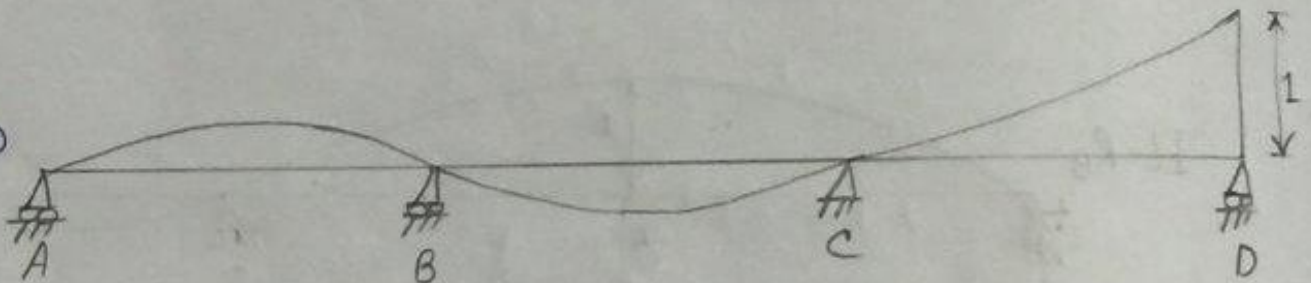




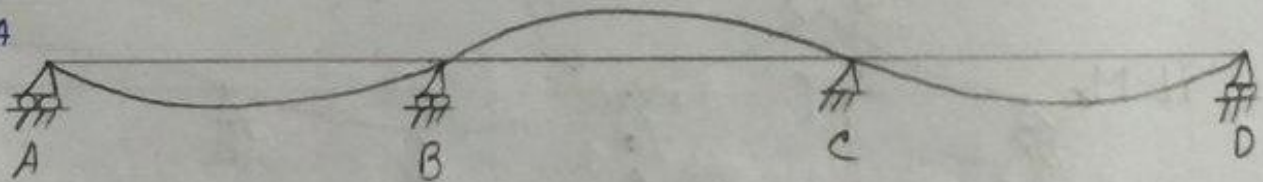
IL- R_c



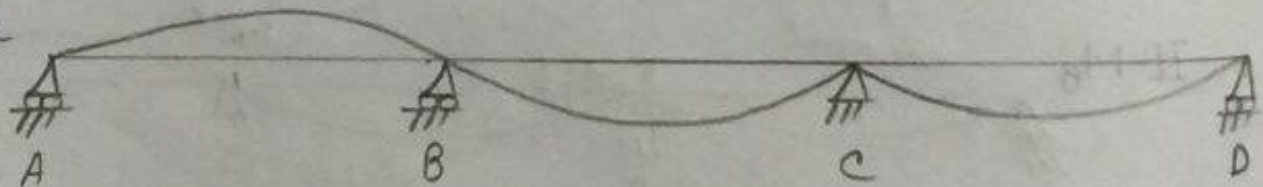
IL- R_D



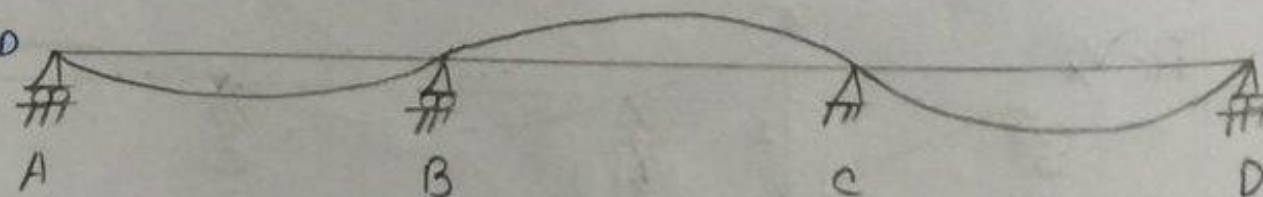
