

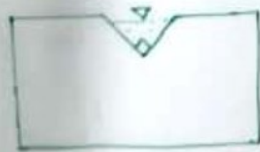
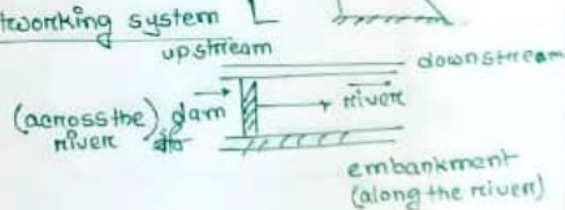
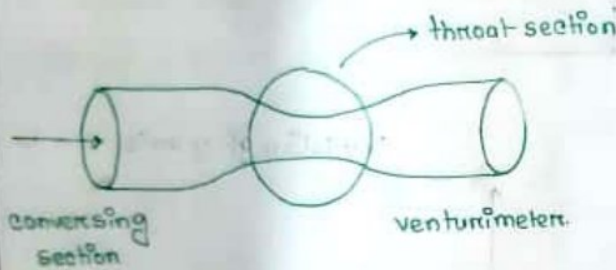
Fluid Mechanics Sessional

- ① Orifice → small piece of a cross sectional area.
- ② Mouthpiece → orifice का आगे Pipe जोड़ना (standard pressure vessel dia)
- ③ Cv by co-ordinate method
- ④ Venturimeter
- ⑤ V-notch
- ⑥ Sharp crested wire (बुझा)

Sharp crested



ori →  $C_d = 0.61 \sim 0.69$   
 math →  $C_d = 0.81 \sim 0.9$



measure the rate of flow of liquid  
 $Q = \text{rate of flow}$

close flow

$$\# y = mx + c$$



$$\# y = mx$$



$$\# y = ax^2 + 2$$



$$\begin{aligned} Q_d &= A \sqrt{2gh} \\ &= a \sqrt{2g} h^{1/2} \\ &= K h^{1/2} \end{aligned}$$



Variation of  $Q_d$  axis w.r to  $h$  axis

01/02/2020

Exp. no: 01

co-efficient of-  
Exp. Name: Determination of discharge of an orifice.

Theory:

orifice: Orifice is a small opening of any cross section (circular, triangular, rectangular etc.) on the side or at the bottom of a tank or a vessel through which the fluid is flowing.

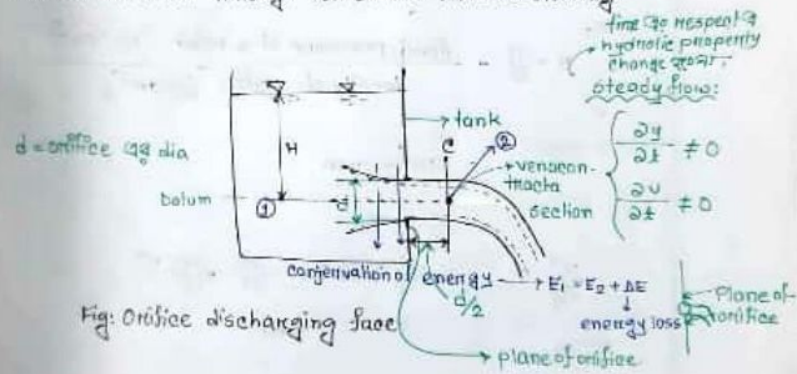


Fig: Orifice discharging face

pressure head  $\rightarrow P$

1  $\rightarrow$  fluid pressure

2  $\rightarrow$  atmospheric

$$\frac{P_1}{\rho} + \frac{v_1^2}{2g} + z_1 = \frac{P_2}{\rho} + \frac{v_2^2}{2g} + z_2$$

$\leftarrow$  velocity head

$z_1 = z_2$   $\rightarrow$  orifice dia same datum.

vena contracta  $\rightarrow$  when the stream lines are parallel to each other.

Consider 2 points 1 and 2, as shown in figure. Point 1 is inside the tank and point 2 is at the vena-contracta.

Let the flow is steady and at a constant head,  $H$ .

