

Quality of Water

Pure Water: It is a chemical compound H_2O

Potable Water: Water which is fit for drinking no matter how it tastes or looks.

Palatable Water: Not only safe for drinking but also free from objectionable tastes, odors, colors and turbidity. Aesthetically looks good

Wholesome Water: Chemically may not pure but doesn't contain anything harmful to human beings.

Mineral Water: It contains useful minerals like calcium, magnesium & iron in required proportions.

Following are the requirements of potable or wholesome water for domestic use -

- (i) It should be clear, odorless & colorless.
- (ii) It should be free from harmful & disease producing bacteria
- (iii) It should be free from all objectionable substances.

- (4) It should be fresh & cool
- (5) It should be palatable i.e. aesthetically attractive
- (6) It should be tasty
- (7) It should not cause corrosion to the pipes & other fittings.

Characteristics of Water

Physical characteristics:

(1) Turbidity:

⇒ Turbidity is the measure of resistance to the passage of light through water.

⇒ It is caused by suspended materials such as clay, silt or some other finely divided organic & inorganic matter.

Turbidity is also due to presence of bacteria, algae, protozoa, fungi etc.

Jackson Turbidity Unit (JTU) →

→ Used to measure high turbidity (>25ppm)

Nephelometric Turbidity Unit (NTU)

→ Small turbidity (even smaller than one) can be measured. Hence used for domestic water supply

→ based on scattering light principle

Formazin Turbidity Units (FTU)

→ Same as NTU &

→ when formazin was initially adopted as the primary reference standard then FTU is used.

(ii) Color:

⇒ It is caused by dissolved organic matter from decaying vegetation or some inorganic colored soils, growth of algae, metallic ions

(Fe & Mn)

⇒ Iron (Fe) gives reddish & Mn gives brown or blackish color

(iii) Taste & Odor:

⇒ due to dissolved organic matter or inorganic salts, dissolved gases (H_2S , Methane etc)

⇒ Taste measurement unit = Flavor Threshold Number (FTN)

⇒ Odor measurement Unit = Threshold Odor Number (TON)

(iv) Temperature: $10^\circ C$ is desirable for drinking water

(5) Specific conductivity: To know the dissolved salt content.

Chemical Properties:

(i) Total Solids, Suspended Solids & dissolved Solids:

⇒ Total solids can be found by evaporating a sample of water and weighing the dry residue left

⇒ Suspended solids can be found by filtering water sample. SS comes from inorganic particles like SiO_2

silt, clay, oils & organic particles

⇒ Total dissolved solids (TDS) = TS - SS

⇒ Sources of Total dissolved solids -

Major
Na, Ca, Mg, HCO_3^- , SO_4^{2-} ,
 Cl^-

Minor
Fe, K, CO_3^{2-} , NO_3^- ,
Fluoride, Boron, Silica

(ii) pH value

⇒ It indicates hydrogen ion concentration in water

⇒ $\text{pH} = \log \left[\frac{1}{\text{H}^+} \right] = -\log [\text{H}^+]$; where $[\text{H}^+]$ is in moles/litre

⇒ Permissible limit of pH = 6.5 to 8.5

⇒ If $\text{pH} > 7$ it is alkaline, If $\text{pH} < 7$ it is acidic

⇒ $\text{pOH} = -\log [\text{OH}^-] = \log \left[\frac{1}{\text{OH}^-} \right]$

$\text{pH} + \text{pOH} = 14$; $[\text{H}^+] \times [\text{OH}^-] = 10^{-14}$

(iii) Alkalinity: is the ability to neutralise acids of the solution

⇒ Most common constituents of alkalinity are

CO_3^{2-} , HCO_3^- , OH^- → [very rare, not considered in practical calculation]

⇒ effects of alkalinity

→ Incrustation & sediment deposition in pipe line.

→ difficulties in chlorination

⇒ Alkalinity is calculated as amount of CaCO_3 in mg/l or ppm

⇒ if amount of CaCO_3 is not given,

Total alkalinity, TA

$$= \left[\text{HCO}_3^- (\text{mg/L}) \times \frac{\text{equivalent wt. of CaCO}_3}{\text{equivalent wt. of HCO}_3^-} \right]$$

$$+ \left[\text{CO}_3^{2-} (\text{mg/L}) \times \frac{\text{eq. wt. of CaCO}_3}{\text{eq. wt. of CO}_3^{2-}} \right]$$

$$= \text{HCO}_3^- (\text{mg/L}) \times \frac{50}{61} + \text{CO}_3^{2-} \times \frac{50}{30}$$

*** equivalent weight = $\frac{\text{molecular weight}}{\text{valance}}$

$$\text{equi. weight of CaCO}_3 = \frac{100}{2} = 50$$

$$\text{eq. wt. of HCO}_3^- = \frac{61}{1} = 61$$

*** Equivalent weights of different matter

~~CaCO₃ = 100~~; $\text{CaCO}_3 = 50$, $\text{CO}_3^{2-} = 30$,
 $\text{HCO}_3^- = 61$, ~~CaCO₃ = 100~~ $\text{Ca}^{++} = 20$, $\text{Mg}^{++} = 12$,

*** Molecular weights of different matter

$$\text{Ca}^{++} = 40, \text{Mg}^{++} = 24, \text{OH}^- = 17$$

(iv) Hardness

⇒ A characteristics which prevents formation of lather or foam with soap

⇒ Effects of hardness

- scaling of boilers
- greater soap consumption
- corrosion & incrustation of pipe lines
- food becomes tasteless

⇒ Type of hardness carbonate hardness (CH)
 Non-carbonate hardness (NCH)

*** ⇒ Temporary / Carbonate Hardness

→ Caused by HCO_3^- (bicarbonate) & CO_3^{2-} (carbonate) of Ca & Mg

→ can be removed by boiling / addition of lime. That's why it is called temporary hardness.

*** ⇒ Permanent / Non-carbonate Hardness

→ Caused by SO_4^{2-} , Cl^- , NO_3^- of Ca & Mg

→ water softening methods are required to remove

⇒ Hardness is measured in terms of ppm or mg/litre of CaCO_3

⇒ Total Hardness, TH = $\left[\text{Ca}^{++}(\text{mg/L}) \times \frac{\text{eq. wt. of CaCO}_3}{\text{eq. wt. of } \text{Ca}^{++}} \right]$
 $+ \left[\text{Mg}^{++}(\text{mg/L}) \times \frac{\text{eq. wt. of CaCO}_3}{\text{eq. wt. of } \text{Mg}^{++}} \right]$
 $= \text{Ca}^{++}(\text{mg/L}) \times \frac{50}{20} + \text{Mg}^{++}(\text{mg/L}) \times \frac{50}{12}$

$$\Rightarrow TH = CH + NCH$$

If $TH > \text{alkalinity}$, then $CH = \text{alkalinity}$

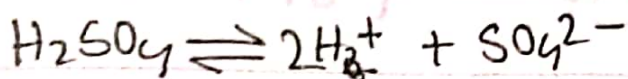
$$\therefore NCH = TH - \text{alkalinity (TA)}$$

If $TH \leq \text{alkalinity}$, then $CH = TH$

$$NCH = 0$$

* If 100mg of H_2SO_4 is added to 1L of water, what is the final pH? [NPCBL'19]

Solⁿ: H_2SO_4 concentration = $\frac{100 \times 10^{-3} g}{98 g} = 0.00102 \text{ mol/L}$



molar ratio, $H_2SO_4 : H_3O^+ = 1 : 2$

$$\therefore [H^+] = [2 \times 0.00102] = [0.00204]$$

$$\therefore pH = -\log [0.00204] = 2.69 \quad \underline{\underline{A}}$$

* If $[H_3O^+] = 7.1 \times 10^{-2} M$, calculate the $[OH^-]$ concentration.

$$pH = -\log (7.1 \times 10^{-2}) = 1.149$$

$$\therefore pOH = 14 - 1.149 = 12.851$$

$$[OH^-] = 10^{-pOH} = 10^{-12.851} = 1.41 \times 10^{-13} M$$

again, $[H_3O^+][OH^-] = 10^{-14}$ [for water]

$$\Rightarrow [OH^-] = \frac{10^{-14}}{7.1 \times 10^{-2}} = 1.41 \times 10^{-13} M$$

* If $\text{pH} = 9.5$, what is the $[\text{OH}^-]$ concentration? [PGCB'19]

Solⁿ

$$\text{pH} + \text{pOH} = 14$$

$$\Rightarrow \text{pOH} = 14 - 9.5 = 4.5$$

$$[\text{OH}^-] = 10^{-\text{pOH}} = 10^{-4.5} = 0.03 \times 10^{-3} \text{ M}$$

↓
mole

* The $[\text{OH}^-]$ is 10^{-4} mole/l concentration. is given, find the pH 10 [GTCL'16]

Solⁿ $[\text{OH}^-] = 10^{-\text{pOH}}$

$$\Rightarrow 10^{-4} = 10^{-\text{pOH}}$$

$$\Rightarrow \therefore \text{pOH} = 4$$

$$\text{pH} + \text{pOH} = 14 \quad \therefore \text{pH} = 14 - 4 = 10 \quad \text{A}$$

* The measured pH values of incoming and outgoing water at a water treatment plant are 7.3 and 8.5 respectively. What is the average pH of water, assuming a linear variation of pH with time?

[CAAB 2022]

$[H^+]$ of incoming water, $[H^+]_i = 10^{-7.3}$

$[H^+]$ of outgoing water $[H^+]_o = 10^{-8.5}$

$$\therefore [H^+]_{avg} = \frac{10^{-7.3} + 10^{-8.5}}{2} = 2.664 \times 10^{-8}$$

$$\therefore pH_{avg} = -\log [2.664 \times 10^{-8}] = 7.574$$

~~Q2~~ (2) For a water sample, the total alkalinity is 200 mg/l as CaCO_3 . The Ca^{2+} is 120 mg/l, Mg^{2+} is 60 mg/l. What is total hardness, carbonate hardness, Non-carbonate hardness. [DNCC'20]

Solⁿ: Given, $\text{TA} = 200 \text{ mg/l}$

$$\begin{aligned} \text{TH} &= \text{Ca}^{2+} * \frac{50}{20} + \text{Mg}^{2+} * \frac{50}{12} \\ &= 120 * \frac{50}{20} + 60 * \frac{50}{12} = 550 \text{ mg/l as CaCO}_3 \end{aligned}$$

$\therefore \text{TH} > \text{TA}$

$$\text{CH} = \text{TA} = 200 \text{ mg/l as CaCO}_3$$

$$\text{NCH} = \text{TH} - \text{CH} = 550 - 200 = 350 \text{ mg/l as CaCO}_3$$

* In a water sample, the concentrations of Ca^{2+} , Mg^{2+} and HCO_3^- are 100mg/L , 36mg/L and 122mg/L respectively. Calculate the total hardness and the temporary (carbonate) hardness.

Solⁿ: Total hardness = $\text{Ca}^{2+} * \frac{50}{20} + \text{Mg}^{2+} * \frac{50}{12}$

$$= 100 * \frac{50}{20} + 36 * \frac{50}{12}$$

$$= 400\text{mg/L as CaCO}_3$$

$$\text{Total Alkalinity} = \text{HCO}_3^- * \frac{50}{61} = 122 * \frac{50}{61} = 100\text{mg/L}$$



$$\therefore \text{Temporary (Carbonate) Hardness} \equiv \text{TA} = 100\text{mg/L}$$

$$\therefore \text{Non-carbonate hardness} = 400 - 100 = 300\text{mg/L as CaCO}_3$$

(3) The chemical analysis of water sample indicates the presence of cations as follows -

$$\text{Na}^+ = 20 \text{ mg/L}, \text{Ca}^{2+} = 45 \text{ mg/L}, \text{Mg}^{2+} = 60 \text{ mg/L},$$

$$\text{HCO}_3^- = 248 \text{ mg/L}, \text{SO}_4^{2-} = 220 \text{ mg/L}, \text{Cl} = 79.2 \text{ mg/L}$$

Compute, TH, CH, NCH (equivalent to CaCO_3).

Solⁿ:

$$\text{Alkalinity} = \text{HCO}_3^- \times \frac{50}{61}$$

[এখন CO_3^{2-} এর
নাই, তাই শুধু
আলকালি হিসাব করি]

$$= 248 \times \frac{50}{61}$$

$$= 203.3 \text{ mg/L as } \text{CaCO}_3$$

$$\text{TH} = \text{Ca}^{2+} \times \frac{50}{20} + \text{Mg}^{2+} \times \frac{50}{12}$$

$$= 45 \times \frac{50}{20} + 60 \times \frac{50}{12} = 362.5 \text{ mg/lit as } \text{CaCO}_3$$

TH > Alkalinity

$$\therefore \text{CH} = \text{Alkalinity} = 203.3 \text{ mg/lit as } \text{CaCO}_3$$

$$\text{NCH} = 362.5 - 203.3$$

$$= 159.2 \text{ mg/L as } \text{CaCO}_3$$

* meq = milliequivalent

mg/L = meq/L * equivalent weight.

(7) Laboratory test shows $Ca^{2+} = 40 \text{ mg/L}$.

Total carbonate hardness = 3 meq/L. Assume carbonate hardness only due to HCO_3^- .

Non carbonate hardness = 1 meq/L.