IL- M_A



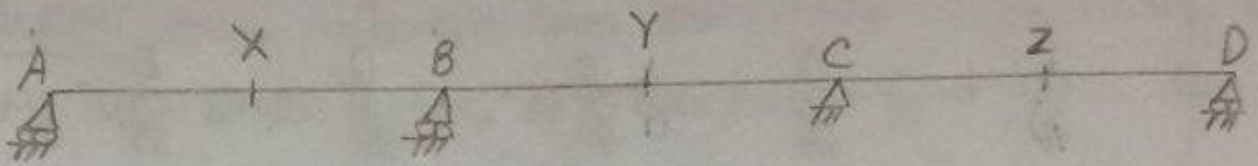
IL- M_c



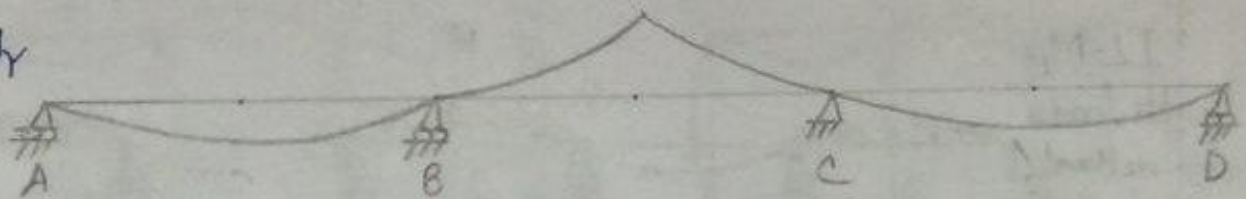
IL- M_D



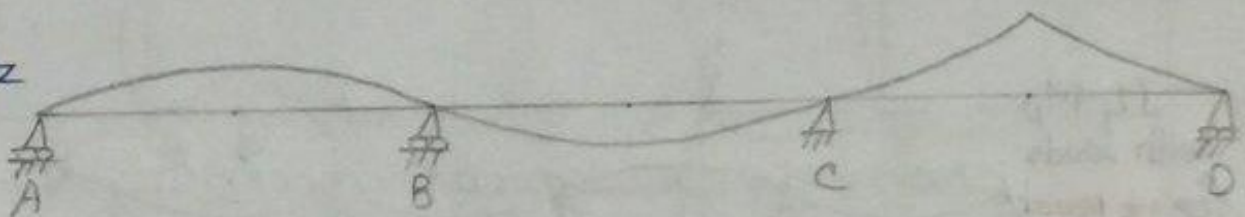
Qualitative influence lines for beam