Applying Bernoulli's equation at points 1 and 2  $\rightarrow$

$$\frac{P_1}{\omega} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\omega} + \frac{V_2^2}{2g} + z_2$$

here,

$$H = \frac{P}{\omega} = \frac{\text{fluid pressure at a point } (kg/cm^2)}{\text{density of water } (g/cm^3)}$$

its a height = 'cm'  $\rightarrow$  m

$$\frac{V_1^2}{2g} \rightarrow \text{velocity head} = \frac{m^2}{s^2} \times \left(\frac{m}{s^2}\right)^{-1} = m$$

But  $z_1 = z_2$

$$\frac{P_1}{\omega} + \frac{V_1^2}{2g} = \frac{P_2}{\omega} + \frac{V_2^2}{2g}$$

$v_1$  is very small in comparison to  $v_2$ . as the area of the tank is very large as compared to the area of the jet of liquid.

therefore,

$$\frac{P_1}{\omega} = H, \quad \frac{P_2}{\omega} = 0 \text{ (atmospheric pressure)}$$

↙ fluid pressure

and  $v_2 \gg v_1$

$$\therefore H + 0 = 0 + \frac{v_2^2}{2g}$$

$$\Rightarrow H = \frac{v_2^2}{2g}$$

$$\Rightarrow v_2^2 = 2gH$$

$$\Rightarrow v_2 = \sqrt{2gH}$$

$$\Rightarrow \boxed{v_1 = \sqrt{2gH}}$$

Therefore,  
 $Q_t = A \times v_t$   
 $= A \sqrt{2gH}$  — (1)  
theoretical discharge / velocity.

Therefore, this is the theoretical velocity. also known as Torricelli's theorem.

### Hydraulic co-efficients:

(i) Co-efficient of discharge,  $(C_d) = \frac{Q_a}{Q_t}$

(ii) Co-efficient of velocity  $(C_v) = \frac{V_a}{V_t}$

(iii) Co-efficient of contraction,  $(C_c) = \frac{a_c}{a}$

↗ area of jet at c  
↘ area of orifice

✓ [Prove that  $C_d = C_v \times C_c$ ]

### Objectives:

- (i) To find the value of  $C_d$  for the orifice.
- (ii) To plot a graph to show the variation of  $Q_a$  with respect to  $Q_t$  in plain graph paper.
- (iii) To plot a graph to show the variation of  $Q_a$  with respect to actual head (H).
- (iv) To plot a graph to show the variation of  $Q_a$  with respect to H in log-log graph paper and find the exponent of H.

$$(H^{\frac{1}{2}})$$

$$n = 0.5$$

\* plane and log-log graph are diff.

↓  
linearly varying ...  $10^2, 10^3, 10^4, 10^5, 10^6$  ...  
non-linear variation

(v) find the adve-efficient of discharge from the log-log graph paper mention in number. 4. plain and the

### ③ Apparatus:

- (i) Constant head water tank.
- (ii) Orifice
- (iii) discharge measuring tank.
- (iv) stop watch.
- (v) point gauge.

### ④ Procedure:

- (i) dia of orifice measurement.
- (ii) Supply water to the cons. head water tank.
- (iii) Manometer  $\rightarrow$  read head.
- (iv)  $Q_d$
- (v)  $Q_d \rightarrow A \times \dots m^2 \times \frac{h}{t} = \frac{m^3}{\text{sec}} = Q_d$

Page ①

Sample  
 Calculation:  $H$   
 $Q_t$   
 $t$   
 and height of  $H_2O$  in the measuring tank (h)  
 $v = Ah$

Observation sheet:  $Q_a$   
 $C_d = Q_a / Q_t$

Dia of orifice = 0.000m

Cross sectional area of the orifice =  $\frac{\pi}{4} \times 0.0^2 =$

Cross sectional area of measuring tank,  $A =$

Theoretical discharge,  $Q_t =$  ---  $t =$  ---  $Q_a =$  ---  
 Actual head,  $H =$  ---  $v =$  ---  $C_d =$  ---

Data Table: Page ② → Calculation from log-log graph paper

No. of obs.	Actual head H	Theoretical discharge $Q_t$ (m <sup>3</sup> /sec)	Collection time, t (sec)	Volume of water, V (m <sup>3</sup> )	Actual discharge $Q_a$ (m <sup>3</sup> /sec)	Co-efficient of discharge $C_d = Q_a / Q_t$
1.						
2.						
3.						
4.						
5.						
6.						