Determine total hardness, Mg^{2+} & HCO_3^- as mg/L. [BWDB'19]

Solⁿ: $TH = CH + NCH$
 $= 3 + 1 = 4 \text{ meq/L}$
 $= 4 \times 50 \text{ mg/L of } CaCO_3$
 $= 200 \text{ mg/L of } CaCO_3$

HCO_3^- alkalinity = CH
 $= 3 \text{ meq/L}$
 $= 3 \times 50 \text{ mg/L of } CaCO_3$
 $= 150 \text{ mg/L of } CaCO_3$

$$TH = Mg^{2+} * \frac{50}{12} + Ca^{2+} * \frac{50}{20}$$

$$\Rightarrow 200 = Mg^{2+} * \frac{50}{12} + 40 * \frac{50}{20}$$

$$\Rightarrow Mg^{2+} * \frac{50}{12} = 100$$

$$\therefore Mg^{2+} = 24 \text{ mg/L}$$

(8) Alkalinity of a water sample is 200 mg/L as CaCO_3 . The sample has 160 mg/L of Ca^{2+} & 40 mg/L of Mg^{2+} . The pH is 8.1 . Find TH, CH, NCH (PGCB'19)

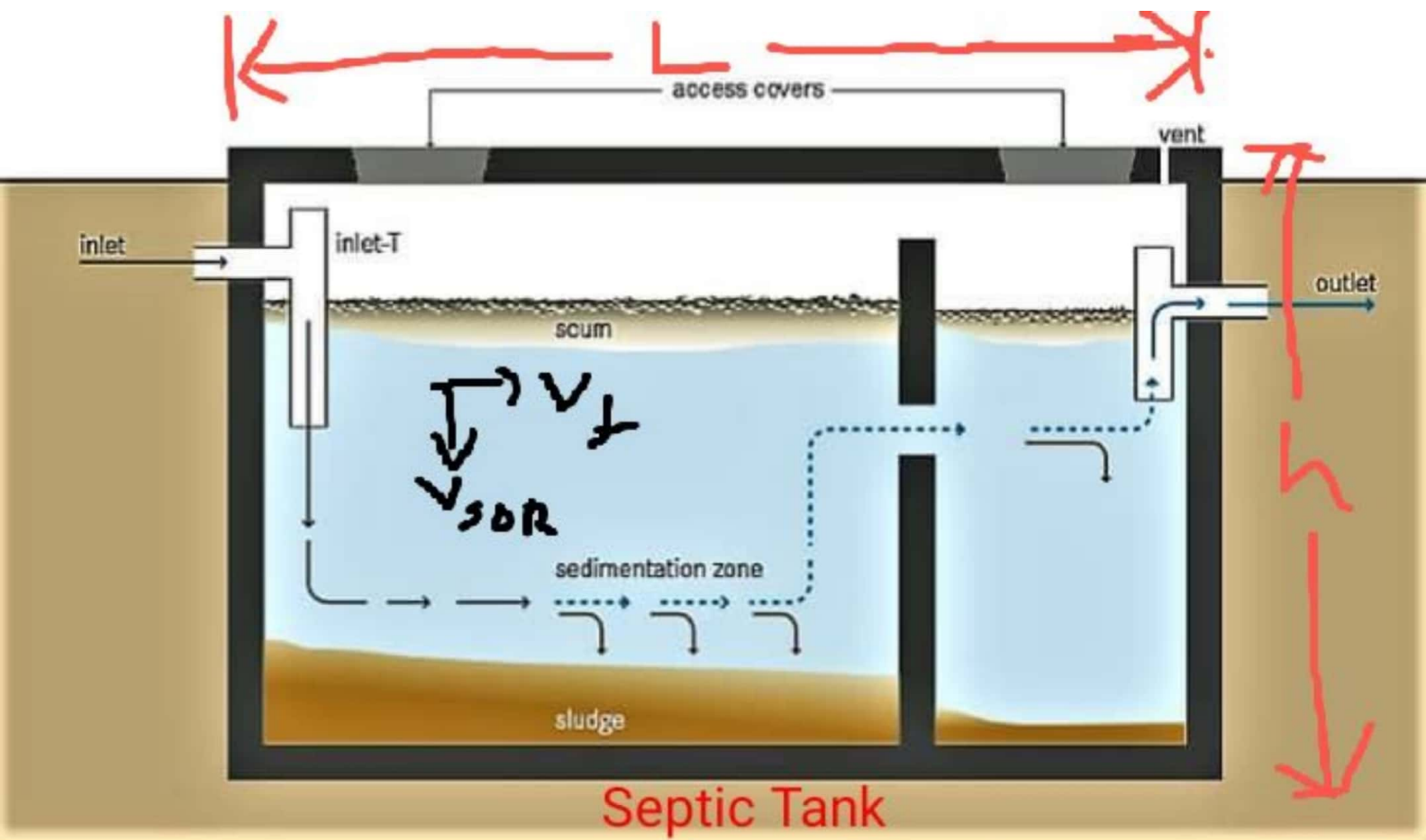
Solⁿ:

$$\begin{aligned} \text{TH} &= \text{Ca}^{2+} * \frac{50}{20} + \text{Mg}^{2+} * \frac{50}{12} \\ &= 160 * \frac{50}{20} + 40 * \frac{50}{12} \\ &= 564 \text{ mg/L as } \text{CaCO}_3 \end{aligned}$$

$\text{TH} > \text{Alkalinity}$

$$\therefore \text{CH} = \text{Alkalinity} = 200 \text{ mg/L as } \text{CaCO}_3$$

$$\therefore \text{NCH} = 564 - 200 = 364 \text{ mg/L as } \text{CaCO}_3$$



Septic Tank

B = width of the tank

V_s = Settling Velocity

Approach

Flow velocity, $v_f = \frac{Q}{BH}$

Surface loading / overflow rate,

$$v_{SOR} = \frac{Q}{BL}$$

if settling velocity $v_s \geq v_{SOR}$, then the particle can be removed (i.e. as sludge) from water.

If $v_s < v_{SOR}$, will not get 100% removed.

\therefore sedimentation efficiency, $\eta = \frac{v_s}{v_{SOR}} \times 100$

Detention time, D_t : Theoretical average time for which water is detained in the tank.

$$D_t = \frac{\text{Vol. of tank}}{\text{discharge}} = \frac{LBH}{Q} = \frac{H \cdot L}{\frac{Q}{L}} = \frac{H}{V_{50\%}}$$

$$\therefore \text{Length, } L = \frac{Q \times D_t}{BH} = D_t \times V_f$$

* In order to increase the efficiency, the D_t should be increased, therefore smaller size of particles can also be settled.

(BUET) million gallon per day
 (4) ~~1 MGD~~ water passage through a sedimentation tank of 50' x 20' x 10'. Find detention time.

Solⁿ: $T = \frac{BLH}{Q}$

$$\boxed{1 \text{ gallon} = 7.46 \text{ ft}^3} = \frac{50 \times 20 \times 10}{134.05 \times 10^3} = 0.0746 \text{ days} = 1.8 \text{ hr}$$

$$\begin{aligned} Q &= \cancel{1 \text{ MGD}} \\ &= 10^6 \text{ L/D} \\ &= \cancel{10^3 \text{ m}^3/\text{day}} \\ &= 1 \times 10^6 \text{ gallon/day} \\ &= \frac{10^6}{7.46} \text{ ft}^3/\text{day} \\ &= 134.05 \text{ ft}^3/\text{day} \times 10^3 \end{aligned}$$

* one million gallon ~~(1000000)~~ water passes through a sedimentation tank of 50'x20'x10' size per day. what will be the detention time? [CPDC '16] [GTCL '18]

Solⁿ:

$$\text{Detention time} = \frac{50 \times 20 \times 10 \text{ ft}^3}{\frac{1 \times 10^6 \text{ ft}^3}{7.485 \times 24}} = 1.8 \text{ hr}$$

~~1 ft³ = 7.485 gallon~~

* A horizontal flow grit chamber, having flow rate 30 ft³/sec, 6ft deep, width is 15 times of its length. Approach is 1 ft/sec. Determine the width of the grit chamber. [EGCB '20] [CPGCB '21]

Solⁿ: ~~(at given depth (over on 25/3/2024))~~ [BPDB '23]

~~$$Q = AV$$~~

~~$$\Rightarrow 30 = (x \times 15x) \times 1$$~~

~~$$\Rightarrow x = 1.42 \text{ ft}$$~~

~~$$\therefore \text{Length} = 1.42 \text{ ft}; \text{Width} = 15 \times 1.42 = 21.21 \text{ ft}$$~~

* ~~1000000~~

Approach velocity, $V_a = \frac{Q}{BH}$ [width x height]

$$Q = AV$$

$$\Rightarrow 30 = 15x \times 6 \times 1$$

$$\Rightarrow x = 0.33 \text{ ft}$$

$$\therefore \text{width} = 0.33 \times 15 \text{ ft}$$

$$= 5 \text{ ft Ans}$$

Take, length is x ft

* Design a sedimentation tank for 3 hrs of detention period with discharge ~~125 lit/hr~~ 125 lit/hr, where the ratio of length, breadth & height is 1:1:3? [BWD B'13]

Solⁿ: $T = \frac{BLH}{Q}$

$$\Rightarrow 3 \times \cancel{125} = \frac{x \cdot x \cdot 3x \cdot m^3}{125 \times 10^{-3} m^3/hr}$$

$$\Rightarrow \frac{0.375}{\cancel{125}} = 3x^3$$

$$\Rightarrow x^3 = 0.125$$

$$\therefore x = 0.5$$

$$\therefore \text{length} = 0.5m, \text{breadth} = \cancel{2 \times 0.5 = 1m} = 0.5m$$

$$\text{height} = 3 \times 0.5 = 1.5m \quad \star$$

* A sample ^{waste} water plant has a raw water inflow rate of $0.6 m^3/sec$ and it has been found through experiment that all particles settle at a rate of $v_s = 0.004 m/sec$. A proposed rectangular settling tank has

$L = 20m, D = 2m,$

width = $6m$. Calculate an effective zone of

- (i) surface overflow (SOR)
- (ii) what fraction of particles expected to be removed from the tank? [SG FL'21]

(i) SOR = $\frac{0.6}{20 \times 6} = 5 \times 10^{-3} m^3/s = 18 m^3/h$

→ SOR area \times depth \times velocity

SOR is unit surface velocity \Rightarrow m/s or m/hr $[SOR = \frac{\text{discharge}}{BL} = m/s]$

$$(ii) \eta = \frac{0.004}{5 \times 10^{-3}} \approx 100\% \\ = 80\%$$

$$\text{Surface overflow} \\ = \frac{\text{discharge}}{\text{surface area (bxh)}}$$

therefore, 80% of particles expected to be removed from the tank.

* Unit of noise is expressed as dB [BPDB'21]

[BPDB '16]

(5) one million gallons of water per day (1mgd) passage through a sedimentation tank which is 20ft wide, 50ft long & 10ft deep. Find (a) Detention time (b) Average velocity of flow through basin (c) If the suspended solids content of the water averages 40ppm, what weight of dry solids will be deposited every 24 hours assuming 75% removed in the basin. d) surface overflow rate (SOR)

Solⁿ:

$$(a) D_t = \frac{20 \times 50 \times 10}{106} = 9.43 \text{ hrs} = 0.393 \text{ days}$$

$$(b) v = \frac{L}{D_t}$$

$$= \frac{50}{1.8} = 27.78 \text{ ft/hr}$$

(c) Total suspended solids = $\left(\begin{array}{l} 40 \text{ parts/million gallon} \\ \times 1 \text{ million gallon} \end{array} \right)$

$$= 40 \times 1 \times 0.75$$

$$= 30 \text{ gallons}$$

$$= \frac{30}{7.46} \text{ ft}^3$$

$$= 4.02 \text{ ft}^3 \times \frac{2.65 \times 62.4 \text{ lb/ft}^3}{\text{Sp. Grm of solid}} \rightarrow \text{res}$$

$$= 665.3 \text{ lb}$$

$$(d) \quad v_s = v_f \times \frac{H}{L}$$

$$(\text{SOR}) = 27.78 \times \frac{10}{50}$$

$$= 5.5 \text{ ft/hrs}$$

(6) Calculate the dimension of a settling tank if discharge is $45 \text{ m}^3/\text{hr}$, surface overflow rate 0.5 m/hr , detention period 3 hrs . (BB, AD 2011)

Soln: $\text{SOR} = \frac{Q}{BL} = 90 \text{ m}^3$

$$\Rightarrow BL = \frac{45}{0.5} = 90 \text{ m}^3$$

Again, $D_T = \frac{BHL}{Q}$

$$\Rightarrow H = \frac{Q \times D_T}{BL} = \frac{45 \times 3}{90} = 1.5 \text{ m}$$

Let, $L = 4B$

$$4B \times B = 90$$

$$\Rightarrow B^2 = \frac{90}{4}$$

$$\Rightarrow B^2 = 22.5$$

$$\Rightarrow B = 4.75$$

$$\therefore L = 4B = 4 \times 4.75 = 19$$

take $B=5\text{m}$, $L=20\text{m}$
 Provide an extra depth of 1m for
 sludge and 0.5m for free board
 making total depth = ~~$3+1.5=4.5$~~
 $=1.5+1.5=3\text{m}$ (b)

Hence settling tank dimension $20\text{m} \times 5\text{m} \times 3\text{m}$

~~Q. 1~~
~~Surface overflow rate = $\frac{45\text{m}^3/\text{hr}}{20\text{m} \times 5\text{m}}$~~
 ~~$= 0.45\text{m}^3/\text{hr}/\text{m}^2$~~

(7) Calculate the dimension of a rectangular
 settling tank to treat $120\text{m}^3/\text{hr}$
 when the overflow rate is $0.75\text{m}/\text{hr}$
 & detention time is 2hr . (31st BCS)

Solⁿ: $\text{SOR} = \frac{Q}{BL}$

$\Rightarrow BL = \frac{120\text{m}^3/\text{hr}}{0.75\text{m}/\text{hr}} = 160\text{m}^2$

Again, $D_T = \frac{BHL}{Q}$

$\Rightarrow H = \frac{Q \cdot D_T}{BL} = \frac{120 \times 2}{160} = 1.5$

Not necessary
↓

$$\text{Let, } L = 4B$$

$$\therefore 4B^2 = 160$$

$$\Rightarrow B \approx 6.5 \text{ m}$$

$$\therefore L = 26 \text{ m}$$

Provide an extra depth of 1m for sludge & 0.5m for free board making total depth = $1.5 + 1 + 0.5 = 3 \text{ m}$

Hence settling tank dimension $26 \times 6.5 \times 3 \text{ m}$

check
surface loading rate
 $= \frac{120 \text{ m}^3/\text{hr}}{26 \times 6.5 \text{ m}^2}$
 $= 0.71 \text{ m}^3/\text{hr}/\text{m}^2$
 $= 710 \text{ m}^3/\text{hr}/\text{m}^2$ which is satisfactory

(8) A water supply project has to supply water to a town having population of 50,000. Design a suitable sedimentation tank with the following data:

(i) Per capita demand = 150 lits/day

(ii) velocity of flow = 30 cm/min

(iii) Detention time = 4 hrs

Soln: Max^m daily flow = $1.8 \times \text{Avg daily flow}$
 $= 1.8 \times 150 \times 50,000$
 $= 13.5 \times 10^6 \text{ L/day}$
 $= 13.5 \times 10^3 \text{ m}^3/\text{day}$

Volume of water in 4 hrs = $\frac{13.5 \times 10^3 \times 4}{24}$
 $= 2.25 \times 10^3 \text{ m}^3$

$$\begin{aligned}\text{Length of tank, } L &= D_t \times V_f \\ &= 0.3 \text{ m/min} \times (4 \times 60) \text{ min} \\ &= 72 \text{ m}\end{aligned}$$

$$\begin{aligned}\therefore BH &= \frac{Q}{L} = \frac{2.25 \times 10^3}{72} \\ &= 31.25 \text{ m}\end{aligned}$$