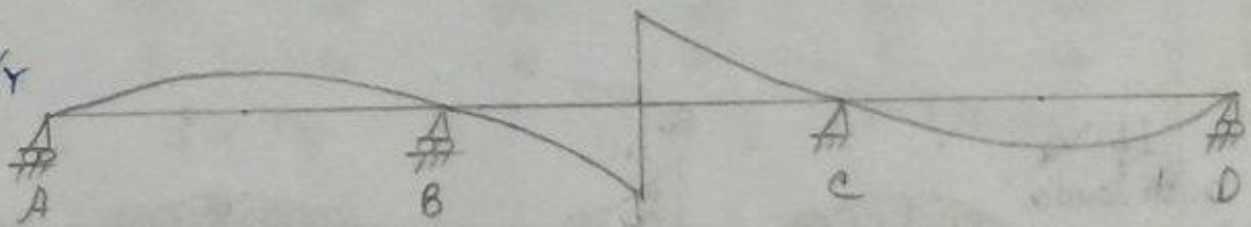
IL- M_y



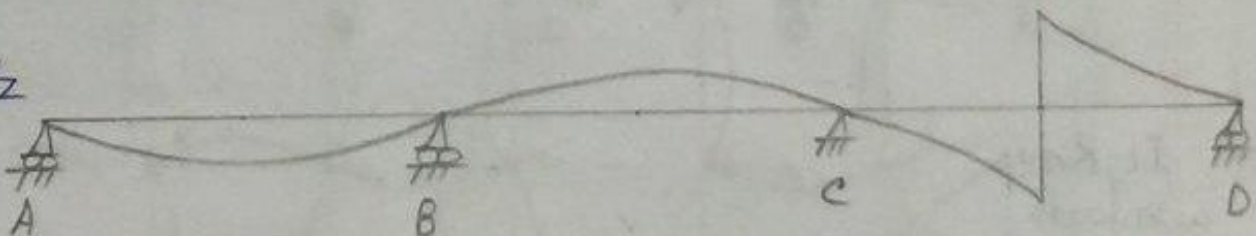
IL- M_z



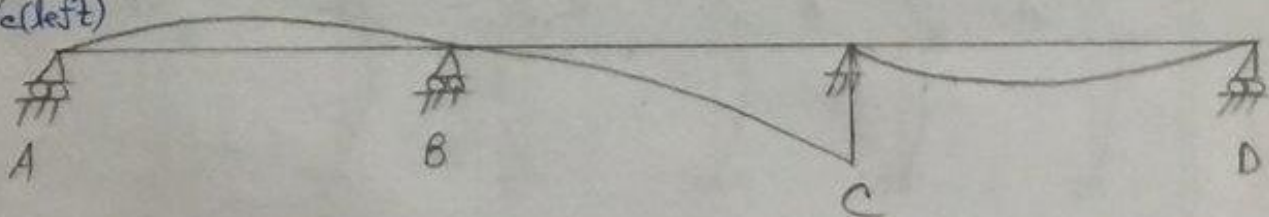
IL- V_y



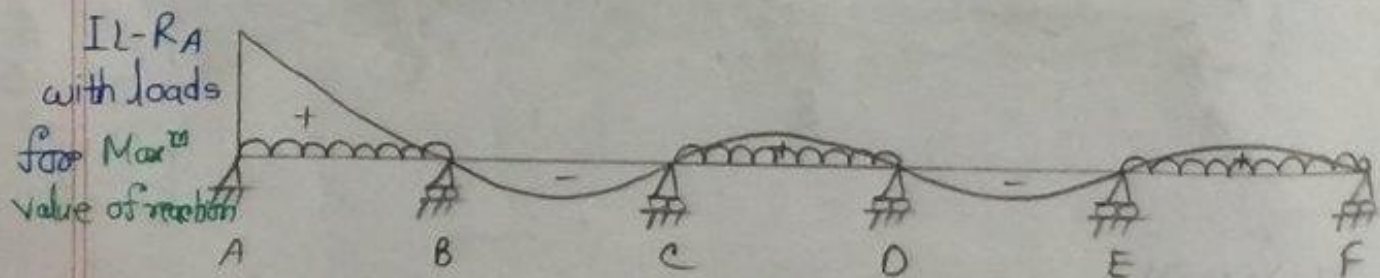