Mean  $C_d =$

Objective number 1.#

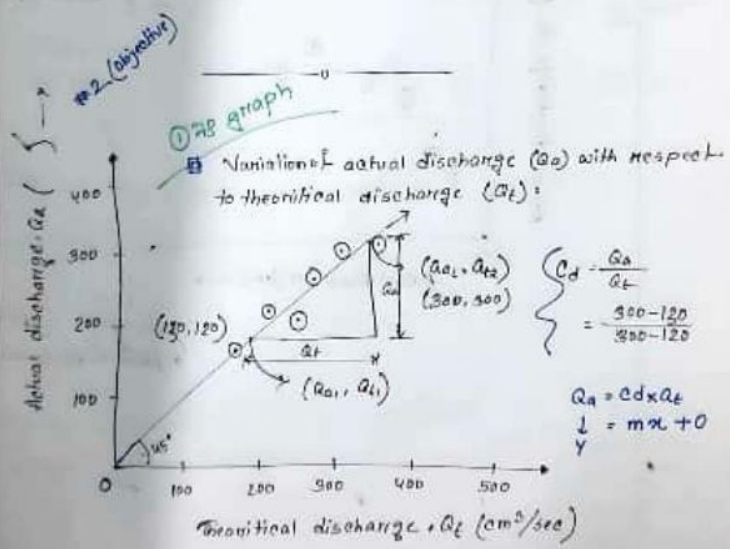
Graph

- Average  $C_d$  value for the orifice =
- The exponent of  $H$ ,  $n$  =
- The  $C_d$  value from plain graph paper =
- The  $C_d$  value from log-log graph paper =

am

⑥ Results: The average co-efficient of discharge = ...  
 and The exponent of  $H$  = ...  
 Discussion: The  $C_d$  from log-log graph paper = ...

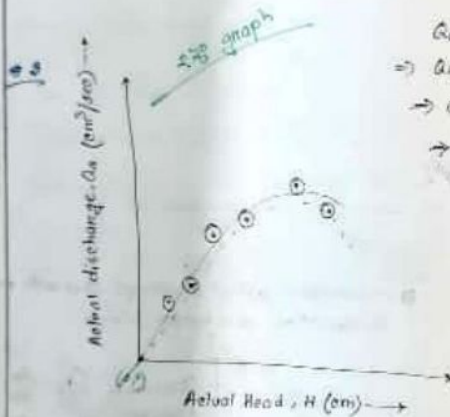
⑦ Assignment:



$C_d = \frac{Q_a}{Q_t}$   
 $\Rightarrow Q_a = C_d \times Q_t$   
 $\Rightarrow y = mx$

02/02/2020

Why the co-eff. of discharge of mouthpiece is greater than orifice.



$$Q_a = C_d \times Q_t$$
$$\Rightarrow Q_a = C_d A \sqrt{2gH}$$
$$\rightarrow Q_a = KH^{1/2}$$
$$\rightarrow y = mx^n \quad [n = \frac{1}{2}]$$

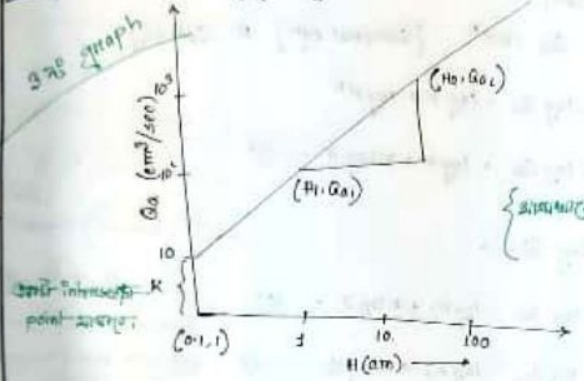
$$Q_a = A \times \frac{h}{t} \quad (\text{cm}^3/\text{sec})$$