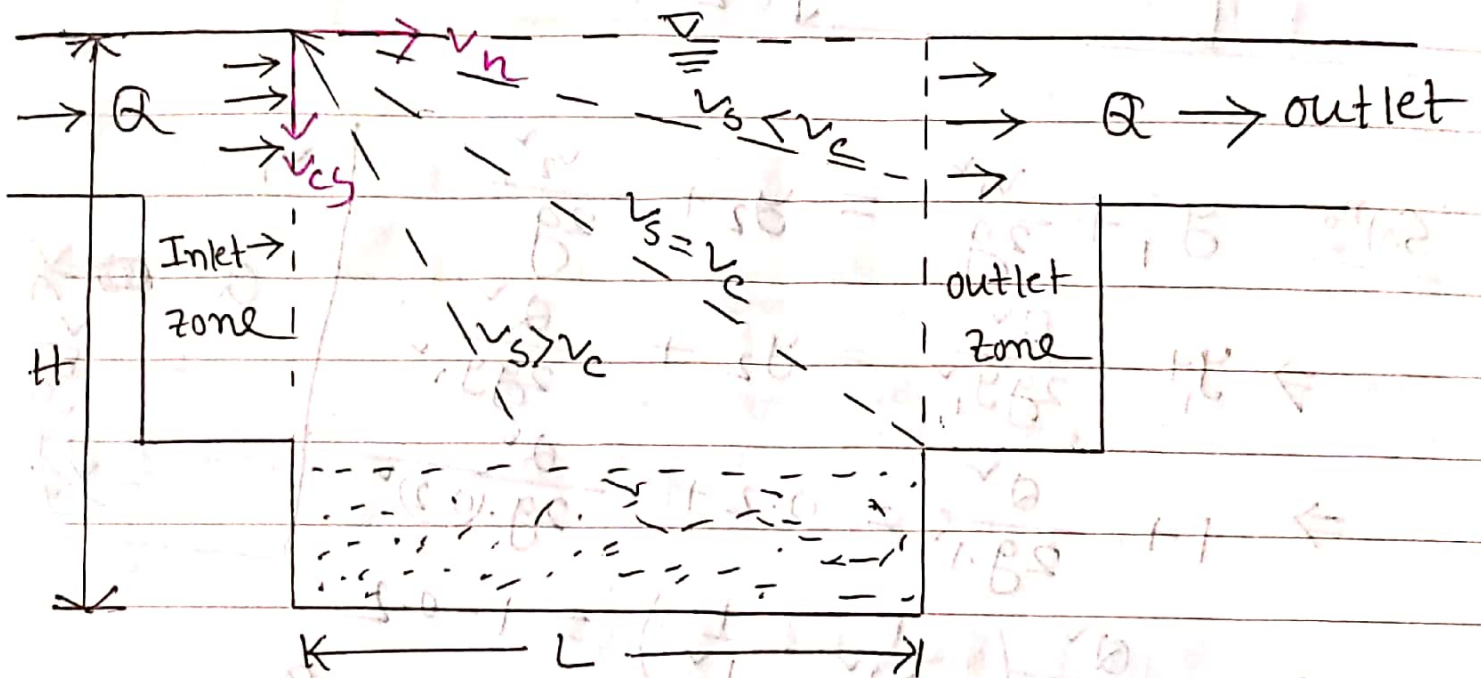
Assume, depth, $H = 3 \text{ m}$

$$\therefore \text{width, } B = \frac{31.25}{3} \approx 10.5 \text{ m}$$

Provide an extra depth of 1m for sludge storage and 0.5m for free board, making total depth = $3 + 1.5 = 4.5 \text{ m}$

Hence provide a settling tank of size $72 \text{ m} \times 10.5 \text{ m} \times 4.5 \text{ m}$

* Draw the settling trajectories of different types of particles in water in a sedimentation tank. [RRI '21]



$$v_h = \text{flow velocity} = \frac{Q}{BH}$$

$$v_{cs} = \text{Surface overflow (SOR)} = \frac{Q}{BL}$$

$$v_s = \text{Resultant velocity} = \sqrt{v_h^2 + v_{cs}^2}$$

$v_c = \text{critical velocity}$

* When,

$v_s \geq v_c \Rightarrow$ particles get settled i.e. removed

Date: / /

Sun	Mon	Tue	Wed	Thu	Fri	Sat
-----	-----	-----	-----	-----	-----	-----

* Design an aerated grit chamber installation for an average flow of $0.30 \text{ m}^3/\text{sec}$ and a peak flow rate of $1 \text{ m}^3/\text{sec}$. The average depth is 3 m , the width to depth ratio is $1.5:1$ and the detention time at peak flow is 3.5 min . The aeration rate is $0.4 \text{ m}^3/\text{min}$ per meter of tank length. Determine the dimensions of the grit chamber ~~is required~~ and the total air required.

Solⁿ Volume of chamber, $V = \frac{Q_p \times t}{n}$

$n = \text{number of chamber}$
 $= 1$

$$= \frac{1 \times 3.5 \times 60}{1}$$

$$= 210 \text{ m}^3$$

width of chamber, $w = 1.5 \times 3 = 4.5 \text{ m}$

length of chamber, $L = \frac{V}{w \times d}$

$$= \frac{210}{4.5 \times 3} = 15.55 \text{ m}$$

detention time at average flow ~~depth~~ rate,

$$t_{\text{avg}} = \frac{nV}{Q_{\text{avg}}} = \frac{1 \times 210}{0.30} = 700 \text{ sec}$$

$$= 11.66 \text{ mins}$$

Total air supply = length \times air supply rate

$$= 15.55 \times 0.4$$

$$= 6.22 \text{ m}^3/\text{min}/\text{m} \text{ of tank length}$$



(2) Breakpoint Chlorination: (WZPDC'19, DPDC'14) MSc'19

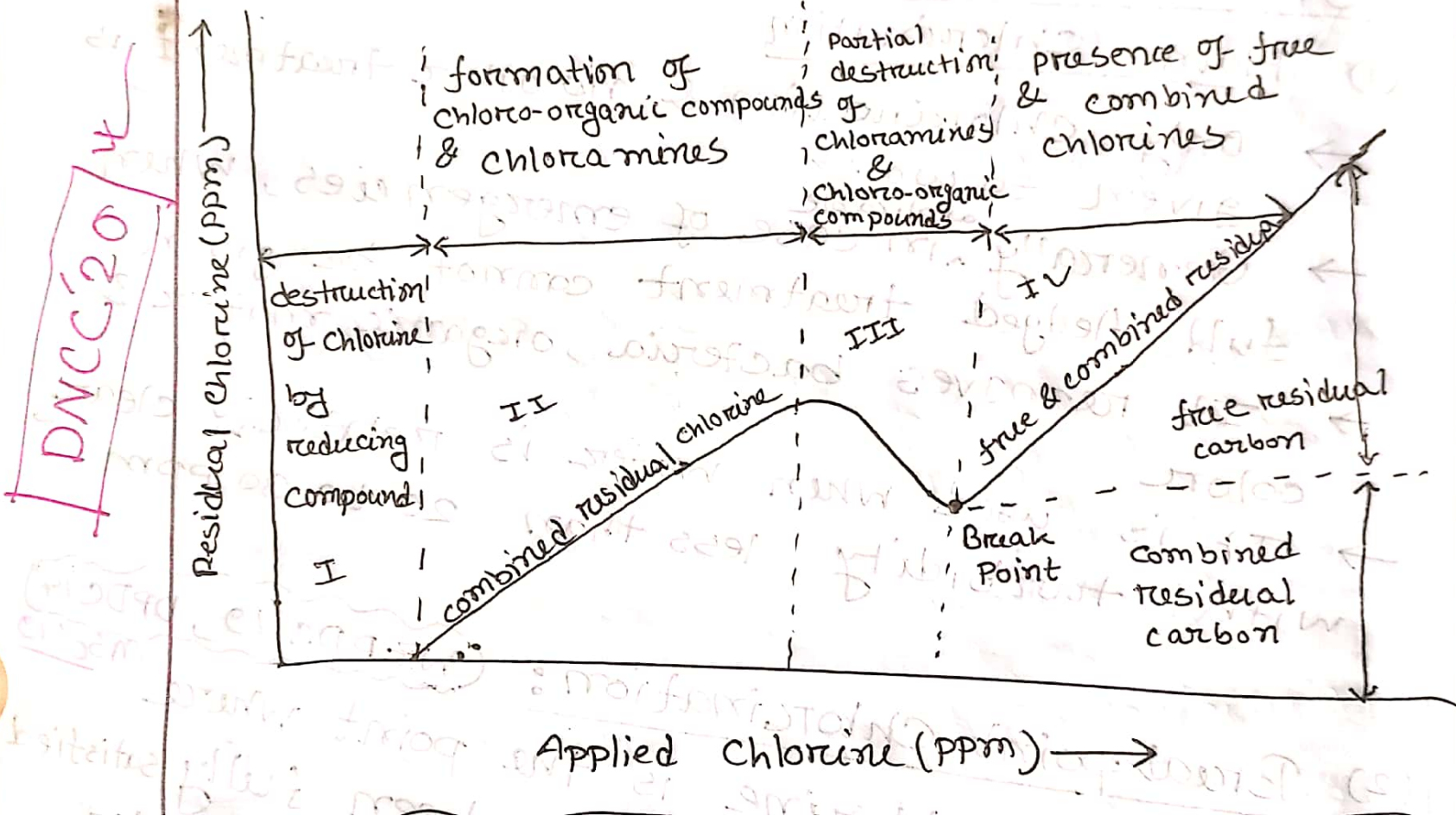
Breakpoint chlorine is the point where demand for chlorine has been fully satisfied in terms of chlorine addition to water.

or,

✓ Breakpoint chlorination ϕ indicates the maximum amount of chlorine required in raw water to kill all microorganisms & destroy it completely by oxidation. Any further addition of chlorine beyond this point will appear as free residual chlorine.

To ensure safety against future contamination

some extra chlorine is added beyond breakpoint chlorination to result in residual chlorine as 0.2 to 0.3 mg/l.



Solved Problems:

(1) Find Cl_2 demand, if Cl_2 dose of 0.6 mg/l is added to have Cl_2 residual of 0.2 mg/l . Find dose of Bleaching powder required, if it contains 30% of Cl_2 . Also find monthly bleaching powder requirement in kg to treat 10 MLD of water.

Solⁿ:

$$\begin{aligned} Cl_2 \text{ demand} &= Cl_2 \text{ dose} - Cl_2 \text{ residual} \\ &= 0.6 - 0.2 \\ &= 0.4 \text{ mg/L} \end{aligned}$$

$$\begin{aligned} \text{Bleaching powder dose} &= \frac{Cl_2 \text{ dose}}{\% Cl_2 \text{ in BP}} \\ &= \frac{0.6}{0.3} \end{aligned}$$

$$= 2 \text{ mg/l} \quad \text{mg to kg}$$

$$\begin{aligned} \text{Monthly BP required} &= 30 \times 10 \times 10^6 \times 2 \times 10^{-6} \\ &= 600 \text{ kg} \end{aligned}$$

*** Chlorine required to disinfect
or Cl_2 demand 0.2 mg/l residual 0.2 mg/l

Cl_2 dose

$$Cl_2 \text{ dose} = Cl_2 \text{ demand} + Cl_2 \text{ residual}$$

(ii) In a village 5000 litres water is required daily. If 0.05 mg/l chlorine is required to disinfect the water and 0.10 mg/l remains as residual, determine the amount of bleaching powder required if it contains 25% Cl_2 . [BB AD 2017]

Solⁿ: Cl_2 dose = Cl_2 demand + Cl_2 residual

$$= 0.05 + 0.1$$
$$= 0.15 \text{ mg/l}$$

\therefore Bleaching powder dose required = $\frac{\text{Cl}_2 \text{ dose}}{\% \text{Cl}_2 \text{ in BP}}$

$$= \frac{0.15}{0.25}$$
$$= 0.6 \text{ mg/L}$$

Total BP required = 0.6×5000

$$= 3000 \text{ mg}$$

$= 3 \text{ gm/day}$

(iv) A slow sand filtration unit produces 900 m³ of water per day. How much bleaching powder with 30% available Cl₂ will be required per day to treat this water with a Cl₂ dose 0.5 mg/L? [DPDC]

Solⁿ: BP dose = $\frac{0.5}{0.3} = 1.67 \text{ mg/l}$

BP required per day = $900 \times 10^3 \times 1.67 \times 10^{-6}$

= 1.5 kg

(v) The population of two individual years 1990 & 2000 is given 200,000 & 300,000 respectively. Determine the population of 2010. If per capita water demand 90 lpcd, Chlorine content of 0.5 mg/l is to be added in water to disinfect, how much water bleaching powder will be needed in 2010.

Given % of Cl₂ in BP is 20%
 [B.WDB, PGCB, DPDC, DESCO, Ashuganj, ...]

Solⁿ: $1+r = \frac{P_{2000}}{P_{1990}} = \frac{300,000}{200,000} = 1.5$

$n = 1 \text{ decade}$

$P_{2010} = P_{2000} \times (1.5)^1$

= 300,000

= 450,000

১০০০ প্রসিদ্ধি মাত্র মাত্র ০.৫ mg/L add করে ২০১
 ০.২ mg/L extra ০.২ mg/L add করে অন্তর্ভুক্ত।

$$\text{BP dose} = \frac{0.5}{0.2} = 2.5 \text{ mg/L}$$

BP required per day in ২০১০

$$\begin{aligned}
 \therefore &= 2.5 \times 10^{-6} \times 90 \times 450,000 \\
 &= 101.25 \text{ kg} \quad \underline{\underline{A}}
 \end{aligned}$$

*** আনক সন্থা @ BP এর পরিমাণ - বাড়ান্ড এ চায়।
 ১ kg = ২.২ lb (২.২০৫ lb more precise)

* $500\text{m}^3/\text{day}$ water is to be supplied from a water treatment plant with chlorine concentration of 0.5mg/L , if bleaching powder that is used for chlorine contains 30% available Cl_2 , find the amount of bleaching powder in kg/day ? [BIFPCL'22]

Soln: Bleaching powder required

$$= \frac{500\text{m}^3/\text{day} * \frac{0.5 \times 10^{-6}\text{kg}}{10^{-3}\text{m}^3}}{0.3}$$

$$= 0.83\text{kg}/\text{day}$$

a city in

* The population of year 2000 is 100,000 and year 2015 is 195,000. What will be the water demand in 2025? Given, water demand is 90 lpd. Chlorine content of 0.5 mg/L is to be added in water for disinfection. How much bleaching powder is required if bleaching powder contains 25% of chlorine?