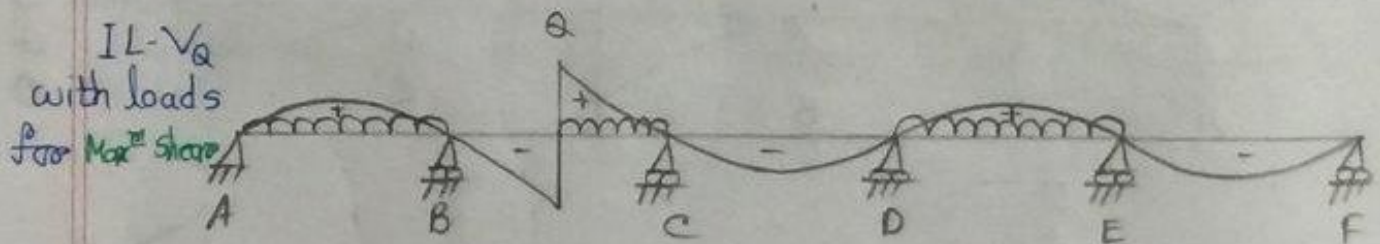
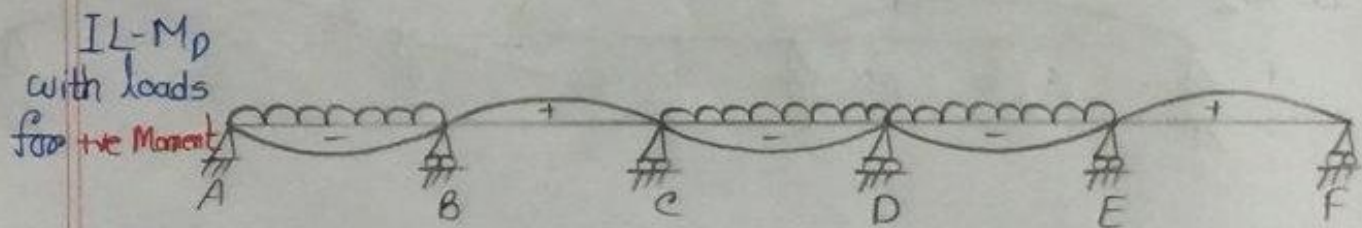
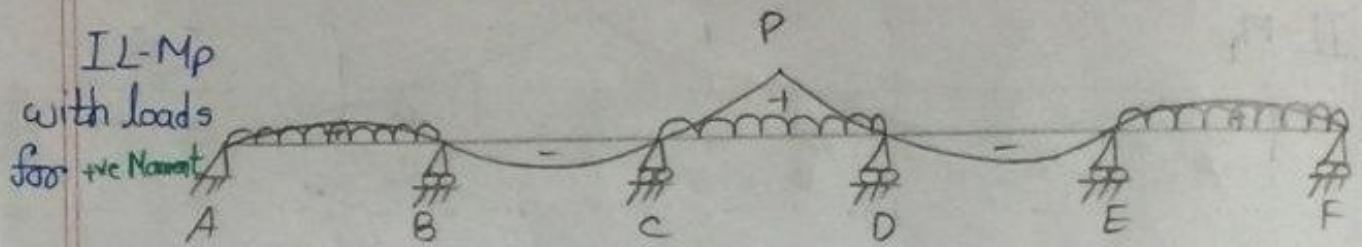
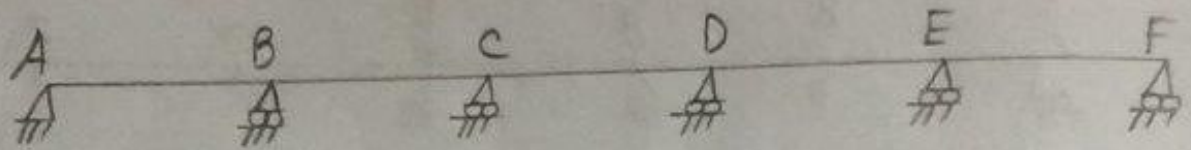
IL- V_z