Area of measuring tank

#4

3rd graph

(log-log)



$$Q_d = C_d A_f$$

$$\Rightarrow Q_d = K H^K$$

শিখানোর গুণক  $C_d$  পাওয়া

#5

① ও ② নং গ্রাফ প্রাথমিক  $C_d$  ও এর মান

let  $K = 5$

$$C_d = \frac{K}{A \sqrt{2g}}$$

derive a relationship to find the exponent of H

We know that

$$C_d = \frac{Q_d}{A_f}$$

$$\Rightarrow Q_d = C_d \times A_f$$

$$\Rightarrow Q_d = C_d \times A \sqrt{2gH}$$

$$= K \sqrt{H}$$

calculation from log-log graph paper

Therefore,

$$Q_a = KH^n \quad [\text{General eqn}] \quad K = C_d A \sqrt{2g}$$

$$\Rightarrow \log Q_a = \log K + n \log H$$

$$\Rightarrow \log Q_a = \log K + n \log H \quad \text{--- (1)}$$

by using (1)  $\rightarrow$

$$\log Q_{a_1} = \log K + n \log H_1 \quad \text{--- (2)}$$

$$\log Q_{a_2} = \log K + n \log H_2 \quad \text{--- (3)}$$

$$\text{eqn (3) - (2) } \rightarrow$$

$$\log Q_{a_2} - \log Q_{a_1} = n (\log H_2 - \log H_1)$$

$$\Rightarrow \log \left( \frac{Q_{a_2}}{Q_{a_1}} \right) = n \log \left( \frac{H_2}{H_1} \right)$$

$$\Rightarrow n = \frac{\log \left( \frac{Q_{a_2}}{Q_{a_1}} \right)}{\log \left( \frac{H_2}{H_1} \right)}$$

$\sqrt{\text{-noah}}$

$$Q_a = C_d \frac{B}{15} \tan \frac{\theta}{2} \sqrt{2g} H^{5/2}$$

$$n = \frac{5}{2} = KH^{5/2}$$

$$= KH^n$$

$$C_d = \frac{K}{B_{15} \tan \frac{\theta}{2} \sqrt{2g}}$$

derivation अवार्ड र(0)

अवार्ड K को अपन change र(0)

Exp. no: 02

Name of exp: Determination of the co-efficient of discharge of an external cylindrical mouthpiece.

① Theory:

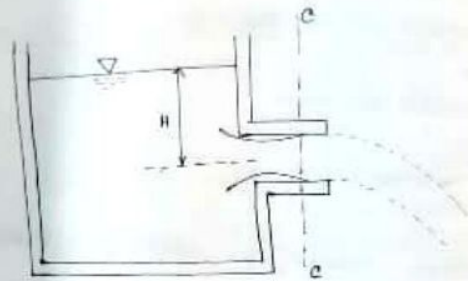


Figure: Flow through a mouthpiece.

$$Q_t = A \sqrt{2gh} \quad (2/3)$$

② Objectives:

① To find the  $C_d$  for the mouthpiece.

② }  
③ } exp - ①  
④ }

③ Apparatus:

④ Procedure:

} exp - ①

⑤ Observation sheet and sample calculation:

Diameter of the mouthpiece - } related to mouthpiece  
exp - ①

⑥ Data Table: exp - ①

Calculation from log-log graph paper  
Cd → graph Cd টিমে প্রস্তুত করা হবে।  
n → " " " " "

অন্য গুণক গুণক (সি)

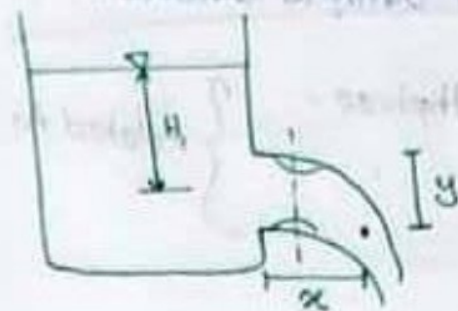
⑦ Result and discussion:

COURSE NO. CE 2122  
COURSE TITLE: ...