[PGCL '21] [DESCO '15]
[GTCL '16] [DMTCL '22]

Solⁿ: ~~Population at 2025, P₂₀₂₅ = 195,000 x~~

~~P₂₀₂₅ = P₂₀₁₅ * (1 + $\frac{P_{2015} - P_{2000}}{P_{2000}}$)~~
 year gap betwⁿ 2025 to 2015
 year gap betwⁿ 2015 to 2000

Population at 2025
 $P_{2025} = P_{2015} * \left(\frac{P_{2015}}{P_{2000}} \right)^{\frac{10}{15}}$
 $= 195,000 * \left(\frac{195,000}{100,000} \right)^{\frac{10}{15}}$
 $= 304362$

∴ Amount of bleaching required
 $= \frac{304362 \times 90 \times 0.5 \times 10^{-6} \text{ kg/L}}{0.25}$
 $= 54.78 \text{ kg/day}$
 $= 0.055 \text{ ton/day}$

Solved problems

① Population of two individual years 1990 & 2000 is given 200,000 & 300,000 respectively. Determine the population of 2010.
[DESCO '15] [GTCL '16]

Solⁿ:
 $1+r+1 = \left(\frac{P_{2000}}{P_{1990}} \right) = \frac{300,000}{200,000} = 1.5$

$\therefore P_{2010} = P_{2000} (1+r)^n$ | decade, $n=1$
 $= 300,000 \times 1.5$
 $= 450,000$

③ The population of a community was 200,000 in 1955 & 233,000 in 1965. Find the probable population in 1990.

Solⁿ:
 $1+r = \frac{P_{1965}}{P_{1955}} = \frac{233,000}{200,000} = 1.165$

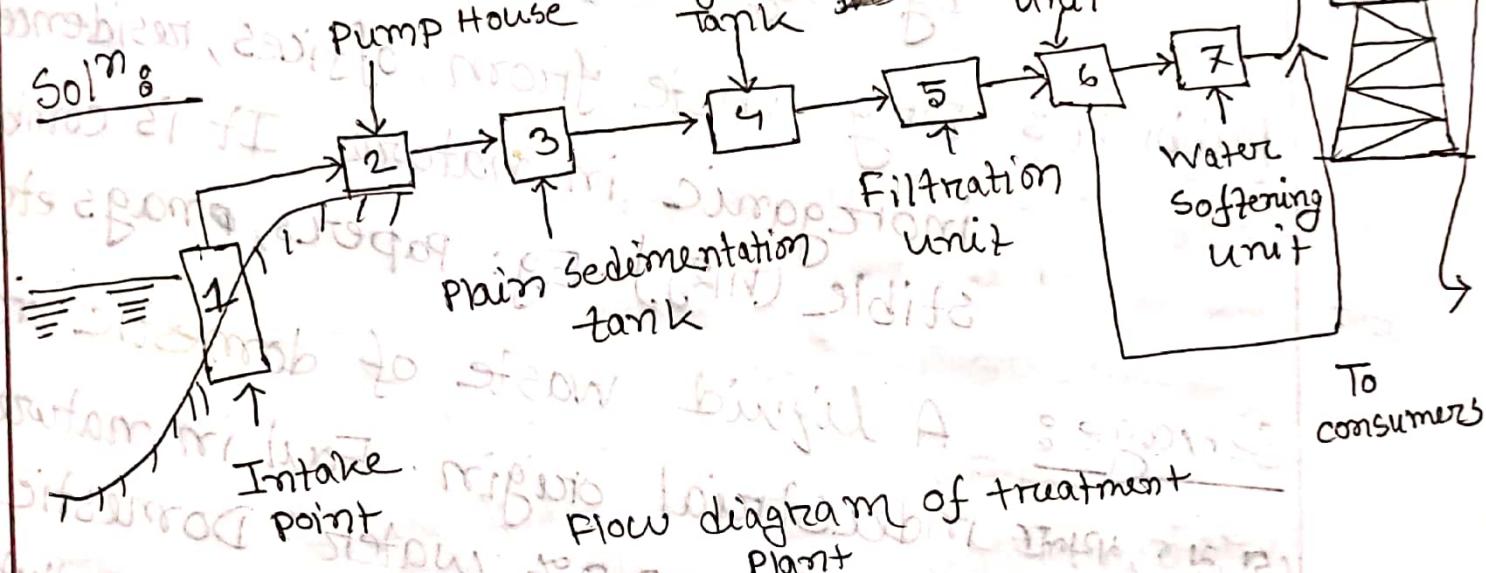
1990 to 1965 = 2.5 decades

$\therefore P_{1990} = P_{1965} (1+r)^{2.5}$
 $= 233,000 (1.165)^{2.5}$
 $= 233,000 (1.65)^{2.5}$
 $= 341,327 \text{ A}$

~~STUDY~~

VI Draw the flow diagram of water treatment of a river water [DWASA '21]

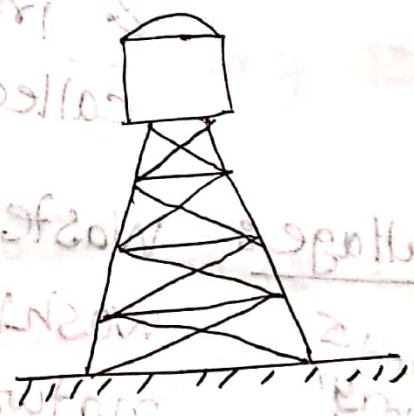
Flow diagram of water treatment / water supply system (BPDB '18, COXDA '19, ~~Titas 21~~, BIPPCl '21) [DWASA '21] [Ward Reservoir]



Flow diagram of treatment Plant

Sequence of units

1. Intake points
2. Pump house
3. Plain sedimentation tank
4. Coagulation tank
5. Filtration unit
6. Chlorination unit
7. water softening plant
8. Overhead reservoir



Formula for the design of sewers:

Generally Manning's formula is used to design sewers.

$$V = \frac{1}{n} R^{2/3} S^{1/2}$$

$$\left[\text{ft} \cdot \text{sec}^{-1} \text{ or } \frac{1.486 R^{2/3} S^{1/2}}{n} \right]$$

R = hydraulic radius of sewer = $\frac{A}{P}$

S = bed slope

n = Manning's roughness coefficient

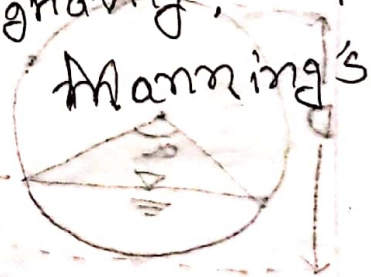
*** for circular sewage with full flow,

$$R = \frac{A}{P} = \frac{\frac{\pi}{4} D^2}{\pi D} = \frac{D}{4}$$

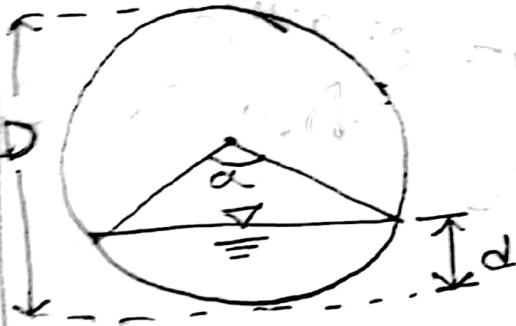
*** for a circular sewage with running half full flow,

$$R = \frac{A}{P} = \frac{\frac{\pi}{8} D^2}{\frac{\pi D}{2}} = \frac{D}{4} \quad (\text{same})$$

* sewers ~~are~~ act like open channel flow, as they are designed as partial flow condition (i.e. flow under gravity, no partial pressure flow). That's why Manning's equation is used.



Partial flow characteristics of circular sewer



$$\frac{d}{D} = \frac{1}{2} (1 - \cos \frac{\alpha}{2})$$

\$d\$ = depth of flow

\$D\$ = dia of ~~sewer~~ sewer

$$\frac{a}{A} = \frac{\alpha}{360} - \frac{\sin \alpha}{2\pi}$$

[\$a\$ = partial flow area]

$$\frac{p}{P} = \frac{\alpha}{360}$$

[\$P\$ = partial perimeter]

$$[P = \pi D]$$

$$\frac{r}{R} = \frac{a/A}{p/P} = 1 - \frac{360 \sin \alpha}{2\pi \alpha}$$

\$r\$ = partial hydraulic radius

~~$$v = \frac{1}{n} R^{2/3} S^{1/2}$$~~

$$\frac{v}{V} = \frac{\frac{1}{n} r^{2/3} S^{1/2}}{\frac{1}{n} R^{2/3} S^{1/2}}$$

[\$v\$ = partial flow velocity]

$$\frac{v}{V} = \left(\frac{r}{R} \right)^{2/3}$$

(2) A 20cm dia sewer is laid at a slope of 0.004 & is designed to carry a discharge at a depth of 10cm with Manning's $n = \cancel{0.01} 0.014$. Calculate design discharge. [DWASA '21]

Soln: $\frac{D_d}{D} = \frac{10}{20} = \frac{1}{2}$
 running half-full $\therefore R = \frac{D}{4}$

Now, $Q = AV$
 $= \frac{\pi}{8} D^3 \times \frac{1}{n} \times R^{2/3} \times S^{1/2}$
half full area $= \frac{\pi}{8} \times (0.2)^3 \times \frac{1}{0.014} \times \left(\frac{0.2}{4}\right)^{2/3} \times (0.004)^{1/2}$
 $= 9.6 \times 10^{-3} \text{ m}^3/\text{sec}$
 $= 9.6 \text{ litre/sec}$ Ans

(3) Determine the size of a circular sewer for a discharge of 500 litre/sec running half full. Assume $S = 0.0001$ & $n = 0.015$

Soln: half full $\therefore R = \frac{D}{4}$

We know, $Q = AV$
 $\Rightarrow Q = \frac{\pi D^3}{8} \times \frac{1}{n} \times R^{2/3} \times S^{1/2}$
 $\Rightarrow 0.5 = \frac{\pi}{8} \times D^3 \times \frac{1}{0.015} \times \left(\frac{D}{4}\right)^{2/3} \times (0.0001)^{1/2}$
 $\Rightarrow 0.5 = 0.104 \times D^{8/3}$
 $\Rightarrow D^{8/3} = 4.81254$
 $\therefore D \approx 1.8 \text{ m}$

WV

radius $\frac{D}{2}$
or dia

Date: _____
Sun Mon Tue Wed Thu Fri Sat

* A pipe ~~flow~~ has a radius 0.6m and flow is $2\text{m}^3/\text{sec}$. If the bed slope is 1:50, determine n if pipe flow is half. ~~5.5~~ [KGDCL'21]

Solⁿ:

$$Q = \frac{1}{n} * \frac{A}{2} * \left(\frac{D}{4}\right)^{2/3} * \sqrt{S}$$

radius to dia

$$\Rightarrow 2 = \frac{1}{n} * \frac{\pi * 0.6^2}{2} * \left(\frac{0.6 * 2}{4}\right)^{2/3} * \sqrt{\frac{1}{50}}$$

for solving in calculator

$$\Rightarrow n = 0.018 \quad \underline{\underline{A}}$$

* A sewer of dia 400mm is laid on a grade 0.015 with Manning's $n = 0.013$. What will be the velocity & discharge when the depth of flow is 100mm [SGCL'20] [GTCL'22] [BGDCL'21] [ERL'22] [CWDIB'19]

Solⁿ

$$\frac{d}{D} = \frac{100}{400} = \frac{1}{2} (1 - \cos \frac{\alpha}{2})$$

$$\Rightarrow \frac{1}{4} = \frac{1}{2} (1 - \cos \frac{\alpha}{2}) \therefore \alpha = 120^\circ$$

$$\frac{r_a}{R} = 1 - \frac{360 \times \sin 120^\circ}{2\pi \times 120^\circ} = 0.5865$$

$$\therefore \frac{v}{V} = \left(\frac{r_a}{R}\right)^{2/3} = 0.7$$

∴ partial velocity, $v = 0.7V$

$$= 0.7 \times \frac{1}{0.013} \left(\frac{0.4}{4}\right)^{2/3} \times (0.015)^{1/2}$$

$$= 1.42 \text{ m/s}$$

~~discharge, $Q = \text{flow area} \times \text{velocity}$~~

~~$$= \frac{\pi \times 0.2^2}{4} \times 1.42$$~~

~~$$= 0.045 \text{ m}^3/\text{s}$$~~



$$\frac{a}{A} = \frac{\alpha}{360} - \frac{\sin \alpha}{2\pi}$$

$$\therefore a = \left(\frac{120}{360} - \frac{\sin 120^\circ}{2\pi}\right) \times \frac{\pi}{4} \times 0.4^2 = 0.0246 \text{ m}^2$$

VESTAR MR
RIMETAZINE

P.T.O

$$\therefore \text{discharge} = 0.0246 \times 1.42$$

$$= 0.035 \text{ m}^3/\text{s}$$

* A circular cross-section sewer pipe dia 20" Manning's roughness coefficient = 0.013, laid on a grade = 0.0015. calculate velocity and discharge when the depth of flow is 5". [ELBL 2022]

Solⁿ: $\frac{d}{D} = \frac{5}{20} = \frac{1}{2} (1 - \cos \frac{\alpha}{2})$
 $\Rightarrow \frac{1}{4} = \frac{1}{2} (1 - \cos \frac{\alpha}{2})$
 $\therefore \alpha = 120^\circ$

$\frac{n}{R} = 1 - \frac{360^\circ \sin \alpha}{2\pi \alpha} = 0.5865$

20" ***
 20 inch = 1.67 ft

$\therefore \frac{V}{V_f} = \left(\frac{n}{R}\right)^{2/3} = (0.5865)^{2/3} = 0.7$

$\therefore \text{velocity} = 0.7 * \frac{1.486}{0.013} * \left(\frac{1.67}{4}\right)^{2/3} * \sqrt{0.0015}$

ft & m² = 1.486
 $D = 20"$ convert into ft
 inch & convert into m²

= 1.73 ft/sec

$R = \left(\frac{D}{4}\right)^{2/3}$

$\frac{a}{A} = \frac{\alpha}{360} - \frac{\sin \alpha}{2\pi}$

$\Rightarrow a = \left(\frac{120}{360} - \frac{\sin 120}{2\pi}\right) * \frac{\pi}{4} * \left(\frac{20}{12}\right)$
 = 0.4265 ft