IL- $V_c(\text{left})$



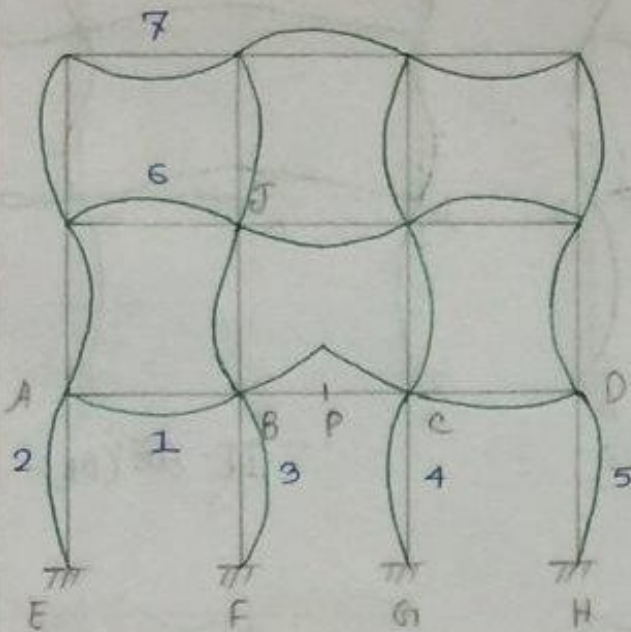
Qualitative Influence Lines & Load Patterns



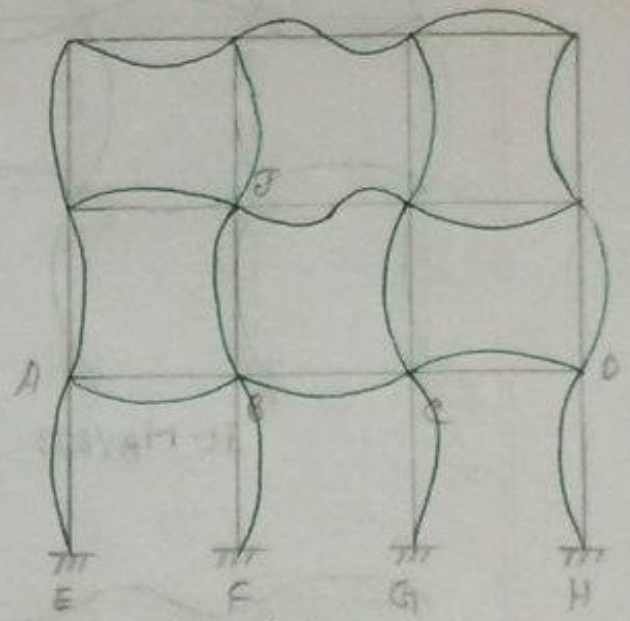
FRAMES

PROBLEM: Draw influence lines for (i) M_p , (ii) M_B of Beam BC (iii) M_B of Beam BA (iv) M_B of Column BF (v) M_B of column BT (vi) Axial force in column BF (vii) V_p

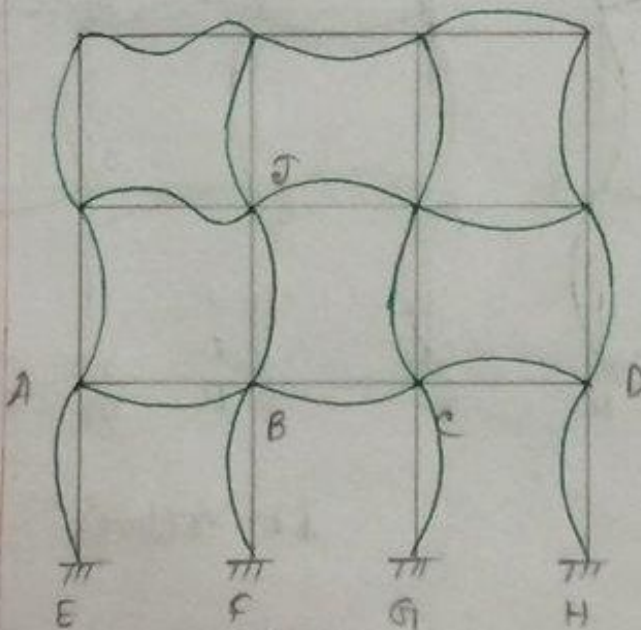
Note:
Sequence
for drawing
IL-1-2
~3-4-5
~6-7