⑧ Assignment:

Submitted by:

NAME:  
CLASS: 2ND YEAR ODD SEMESTER  
ROLL: 1800, SECTION - 0  
GROUP: 01  
SESSION: 2018-19

Exp. no: 03Exp name: Determination of co-efficient of velocity by co-ordinate method.

$$C_v = \frac{V_a}{V_{th}}$$

$$= \frac{V_a}{\sqrt{2gh}}$$

→ cons. water head.

3.1 Theory:

3.1.1 Co-efficient of velocity ( $C_v$ ): Co-efficient of velocity is defined as the ratio bet<sup>n</sup> the actual vel. of the jet of a liquid at vena-contracta and the theoretical vel. of jet.

Mathematically,

$$C_v = \frac{\text{Actual Vel.}}{\text{Theoretical Vel.}}$$

$$= \frac{V_a}{V_{th}}$$

Where,

 $V_a$  = actual vel. of water at vena-contracta $V_{th}$  = theoretical " " "

The value of  $C_v$  varies from 0.95 - 0.99 for different orifices depending on the shape, size of the orifice and on the head under which flow takes place.

Generally the value of  $C_v = 0.98$  is taken for sharp edged orifice.

Co-ordinate method:

3.2. Determination of co-efficient of velocity ( $C_v$ )

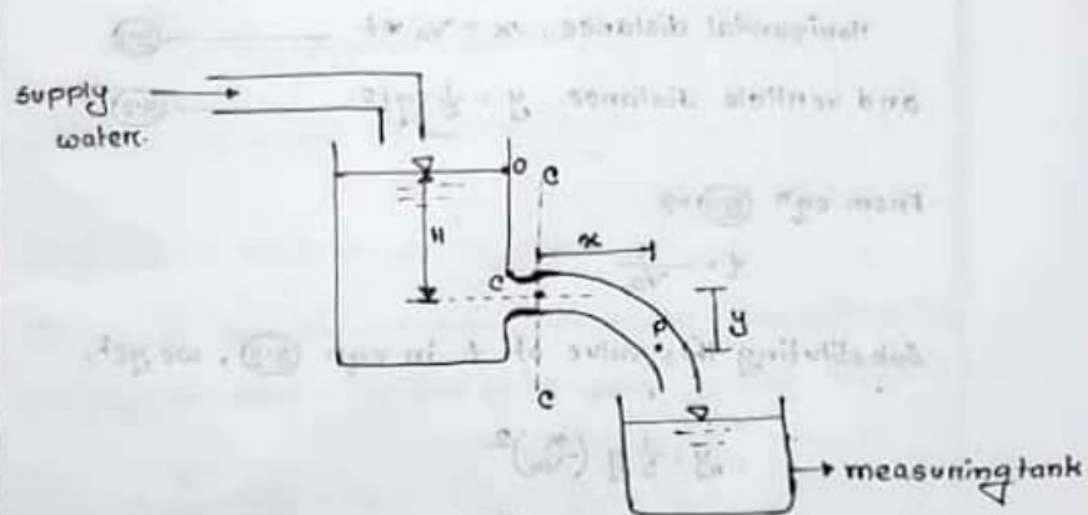


Fig 3.1: Determination of  $C_v$

Let (a-c) represents the vena-contracta of a jet of-water, coming out from an orifice under constant head, H, as shown is Figure 3.1

Consider a liquid particle which is at vena contracta at any time and takes the position at  $p$  along the jet in time  $t$ .

Let's

$x$  = horizontal distance travelled by the particle in time  $t$ .

$y$  = vertical " bet<sup>n</sup>  $p$  and (c-c).

$V_a$  = Actual velocity of jet at vena-contracta.