$\therefore \text{discharge} = 1.73 * 0.4265$
 = 0.738 ft³/sec



* Determine the size of a circular drainage outlet of a 6 hectare drainage system if the discharge coefficient is 1cm and the tile grade is 0.3%. Assume $n = 0.011$ [JGTDGL'21]

Solⁿ:

discharge coefficient 1cm or 22mm or 1cm/day

$$\therefore \text{Discharge, } Q = \frac{1 \times 10^{-2} \text{ m}}{\text{day}} \times 6 \times 10^4 \text{ m}^2$$

$$= 600 \text{ m}^3/\text{day}$$

$$= \frac{600}{24 \times 3600} = \frac{1}{144} \text{ m}^3/\text{sec}$$

for a full flow circular dia outlet,

$$Q = \frac{1}{n} A R^{2/3} S^{1/2}$$

$$\Rightarrow \frac{1}{144} = \frac{1}{0.011} \times \frac{\pi}{4} \times D^2 \times \left(\frac{D}{4}\right)^{2/3} \times \sqrt{\frac{0.3}{100}}$$

$$\Rightarrow D^{3/3} = 4.475 \times 10^{-3}$$

$$\therefore D = 0.1315 \text{ m} = 13.15 \text{ cm} \quad \underline{\text{Ans}}$$

* একটি $3m \times 3m \times 3m$ size tank এর মধ্যে $2.5m$ উচ্চতায় পানি আছে। tank এর সাথে $400m$ dia এর $2m$ লম্বা একটি pipe যুক্ত আছে। টাকান ফিলের loss consider না করে pipe flow চাও। [DMTCL'22]

Solⁿ

$$\text{pipe flow, } Q = AV$$

$$= \frac{\pi}{4} \times \left(\frac{400}{1000}\right)^2 \times \sqrt{2 \times 9.81 \times 2.5}$$

$$= 0.88 \text{ m}^3/\text{sec}$$

* The area of metro rail station is $600m^2$. Intensity of rainfall $100mm/hr$. Slope of pipe 1 in 100. Calculate the size of PVC pipe required. [DMTCL'22]

Solⁿ $Q = 600m^2 \times \frac{100 \times 10^{-3}m}{3600 \text{ sec}} = 0.0167 \text{ m}^3/\text{sec}$

For PVC pipe, $n = 0.009$ ***

Taking full flow condition,

$$Q = \frac{1}{n} A R^{2/3} S^{1/2}$$

$$\Rightarrow 0.0167 = \frac{1}{0.009} \times \frac{\pi}{4} \times D^2 \times \left(\frac{D}{4}\right)^{2/3} \times \sqrt{\frac{1}{100}}$$

$$\Rightarrow D^{2 + \frac{2}{3}} = \frac{0.0167 \times 0.009 \times 4 \times 4^{2/3} \times \sqrt{100}}{\pi}$$

$$\Rightarrow D^{\frac{8}{3}} = 4.82 \times 10^{-3}$$

$$\therefore D = 0.135 \text{ m}$$

$$\therefore D = 135 \text{ mm } \underline{A}$$

6) 18 inch sewer with $n = 0.013$ is laid on a grade of 0.015

- (i) find capacity when flowing full
- (ii) velocity when depth of flow is 4.5 inch

[BCS] [Bakhrabad '21] [GTCL '22] 18" = 1.5 ft — full flow

Soln: $Q = AV$

$$= \frac{\pi}{4} \times (1.5)^2 \times \frac{1.49}{n} \times R^{2/3} \times S^{1/2}$$

$$= 1.767 \times \frac{1.49}{0.013} \times \left(\frac{1.5}{4}\right)^{2/3} \times (0.015)^{1/2}$$

$$\frac{1.49}{n} \text{ ft}^2 \text{ sec}^{-1}$$

$$= 1.767 \times 7.29$$

$$= ~~8.656~~ \text{ ft}^3/\text{sec}$$

$$= 7.3 \text{ ft}^3/\text{sec}$$

(ii) full flow velocity, $V =$

$$\frac{d}{D} = \frac{4.5}{18} = \frac{1}{4} = \frac{1}{2} (1 - \cos \frac{\alpha}{2})$$

$$\Rightarrow \frac{1}{4} = \frac{1}{2} (1 - \cos \frac{\alpha}{2})$$

$$\Rightarrow \alpha = 120^\circ$$

Slope & n
 (for $2\pi\theta$)
 Manning's formula
 we use $2\pi\theta$
 in formula
 we use 2π

$$1 - \frac{360^\circ \sin 60^\circ}{2\pi \times 60^\circ} = 1 - \frac{3 \times 0.866}{2\pi} = 0.586$$

$$\frac{v}{V} = 1 - \frac{360^\circ \times \sin 120^\circ}{2\pi \times 120^\circ} = 1 - \frac{3 \times 0.866}{2\pi} = 0.586$$

$$\frac{v}{V} = \left(\frac{v}{R}\right)^{2/3} = 0.7 \Rightarrow v = 0.7V$$

$$\Rightarrow \frac{v}{V} = (0.586)^{2/3} = 0.7 \Rightarrow v = 0.7 \times 7.3$$

$$= 5.11 \text{ ft/sec}$$

* Define BOD, COD. Why ~~BOD~~ COD is always greater than BOD? [GTCL'22] [BIFPCL'21] [PGCB'15] [PGCB'10] [Titas'19] [DNASA'17] [DESCO'18] [WRGCL'14]

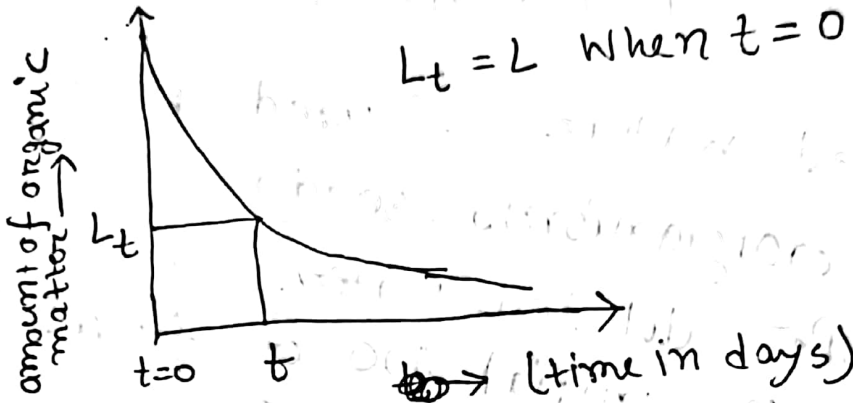
Solⁿ: BOD: Biochemical oxygen demand (BOD) is the amount of dissolved oxygen (DO) needed by bacteria and other microorganisms to ~~break down~~ ^{decompose} organic material present in a given water sample under aerobic conditions at certain temperature over a specified time period.

COD: ~~The~~ The amount of oxygen that is required for the chemical oxidation of the organic and inorganic ^{substances} ~~chemicals~~ present in the wastewater by utilising oxidising agents like potassium permanganate ($KMnO_4$) and potassium dichromate ($K_2Cr_2O_7$) etc is called as chemical oxygen demand (COD).

COD is always greater than BOD because -

- (1) ~~More~~ more organic compounds can be chemically oxidized than biologically oxidized in a given period.
- (2) COD includes both biodegradable and non-biodegradable substances whereas BOD ~~contains~~ contains only bio-degradable substances.

BOD at different days & ultimate BOD



L_t = amount of organic matter present at time t

L = total amount of organic matter present in waste water

~~Equation~~

$$L_t = L e^{-kt}$$

$$= L \cdot 10^{-k_d t}$$

k = rate constant

$k_{20^\circ\text{C}} = 0.23/\text{day}$
 (Not temp. dependent) (constant)

k_d = deoxygenation constant

k_d changes with temperature

BOD $t = L(1 - e^{-kt})$ — (i)

BOD $t = L(1 - 10^{-k_d t})$ — (ii)

$k_d(20^\circ\text{C}) = 0.1/\text{day}$
 (standard)

when $t \rightarrow \infty$, $L = \text{BOD}_\infty$

maximum

k_d for sewage in 20°C is $0.15/\text{day}$.

যদি k_d ও k এর মান জানা থাকে তবে k এর মান $0.15 \sim 0.18$ দিন^{-১}।

k_d হিসেবে বীর সিন্ধু (i) নগর স্বাস্থ্যকর্তা-অফিসের তত্ত্বাবধায়,

$k = 0.2 + 21^\circ\text{C}$ (ii) নগর স্বাস্থ্যকর্তা-ব্যবহার করবেন।

** $k_T = k_{20} (1.047)^{T-20^\circ\text{C}}$

Solved Problems

* (1) In a BOD test the initial DO of the 2% diluted sample is 6 mg/l and its final after 5 day incubation at 20°C is 2 mg/l. Then find 5-day BOD of sewage sample.

Solⁿ: $BOD = [6 - 2] \times \frac{100}{2} = 200 \text{ mg/l}$ \checkmark

* (2) If 5 day BOD at 20°C is 200 mg/l, find 3 day BOD at 15°C and 8 day BOD at 30°C.

Take $k_{20} = 0.23/\text{day}$

Solⁿ: $k_{15} = k_{20} (1.047)^{15-20} = 0.23 \times (1.047)^{-5} = 0.183/\text{day}$

$k_{30} = 0.23 \times (1.047)^{30-20} = 0.364/\text{day}$

$BOD_5 = L_0 [1 - e^{-k_{20} t}]$

$\Rightarrow 200 = L_0 [1 - e^{-0.23 \times 5}]$ $[L_0 = BOD_u]$

$\Rightarrow L_0 = 292.67 \text{ mg/l}$

$\therefore BOD_3 \text{ at } 15^\circ\text{C} = L_0 [1 - e^{-k_{15} t}]$

$= 292.67 [1 - e^{-0.183 \times 3}]$
 $= 123.65 \text{ mg/l}$

$BOD_8 \text{ at } 30^\circ\text{C} = 292.67 [1 - e^{-0.364 \times 8}]$
 $= 276.76 \text{ mg/l}$ \checkmark

* The 5 day BOD of water is 200mg/L at 20°C, with constant rate 0.21/day. Determine the 10 day BOD of waste water at 20°C.

[~~RPSC~~] [RPSC '22] [NESCO '21] [GTCL '22] [DWASA '21]

Solⁿ:
$$BOD_u = \frac{BOD_5}{1 - e^{-kt}}$$

$$= \frac{200}{1 - e^{-0.21 \times 5}} = 307.66 \text{ mg/L}$$

Now,
$$BOD_{10} = BOD_u (1 - e^{-kt})$$

$$= 307.66 * (1 - e^{-0.21 * 10})$$

$$= 270 \text{ mg/L} \quad \underline{A}$$

$$BOD_{10} = BOD_5 * \frac{1 - e^{-k * 10}}{1 - e^{-k * 5}}$$

$$= 200 * \frac{1 - e^{-0.21 * 10}}{1 - e^{-0.21 * 5}}$$

$$= 270 \text{ mg/L} \quad \underline{A}$$

Date: / /

Sun	Mon	Tue	Wed	Thu	Fri	Sat
-----	-----	-----	-----	-----	-----	-----

* Initial and final dissolved oxygen in a BOD bottle after 3 days is 7mg/L and 3mg/L and k is 0.2/day. Determine BOD_5 and ultimate BOD. [DMTCL'22]

Solⁿ: $BOD_3 = (DO_i - DO_f) \times DF$
 $= (7 - 3) \times 1$
 $= 4 \text{ mg/L}$

~~DF~~
dilatation factor
 $= 1$
(25/22 (1/32) (1/12))

$$BOD_5 = \frac{1 - e^{-0.2 \times 5}}{1 - e^{-0.2 \times 3}} \times 4 = 5.6 \text{ mg/L}$$

$$BOD_u = \frac{4}{1 - e^{-0.2 \times 3}} = 8.865 \text{ mg/L}$$

* Initial and final DO of a sample for 5 days is 7.5 mg/L and 3.4 mg/L. Dilution factor is @ 50. Calculate the ultimate BOD if $k=0.2$ day

[CPGCB'22] [PGCB'22]

Solⁿ: $BOD_5 = (7.5 - 3.4) \times 50 = 205 \text{ mg/L}$

$$\therefore BOD_5 = BOD_u (1 - e^{-kt})$$

$$\therefore BOD_u = \frac{205}{1 - e^{-0.2 \times 5}} = 324.305 \text{ mg/L}$$

direct
to initial
value

(3) The wastewater having an organic concentration of 54 mg/l is flowing at a steady rate of $0.8 \text{ m}^3/\text{day}$ through a detention tank of dimensions ~~$2\text{m} \times 2\text{m}$~~ $2\text{m} \times 4\text{m} \times 2\text{m}$. If the decay constant is $0.1/\text{day}$, the outlet concentration is what? [DMTCL MISS]

Solⁿ Detention time, $t = \frac{4 \times 2 \times 2 \text{ m}^3}{0.8 \text{ m}^3/\text{day}} = 20 \text{ days}$

BOD consumed = $54 (1 - 10^{-0.1 \times 20}) = 53.46 \text{ mg/L}$

10 base
210
0.22
0.250
0.25

\therefore outlet concentration = $(54 - 53.46) \text{ mg/L}$
 $= 0.54 \text{ mg/L}$



Date: / /

Sun	Mon	Tue	Wed	Thu	Fri	Sat
-----	-----	-----	-----	-----	-----	-----

(3) A river water temperature is 10°C . Calculate the percentage of oxygen consumption after 4 days of the initial amount of oxygen. The BOD rate constant is $0.115/\text{day}$ at standard condition. [SEFL 23]

Solⁿ: Let, initial oxygen content = L_0

Remaining O_2 after 4 days = L

at standard condition, $k_{20} = 0.115/\text{day}$

$$\begin{aligned}\therefore k_{10} &= k_{20} \times (1.047)^{T-20} \\ &= 0.115 \times (1.047)^{10-20} \\ &= 0.0726/\text{day}\end{aligned}$$

$$\begin{aligned}\therefore L &= L_0 \times e^{-k_{10} \times t} \\ &= L_0 \times e^{-0.0726 \times 4} \\ &= 0.748 L_0\end{aligned}$$

$$\begin{aligned}\therefore \text{Oxygen consumption in 4 days} &= L_0 - L \\ &= (1 - 0.748) L_0 \\ &= 0.25 L_0\end{aligned}$$

\therefore oxygen consumption is 25% of initial oxygen content.