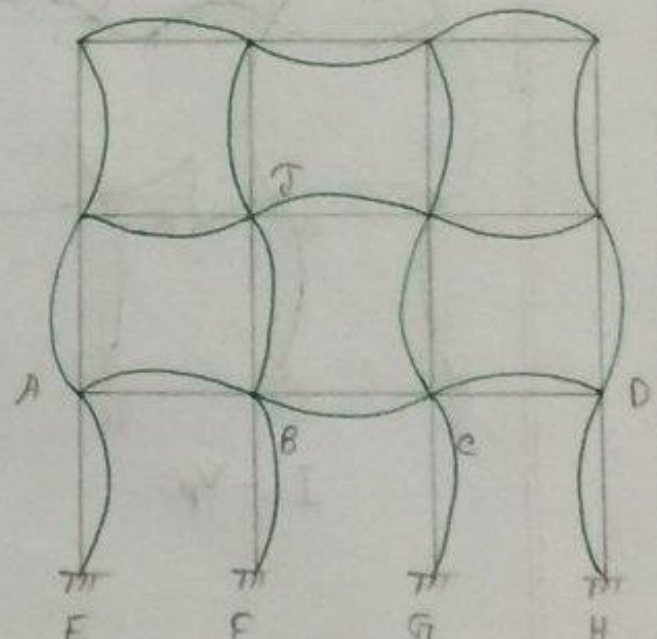
IL - M_p



IL - M_B (bc)

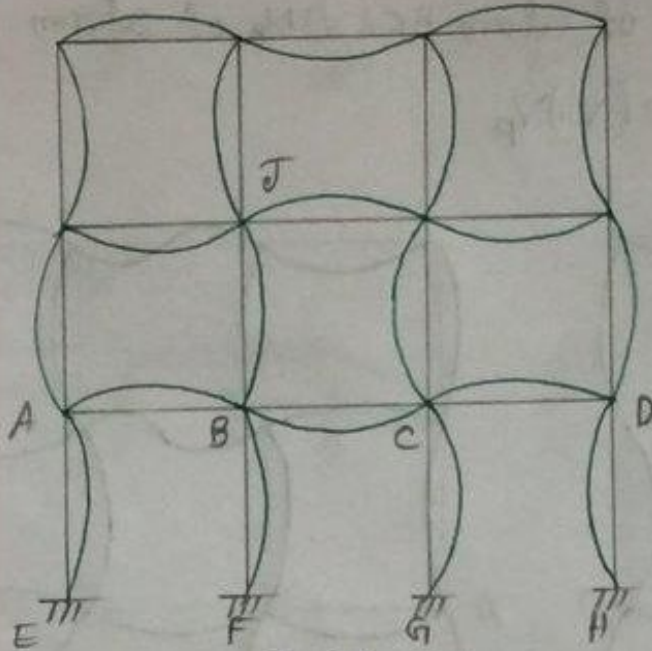


IL - M_B (BA)

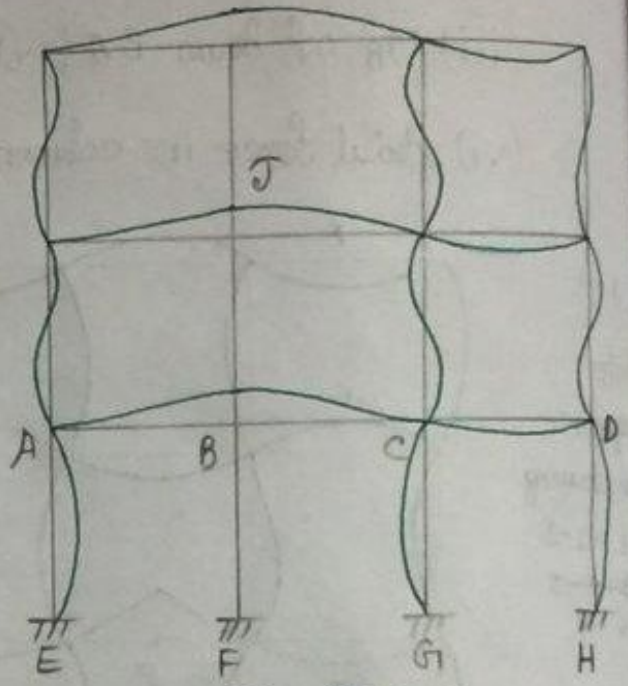


IL - M_B (BF)

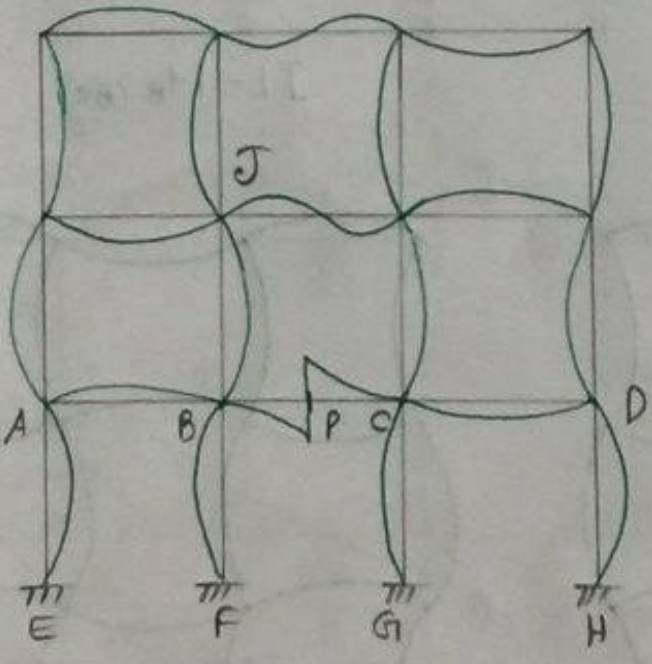
FRAMES



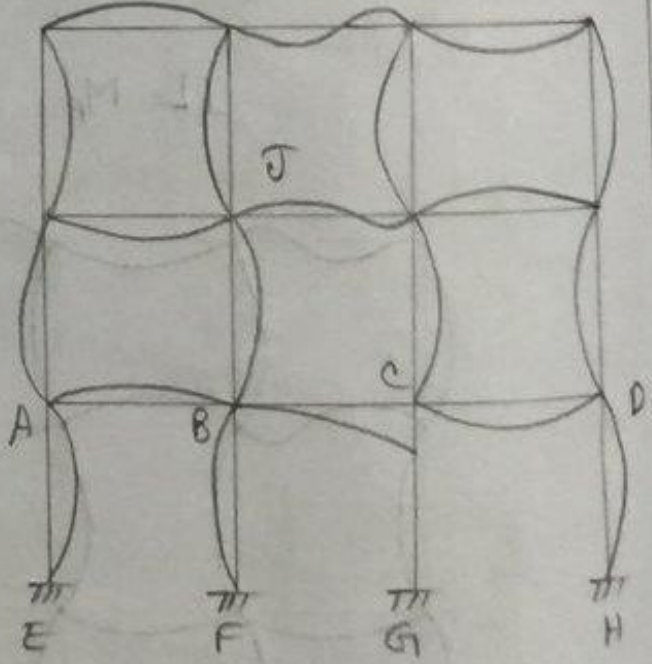
IL-M_B(BJ)



IL-AE(BF)