~~21~~



* Find BOD₅. Initial DO of a soil sample is 8mg/L and final DO is 2mg/L. If 30ml waste sample is mixed with 270ml water. [DPDC'16]

Soln:

$$\begin{aligned} \text{BOD}_5 &= (\text{DO}_i - \text{DO}_f) \times \frac{\text{Total Volume}}{\text{Waste water volume}} \\ &= (8 - 2) \times \frac{(270 + 30)}{30} \rightarrow \text{300ml} \\ &= 60 \text{mg/L } \underline{A} \end{aligned}$$

* Ten 5ml samples of waste water are placed in 300ml BOD bottles and diluted to full volume. Half bottles are titrated immediately and ~~also~~ initial DO is 7.9mg/L. The remaining bottles are incubated for 5 days after which DO is 4.5mg/L. Calculate BOD₅

Soln:

$$\begin{aligned} \text{BOD}_5 &= (7.9 - 4.5) \times \frac{300}{5 \times 10} \\ &= 20.4 \text{mg/L} \end{aligned}$$

Half bottle
in 2ml

* If 2% solution is used from sewage of 5 days at 20°C and dissolved oxygen depletion was 5ppm, determine BOD₅? [PGCB'17]

$$\begin{aligned} \text{Soln: } \text{BOD}_5 &= 5 \times \frac{100}{2} \\ &= 250 \text{mg/L} \end{aligned}$$

$$\text{DE} = \frac{100}{2}$$

Date: / /

Sun	Mon	Tue	Wed	Thu	Fri	Sat
-----	-----	-----	-----	-----	-----	-----

* The BOD_5 of a sample is 180 mg/L . Find out the dilution factor if the volume of the bottle is 300 ml . Also find out the volume of the sample of sewage mixed with water if the consumption of DO is 4 mg/L .

Solⁿ: $BOD_5 = \text{consumed DO} \times DF$

$$\Rightarrow DF = \frac{180}{4} = 45$$

$$DF = \frac{\text{volume of bottle}}{\text{volume of sewage}}$$

$$\Rightarrow \text{volume of sewage} = \frac{\text{volume of bottle}}{DF}$$

$$= \frac{300}{45}$$
$$= 6.67 \text{ ml}$$

* The Waramurungudi tannery with a wastewater flow of $0.011 \text{ m}^3/\text{s}$ and a BOD_5 of 590 mg/L discharges into the Djanggawul Creek. The creek has a 10-year, 7-day low flow of $1.7 \text{ m}^3/\text{s}$. Upstream of the Waramurungudi tannery, the BOD_5 of the creek is 0.6 mg/L . The BOD rate constant k are 0.115 day^{-1} for the Waramurungudi tannery and 3.7 day^{-1} for the creek. Calculate the initial ultimate BOD after mixing. [BWB'20]

Solⁿ:

Ultimate BOD of tannery waste water,

$$\text{BOD}_{u1} = \frac{590}{(1 - e^{-0.115 \times 5})} = 1349.2 \text{ mg/L}$$

Ultimate BOD of creek water,

$$\text{BOD}_{u2} = \frac{0.6}{1 - e^{-3.7 \times 5}} = 0.6 \text{ mg/L}$$

∴ Initial ultimate BOD after mixing

$$= \frac{0.011 \times 1349.2 + 1.7 \times 0.6}{0.011 + 1.7} = 9.27 \text{ mg/L}$$

(Correct)

★

e base 2to or 10 base 2to)

अवधि (2to) $k = 0.115/\text{day}$ 2to 10 base 2to 2to 2to,
 अवधि (2to), $k = 3.7/\text{day}$ 2to base 2to e.



VESTAR MR[®]
 * TRIMETAZIDINE

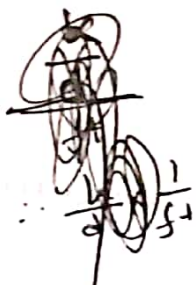
सं. - 2to 2to 2to e base 2to

* Waste water flowing from a city at a rate of 1.35 MGD treated by primary sedimentation & secondary trickling filters with total surface area ~~700,000~~ ^{70,000} ft². The influent BOD₅ concentration = 300 mg/L and suspended solids concentration = 220 mg/L. The primary treatment process removes 33% of the BOD₅. Calculate the required ^{organic} loading rate in kg/ft²/day. [DPDC '20] [Jalalabad Gas '21]

Solⁿ: organic loading = $\frac{(1 - 0.33) \times 300 \times 10^{-6} \times 1.35 \times 10^6}{700,000}$ kg/day

= 0.0147 kg/ft²/day A

1 Gallon = 3.785 Litre



* organic BOD₅ loading rate

Waste water → primary effluent
 count 20.000 by 2000
 or recycle secondary effluent

* In BOD test, dilution wastewater sample (1:50 dilution), initial dissolved oxygen = 8mg/L
 final dissolved oxygen after 5 days = 4mg/L.
 Find 5 days BOD. If wastewater discharged into river at a rate $10 \text{ ft}^3/\text{sec}$ through 24 hrs, estimate yearly BOD₅ load. (metric tons/year) [NHA'19]

Solⁿ $\text{BOD}_5 = (8-4) \times 50 = 200 \text{ mg/L}$

yearly BOD₅ loading ~~$\frac{10}{(3.28)^3} \times 60 \times 60 \times 24 \times$~~ ~~$(200 \times 10^{-6} \text{ kg/L})$~~

$$= \left[\frac{10}{(3.28)^3} \times 3600 \times 24 \right] \text{ m}^3/\text{year} \times \left[\frac{200 \times 10^{-9}}{10^3} \right] \text{ ton/m}^3$$

$$= 1787.37 \text{ ton/year}$$

Sub: Disposal of Sewage Effluent

Day: _____

Time: _____ Date: 14/11/2020

Disposal by Dilution : If dilution factors above 500, then sewage requires no treatment before disposal.

Disposal by dilution is the process whereby the treated sewage or the raw sewage is discharged into a river stream or a large body of water such as a lake or sea.

The discharge sewage, in due course of time, is purified by self purification process of natural water.

Final concentration of DO or BOD is,

$$C = \frac{C_s Q_s + C_R Q_R}{Q_s + Q_R}$$

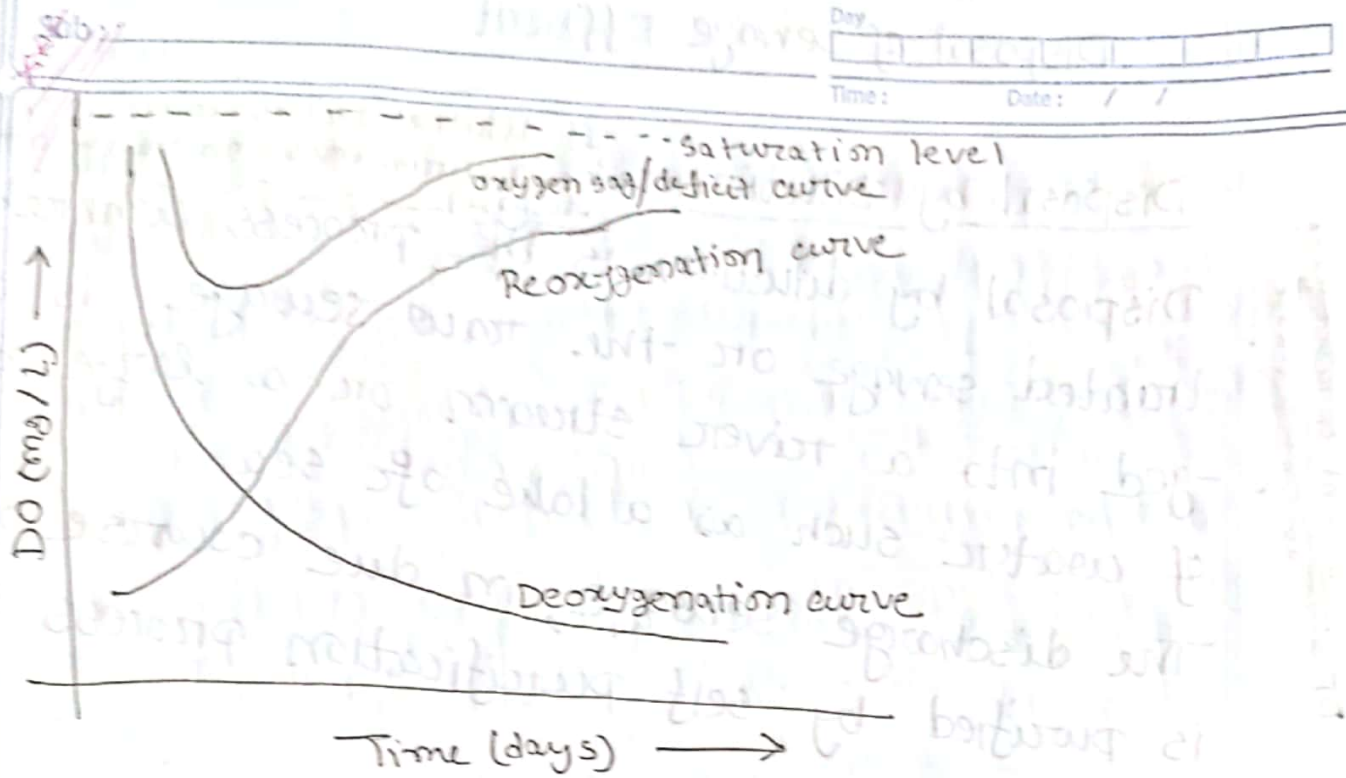
C_s = sewage concentration
 C_R = river concentration
 Q_s / Q_R → flow rate of sewage / river

*** at higher temperature, DO is low, as the rate of bio-chemical activities are high at higher temperature causing rapid depletion of dissolved oxygen.

The oxygen deficit of a polluted river-stream i.e. oxygen deficit (D) = Saturation DO - Actual DO

* Saturated DO = amount of DO if river is fully saturated with oxygen.

DF = amount of treated sewage



In a polluted stream, the DO content goes on reducing due to decomposition of organic matter.

Re-oxygenation curve : In order to counter-balance the consumption of DO due to deoxygenation, atmosphere supplies oxygen to the water and the process is called re-oxygenation. The rate of ~~re-oxygenation~~ receiving oxygen is more in shallow depth than deep water body.

Oxygen Deficit Curve / Sag Curve

Reoxygenation < Deoxygenation

Streeter-Phelps equation :

To calculate DO deficit after t days,

$$D_t = \frac{k_d \cdot L}{k_r - k_d} [(10)^{-k_d \cdot t} - (10)^{-k_r \cdot t}] + [D_0 \times 10^{-k_r \cdot t}] \quad \text{when } k_d \leq 0$$

$$= \frac{k_d \cdot L}{k_r - k_d} [e^{-k_d \cdot t} - e^{-k_r \cdot t}] + [D_0 \times e^{-k_r \cdot t}] \quad \text{when } k_d \geq 0$$

Where,

L = Ultimate first stage BOD/BOD_u

k_d = de-oxygenation coefficient

(k_d is always 10 base) [k is e base]

k_r = Re-oxygenation coefficient

D_0 = initial oxygen deficit / oxygen deficit at the point
of mixing sewage into river

* self purification constant, $f = \frac{k_r}{k_d}$

⇒ Maximum DO deficit / Minimum DO presents in stream = D_c (critical DO), $D_c = \frac{BOD_u}{f} [(10)^{-k_d \cdot t_c} - \frac{BOD_u}{f} e^{-k_d \cdot t_c}]$

time to reach DO deficit = t_c (critical time)

$$t_c = \frac{1}{k_d(f-1)} \log \left[\left\{ 1 - (f-1) \frac{D_0}{L} \right\} f \right] \quad \text{when } k_d < 0.2$$

$k_d > 0.2$ 2 (or) log or 5.1812 in 20

(2) A municipal waste water treatment plant discharge $1.2 \text{ m}^3/\text{sec}$ of effluent having BOD of 60 mg/l ^{into a stream} that has a flow of $9.3 \text{ m}^3/\text{sec}$ and BOD of ~~12~~ 6 mg/l . Estimate the mixing BOD of the river just downstream of flow. [BUTET]

Solⁿ:

$$\text{mixed BOD} = \frac{C_s Q_s + C_r Q_r}{Q_s + Q_r}$$

$$= \frac{1.2 \times 10^3 \times 60 + 9.3 \times 10^3 \times 6}{1.2 \times 10^3 + 9.3 \times 10^3}$$

$$= \frac{1.2 \times 60 + 9.3 \times 6}{1.2 + 9.3}$$

$$= 12.17 \text{ mg/l}$$

*m³ cancel out
litre
cancel conversion
to litre m³*

Sub: _____

Day

Time: _____

Date: / /

(3) A waste water Treatment plant discharges 17360 m³/day of treated effluent into a small stream having a flow rate of 0.43 m³/sec and ~~an ultimate~~ BOD₅ of 5 mg/l. The treated effluent has a BOD₅ of 12 mg/l and BOD decay constant is 0.12/day at 20°C. Stream water temperature is 18°C. Compute ultimate BOD immediately after mixing.

Solⁿ: $0.43 \text{ m}^3/\text{sec} = 0.43 \times 86400 = 37,152 \text{ m}^3/\text{day}$

$$\text{BOD}_{\text{mix}} = \frac{17360 \times 12 + 37152 \times 5}{17360 + 37152} = 7.23 \text{ mg/l}$$

$$k_{d18} = k_{20} (1.047)^{T-20}$$

$$= 0.12 \times (1.047)^{18-20}$$

$$= 0.1095$$

$$\text{BOD}_{\text{mix}} = \text{BOD}_u \left[1 - 10^{-k_{d18} \cdot t} \right] \quad \text{BOD}_{\text{mix}} = \text{BOD}_5$$

$$\Rightarrow 7.23 = \text{BOD}_u \left[1 - 10^{-0.1095 \times 5} \right]$$

$$\Rightarrow \text{BOD}_u = 10.09 \text{ mg/l}$$

Sub: _____

Day

Time: _____

Date: / /

(4) The minimum flow of a river is $50 \text{ m}^3/\text{sec}$ having a DO content of 7.0 mg/l (80% saturation) and BOD_5 of 8 mg/l . It receives a waste water discharge of $5 \text{ m}^3/\text{sec}$ with BOD_5 of 200 mg/l and no DO. If the rate constants of deoxygenation and reaeration are $0.5/\text{day}$ and $1.0/\text{day}$ respectively and velocity of river flow is 0.8 m/s , calculate the distance in kilometers d/s from the point of discharge where min. DO occurs.