IL-V_P

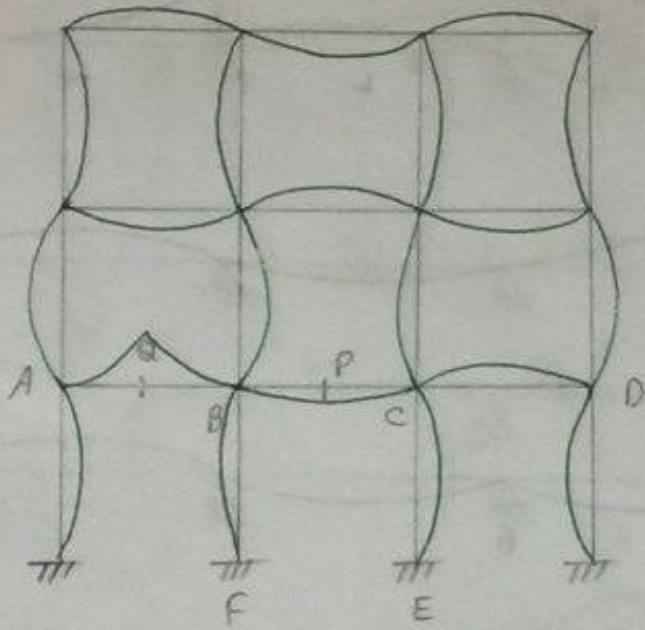


IL-V_c(left)

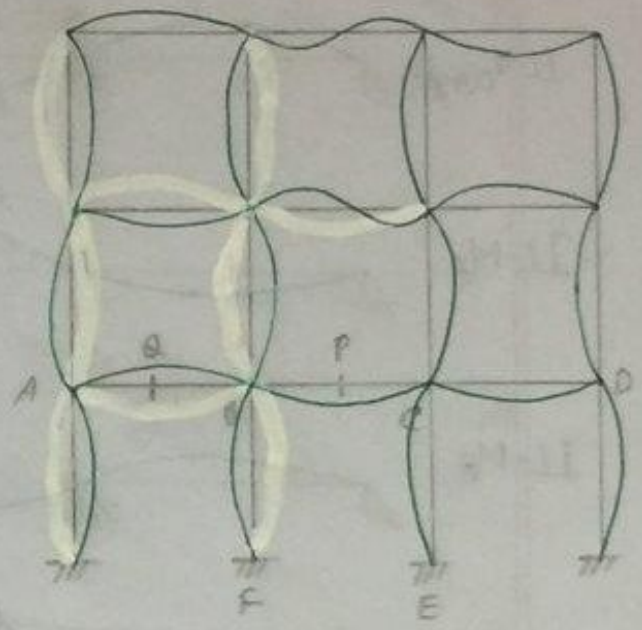
Question Paper Solutions

"2014-15"

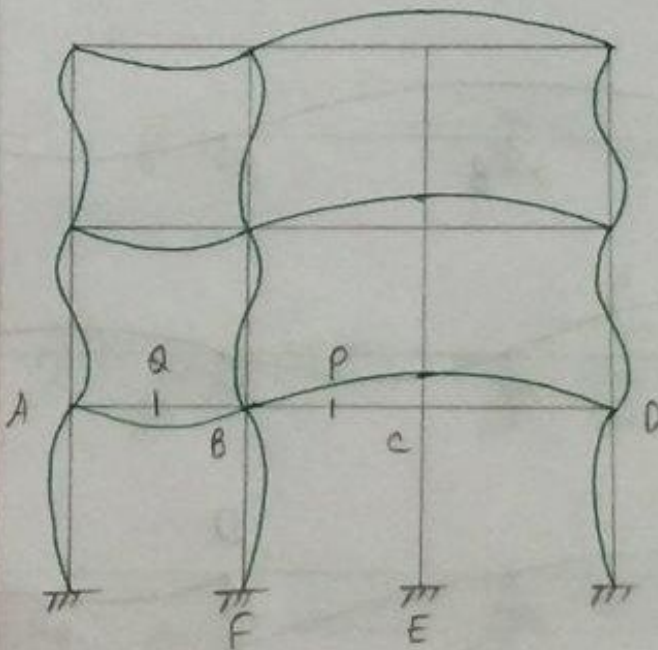
2.(b)



IL-M_a



IL-M_c(bc)



IL-A_F(CE)

7. (b)