Soln:

$$\text{DO}_{\text{mix}} = \frac{50 \times 7 + 5 \times 0}{50 + 5} = 6.36 \text{ mg/l}$$

o. saturation $\text{DO} = \frac{8.75}{0.80} = 8.75 \text{ mg/l}$

DO deficit, $D_0 = 8.75 - 6.36 = 2.39 \text{ mg/l}$

$$\text{BOD}_{\text{mix}} = \frac{50 \times 8 + 5 \times 200}{50 + 5} = 25.45 \text{ mg/l}$$

$$\text{BOD}_5 = \text{BOD}_u [1 - 10^{-k_d \cdot t}]$$

$$\Rightarrow 25.45 = \text{BOD}_u [1 - 10^{-0.5 \times 5}]$$

$$\Rightarrow \text{BOD}_u = 25.53$$

We know,

$$t_c = \frac{L}{k_p - k_d} \ln \left[\frac{k_p}{k_d} \left(1 - \frac{k_p - k_d}{k_d} \times \frac{D_0}{L} \right) \right]$$

Distance = velocity \times time

$$= \frac{0.8 \times 24 \times 3600 \times 1.45}{1000} = 0.517 \text{ days}$$

$$= 35.71 \text{ km}$$

(5) A waste water is discharged there an out-fall to a fresh water stream of mean velocity 4.2 m/s ~~500 m/sec~~. The DO & BOD₅ of the stream after receiving the waste water are 8.5 mg/l & 25 mg/l . Determine the time and distance downstream where DO concentration is minimum. given, $k_d = 0.25/\text{day}$, $k_p = 0.4/\text{day}$. Fully saturated DO = 9.2 mg/l . [DMTCL'19]

Soln:

$$\text{DO deficit } D_0 = \text{DO}_{\text{saturated}} - \text{DO}_{\text{mix}}$$

$$= 9.2 - 8.5$$

$$= 0.7 \text{ mg/l}$$

Sub: _____

Day: _____

Time: _____

Date: / /

$$BOD_{mix} = BOD_u [1 - e^{-k_d \cdot t}]$$

$$f = \frac{0.4}{0.25} = 1.6$$

$$\Rightarrow 25 = BOD_u [1 - e^{-0.25 \times 5}]$$

$$\Rightarrow BOD_u = L = \frac{25}{1 - e^{-1.25}} = 35.04$$

$$\text{we know, } t_c = \frac{1}{k_d(f-1)} \ln \left[\left\{ 1 - (f-1) \frac{D_0}{L} \right\} f \right] = 3.05 \text{ days}$$

$$\text{Distance} = \frac{1.2 \text{ m/s} \times 24 \times 3600 \times 3.05}{1000} \text{ km} = 316.224 \text{ km}$$

(6) A city discharges 100 cumecs of sewage into a river which is fully saturated with oxygen and flowing at the rate of 1500 cumecs during its lean days with a velocity of 0.1 m/sec. The 5 days BOD of sewage at the given temperature is 280 mg/l. Find when and where the critical DO deficit will occur in the d/s and what is its amount. Assume $f = 4$ & $k_d = 0.1$, $D_0 = 9.2 \text{ mg/l}$ (coefficient of purification)

Sub: _____

Day

Time: _____

Date: / /

$$\text{Sol}^n \text{ } DO_{\min} = \frac{9.2 \times 1500 + 0 \times 100}{1500 + 100}$$

$$= 8.62 \text{ mg/l}$$

[assuming DO of sewage is nil]

Initial DO deficit, $D_0 = 9.2 - 8.62 = 0.58 \text{ mg/l}$

$$BOD_{\min} = \frac{280 \times 100 + 0 \times 1500}{100 + 1500}$$

$$= 17.5 \text{ mg/l}$$

$t \therefore$ fully saturated
 $\therefore BOD = 0$

$$f = 4, k_d = 0.1$$

$$\therefore k_r = 0.4$$

$$BOD_5 = BOD_u [1 - 10^{-k_d t}]$$

$$\Rightarrow 17.5 = 2 [1 - 10^{-0.1 \times 5}]$$

$$\Rightarrow L = 25.58 \text{ mg/L}$$

$$\therefore t_c = \frac{1}{0.4 - 0.1} \log \left[\frac{0.4}{0.1} \left(1 - \frac{(0.4 - 0.1) \times 0.58}{25.58} \right) \right]$$

$$= 1.905 \text{ days}$$

$$\text{distance} = \frac{0.1 \times 24 \times 60 \times 60 \times 1.905}{1000}$$

$$= 16.5024 \text{ km}$$

$$\text{Amount of critical DO, } D_c = \frac{0.1}{0.4} \times 25.58 \times 10^{-(-0.1 \times 1.905)}$$

$$= 4.124 \text{ mg/L}$$

Sub: _____

Day _____

Time: _____

Date: / /

(7) A city discharges 1500 l/s of sewage into a stream whose minimum rate of flow is 6000 l/sec. The 5 day BOD for sewage is 200 mg/l and that of river water is 1 mg/l. If maximum permissible BOD of the mix is 14.45 mg/l, find out the degree of sewage treatment required.

Solⁿ:

Let's find out permissible BOD_5 for mix

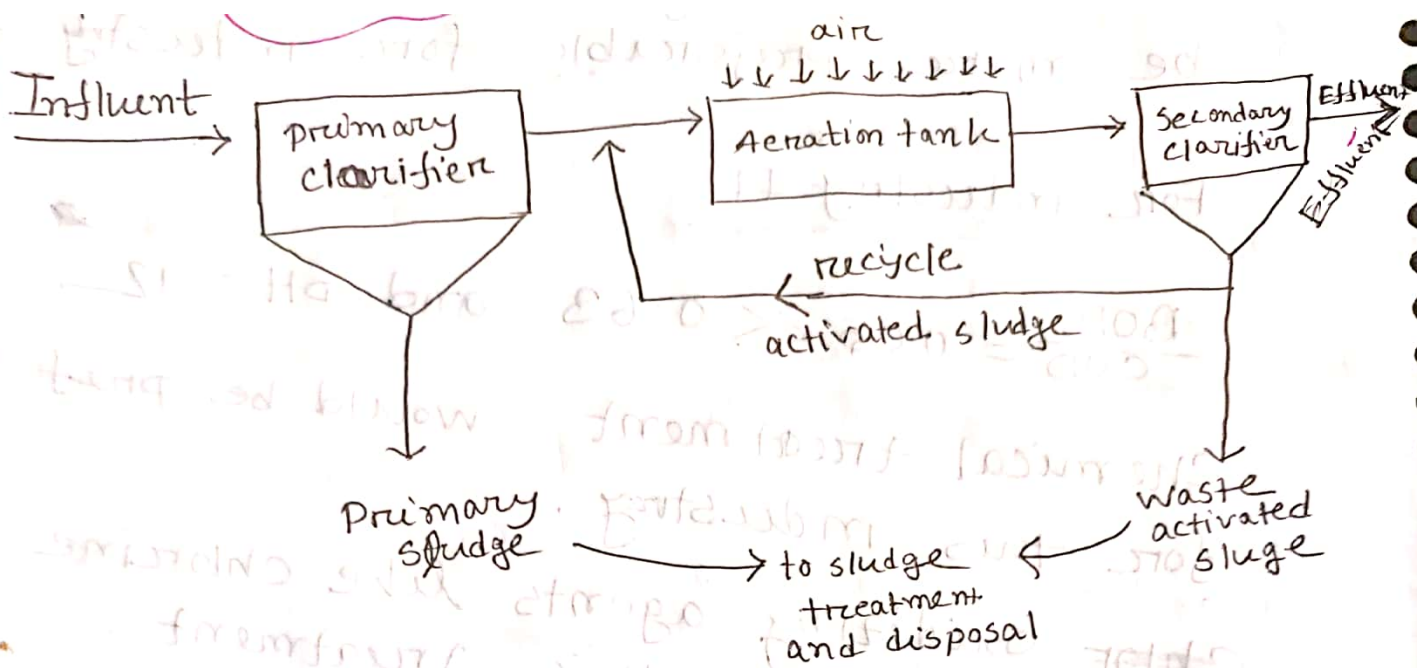
BOD of 14.45

$$14.45 = \frac{C_s \times 1500 + 1 \times 6000}{1500 + 6000}$$

$$\therefore C_s = 68.25$$

\therefore Degree of treatment required = $\frac{\text{original BOD of sewage} - \text{permissible BOD of sewage}}{\text{original BOD}}$

$$= \frac{200 - 68.25}{200} \times 100$$
$$= 65.875\%$$



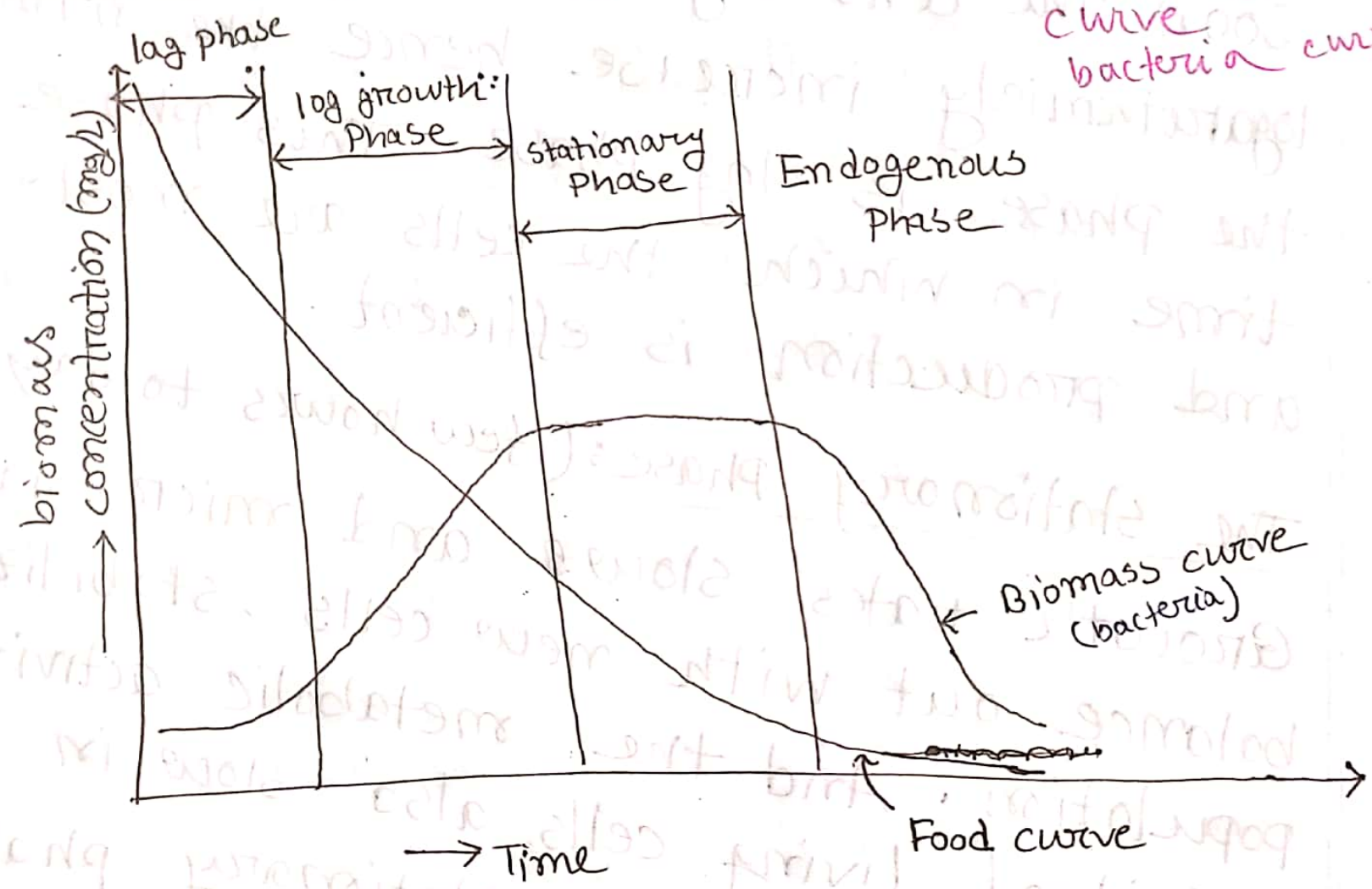
Activated sludge process

* Mechanisms of removal of heavy metals [DDPC'19]

- Sol^m:
- (i) Precipitation
 - (ii) Adsorption
 - (iii) Ion exchange
 - (iv) Electro-coagulation
 - (v) Electro-winning
 - (vi) Cementation
 - (vii) Reverse osmosis & Electro-dialysis

(bacteria)

Q. Draw a figure showing biomass growth and food utilization with time in a batch reactor. [BWB'16] [MSc'16]



Sol^{no}

Coagulation: Coagulation is a process of destabilizing colloidal and fine suspended particles presents in waste water by adding chemical coagulants. ~~and~~

The positive charges of coagulants neutralize the negative charge of suspended particles.

Neutralization causes suspended particles to bind together to make flocs of relatively higher specific gravity which eventually settle down to the bottom and filtered out from water.



P.T.O

VESTAR MR[®]
* TRIMETAZIDINE

* When alum is added to water as coagulant, it decreases pH value [BPDB'15]

* If temperature increases, the dissolved oxygen decreases [DWASA'14]

* The BOD value found from the ^{first} order reaction is approximately the value of NBOD T/F (BWDB'16)

Solⁿ = False. $BOD_5 \approx CBOD$
 $BOD_u \approx NBOD + CBOD$
↳ 2nd order

* In a gravity waste water pipe line system, the self cleansing velocity should be attained at least twice a day. T/F (BWB'16)

solⁿ: False. once a day

*** The only disinfectants chemicals that can be used for waste water treatment are chlorine & ozone T/F [BWB'16]

solⁿ: False

C/A: Three (3) most commonly used primary disinfectants are Chlorine, chlorine dioxide (ClO_2), Ozone (O_3)

also chloramine is used as a residual disinfectant for water distribution.

*** Trickling filter system needs more skilled operation and maintenance than activated sludge process T/F [BWB'16]

solⁿ: False

Activated Sludge Process	Trickling Filter
(1) Need skilled supervision and maintenance	(1) No need skilled supervision
(2) Lower cost of installation	(2) high cost of installation
(3) Small area required	(3) large area required
(4) No fly or odor nuisance	(4) fly and odor nuisance exits
(5) Only useful in certain types of industries	(5) VESTAR MR TRIMETAZOLINE

* What is environmental impact assessment (EIA)?

Why is it done? [CPGCB '15]

Solⁿ: Environmental Impact Assessment (EIA) is a process of evaluating the likely environmental impacts of a proposed project or development, taking into account inter-related socio-economic, cultural and human-health impacts, both beneficial & adverse.

Importance/Benefits of Environmental Impact Assessment (EIA):

- Through EIA, project managers know which project need full screening to prevent any damage to the environment.
- Helps to assess potential impacts relative to the environmental legislation based on the legislative requirements.
- Identifies problems and helps through mitigation process in advance to anticipate disasters likely to happen.
- protects the biodiversity environment by suggesting alternative safe project designs and methods.
- Predict the impact rate for proposed projects, this can be negative or positive.
- Highlights possible alternative safer to the environment and methods with less impact.

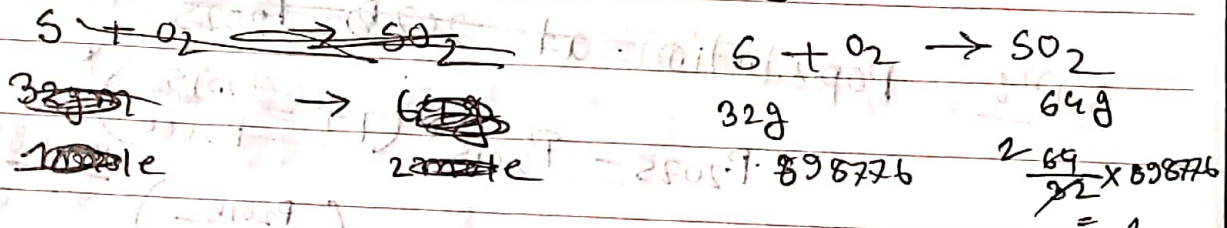
* The Barapukuria coal is burned at a rate of 1kg/sec. Analysis of BUET lab shows that coal release a sulphur content of 3%. What is the annual rate of emission of SO₂. Assume that 5% of the sulphur in the coal ends up in the ash. [APSC '20] & DESCO '15]

Solⁿ:

The mass of sulphur available to convert into SO₂ = $0.95 \times 0.03 \times 1 \text{ kg/s} \times 24 \times 3600 \times 365$ kg/year

(3% sulphur, 5% ash, 0.95 available)

= 898776 kg

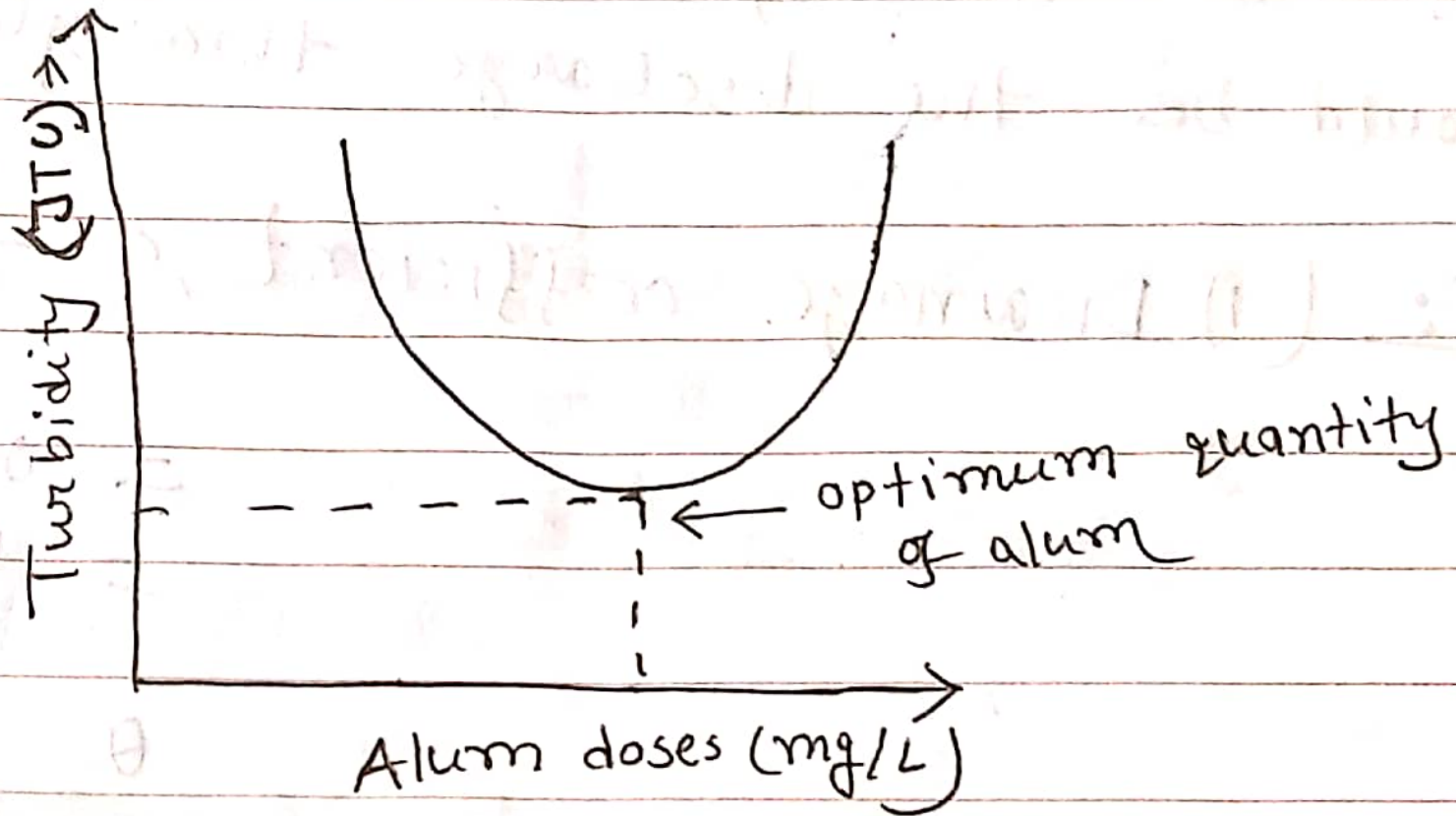


∴ from 898776 kg sulphur, SO₂ produces

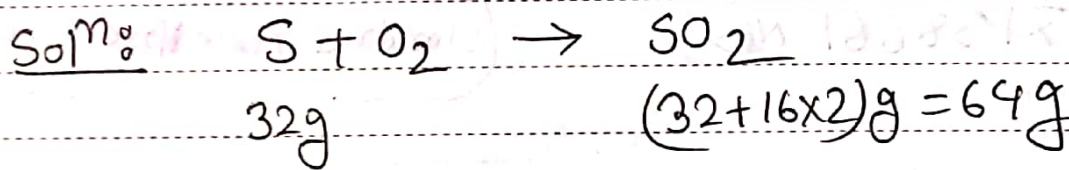
= $\frac{2}{1} \times (898776)$

= 1.797 × 10⁶ kg/year

* Draw a typical qualitative diagram for alum dose v/s residual turbidity in a coagulation-flocculation jar test of surface water sample. [NESCO'21] [BIWTA'22]



* A power plant burns its coal at a rate of 1000kg/sec. The analysis of the coal reveals a ~~S~~ sulfur content at 3%. Calculate the emission of SO_2 in million kg/year. [BIWA 23]



$$\text{Sulfur emission rate} = 0.03 \times 1000 \times 60 \times 60 \times 24 \times 365 \times 10^{-6}$$

$$= 946.08 \text{ million kg/year}$$

$$\therefore \text{SO}_2 \text{ emission rate} = \frac{64^2}{32} \times 946.08 \text{ million kg/year}$$

$$= 1892.16 \text{ million kg/year}$$

Ans



[ELBL'22]

* Abbreviation: [PGCL'17] [APSCCL'21] [B.C.MCL'21]

ETP = Effluent Treatment Plant

STP = Sewage Treatment Plant

ECR = Environment Conservation Rules

PIT = Pile Integrity Test

DCPT = Dynamic Cone Penetration Test

VST = Vane Shear Test

RAD = Rock Quality Designation

OCR = Over consolidation Ratio

* Drinking water standards according to ECR'97:

(1) Arsenic = 0.05 ppm / 50 ppb [PGCB'21] [CPGCB'22] [Titas'18] [SGCL'20] [BPDB'15]

* Lead = 0.05 ppm

(2) Iron = 0.3 ~ 1.0 ppm [NHA'19] [Titas'18]

(3) BOD₅ = 0.2 mg/L [Titas'18] [PGCB'21] [CPGCB'22]

(4) COD = 4 mg/L [ERL'22]

(5) DO = 6 mg/L

(6) Chlorine (residual) = 0.2 mg/L

(7) Coliform = 0 [CPGCB'22] [JGTDSL'21] [NHA'19] [MGML'22] [PGCB'21]

(8) Color = 15 Hazen

(9) Hardness (as CaCO₃) = 200-500 mg/L

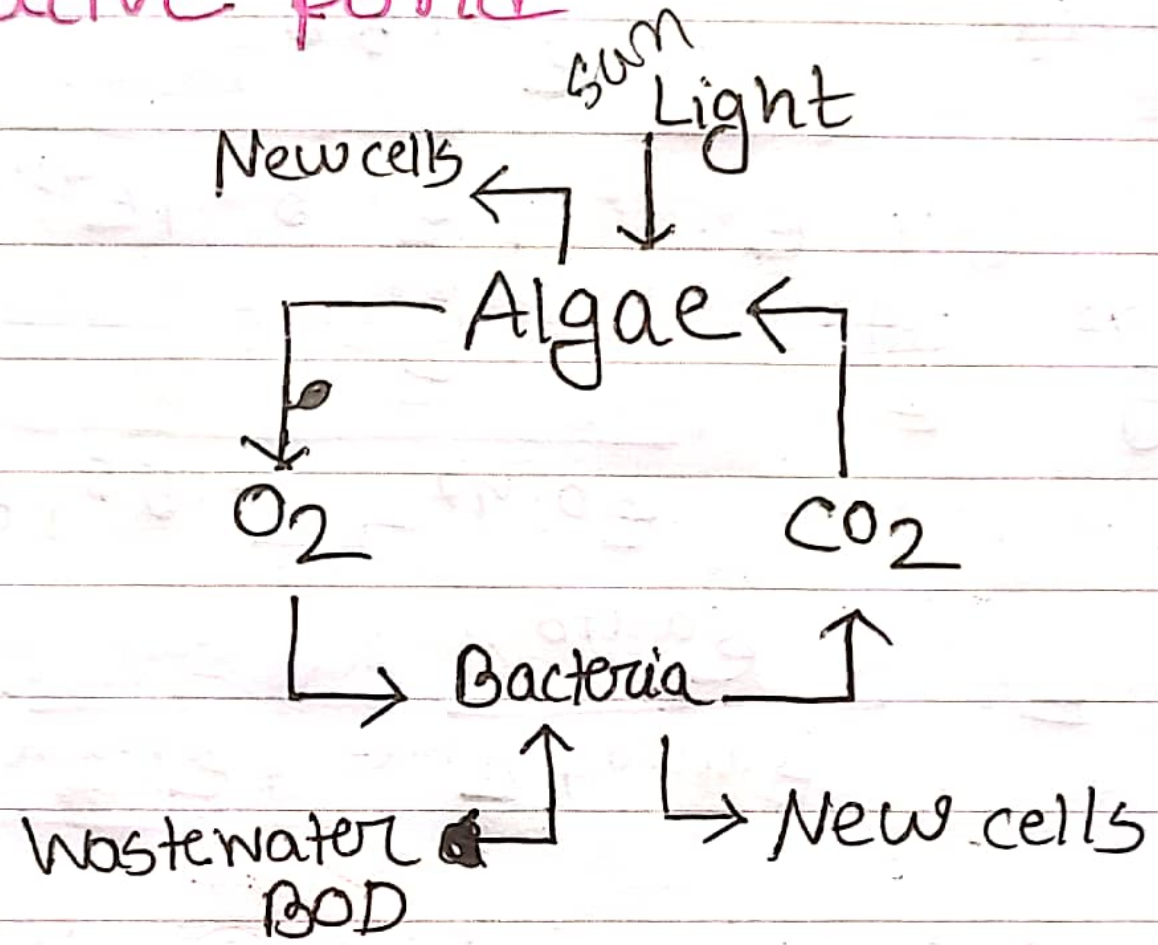
(10) Turbidity = 10 JTU [Titas'18] [GTCL'16]

(11) Total dissolved solids (TDS) = 1000 mg/L [Titas'18]

(12) pH = 6.5 - 8.5 [Titas'18] [CPGCB'22] [PGCB'21]

* Algae-bacteria symbiosis in a facultative pond

Solⁿ



Date: _____

Sun	Mon	Tue	Wed	Thu	Fri	Sat
-----	-----	-----	-----	-----	-----	-----

Write down the full meaning:

EIP = Effluent Treatment Plant

COD = Chemical Oxygen Demand

BOD = Biochemical Oxygen Demand

UNICEF = United Nations International Children's
Emergency Fund

~~SPT~~ SPT = Standard Penetration Test

~~STP~~ STP = Sewage Treatment Plant

ECR = Environment Conservation Rules

What is stabilizing pond? Write down the names of different kinds of waste water stabilizing ponds. Also enlist primary functions [DNCC 22]

⇒ wastewater stabilization ponds are large, man-made water bodies in which waste water sludge are treated by natural occurring process and ~~as~~ the influence of solar light, wind, ~~micro~~ microorganisms and ~~bacteria~~ algae.

⇒ WSPs are used when high quality effluents are not required and when a large area of land is available for such treatment.

⇒ Three main types

→ anaerobic

→ facultative

→ maturation

⇒ These can be used individually or linked in a series for improved treatment.

(anaerobic → facultative → maturation)

P.T.O

Date: / /

Sun Mon Tue Wed Thu Fri Sat

Anaerobic Ponds:

→ generally ~~2.5-5m~~^{2.5m-5m} deep in which anaerobic conditions prevail.

→ Formation of scum at the surface of the pond helps in reducing the possibility of entering of oxygen inside the pond.

→ The main function of anaerobic pond is BOD removal (40 to 85%)

→ Settle undigested material and non-degradable solids as bottom sludge.

→ Dissolve organic materials

→ Breakdown biodegradable materials

Facultative Ponds:

→ generally 1.5-2m deep and divided into three zones. Aerobic at surface, anaerobic zone at the bottom & facultative zone at mid depth.

→ BOD removal efficiency is 80 to 95%

→ Further treat wastewater through sedimentation & oxidation.

→ Reduce odour

~~→ Reduce some disease-causing microbes~~

→ Store residues as bottom sludge.

Date: _____

Sun Mon Tue Wed Thu Fri Sat

Maturation Ponds

→ generally 1-1.5m deep and are normally designed for 3-10 days of hydraulic retention time.

→ whereas anaerobic and facultative ponds are designed for BOD removal, maturation ponds are primarily designed for pathogen removal.

→ It also removes suspended stabilised solids.