Then,

Horizontal distance,  $x = V_a * t$  ————— (3.1)

and verticle distance,  $y = \frac{1}{2} g t^2$  ————— (3.2)

From eq<sup>n</sup> (3.1)  $\Rightarrow$

$$t = \frac{x}{V_a}$$

Substituting this value of  $t$  in eqn (3.2), we get,

$$y = \frac{1}{2} g \left( \frac{x}{V_a} \right)^2$$

$$\Rightarrow y = \frac{1}{2} g \frac{x^2}{V_a^2}$$

$$\Rightarrow V_a = \frac{\sqrt{g x^2}}{2y} \text{ ————— (3.3)}$$

but theoretical velocity,

$$V_{th} = \sqrt{2gH} \quad (3.4)$$

$\therefore$  Co-efficient of velocity,  $C_v = \frac{V_a}{V_{th}}$

$$\Rightarrow C_v = \frac{\frac{\sqrt{g} \pi^2}{2g}}{\sqrt{2gH}}$$

$$\Rightarrow C_v = \frac{\pi}{\sqrt{4gH}}$$

This is the required equation of  $C_v$

\* Friction -  $q_2$   $q_1$   $V_a$   $q_2$   $q_1$

3.1.3 Loss of head in orifice flow:

The loss of head through an orifice can be determined by applying the Bernoulli's eqn bet<sup>n</sup> point  $a$  and  $c$  (Fig 3.1)

$$\frac{P_a}{\omega} + \frac{V_a^2}{2g} + z_a = \frac{P_c}{\omega} + \frac{V_c^2}{2g} + z_c \quad [\text{here, } V_c = V_a]$$

+ loss of head

$$\Rightarrow 0 + 0 + H = 0 + \frac{V_a^2}{2g} + 0 + h_f$$

$$\Rightarrow h_f = H - \frac{V_a^2}{2g}$$
$$= H \left(1 - \frac{V_a^2}{2gH}\right) = H(1 - C_v^2)$$



3.4 - Procedure:

- ① diameter of orifice
- ② Water supply to the tank.
- ③ When H is cons. the reading taken from the manometer.
- ④ Determine the coordinate, x and y from vena-contracta.
- ⑤ Repeat the procedure for different combination.

3.5 - Observation sheet and sample calculation:

Observation sheet:

Diameter of orifice	0.9 cm
Head constant	60 cm

Group No.	Observed Head	Horizontal co-ordinate, $x$	Verticle co-ordinate, $y$
निर्धारित ग्रुप	600 mm = 60 cm	440 mm = 44 cm	88 mm = 8.8 cm

Calculation sheet:

$$\text{Area of orifice, } A_o = \frac{\pi}{4} d^2$$

Group No.	Actual Head, $H$ (cm)	Theoretical Velocity $V_{th}$ (cm/s)	Horizontal Co-ordinate $x$ (cm)	Verticle co-ordinate $y$ (cm)	Actual Velocity $V_a$ (cm/s)	Co-eff of Velocity $C_v = \frac{V_a}{V_{th}}$	Head loss, $h_f$ (cm)
1.	60	343.10	44	88	328.49	0.957	5.05
2.	55	328.33	42	8.6	317.03	0.97	3.25
3.	50	313.21	40	8.4	305.66	0.98	1.98
4.	45	296.98	38	8.3	291.04	0.98	1.52
5.	40	280.14	36	8.4	275.09	0.98	1.58
6.	35	261.92	34	8.7	255.29	0.975	1.73

$$V_{th} = \sqrt{2gH} = 343.1$$

$$V_a = \frac{\sqrt{2gH}}{C_v} = 308.49$$

$$h_f = H(1 - C_v^2)$$

$$= 5.05$$

3.6 Results and Discussions:

Results: (Observation sheet - 40 21/21)

... ..  
 ... ..  
 ... ..

Discussions:

$W_1 = 10 \text{ gm}$   
 $W_2 = 10 \text{ gm}$   
 $W_3 = 20 \text{ gm}$   
 $W_4 = 10 \text{ gm}$

$$\frac{W_1}{W_2} = \frac{10}{10} = 1$$

$$\frac{W_1}{W_3} = \frac{10}{20} = 0.5$$

$$\frac{W_1}{W_4} = \frac{10}{10} = 1$$

$$\frac{W_2}{W_3} = \frac{10}{20} = 0.5$$

$$\frac{W_2}{W_4} = \frac{10}{10} = 1$$

$$\frac{W_3}{W_4} = \frac{20}{10} = 2$$

$$\frac{W_3}{W_2} = \frac{20}{10} = 2$$

$$\frac{W_4}{W_2} = \frac{10}{10} = 1$$

$$\frac{W_4}{W_3} = \frac{10}{20} = 0.5$$

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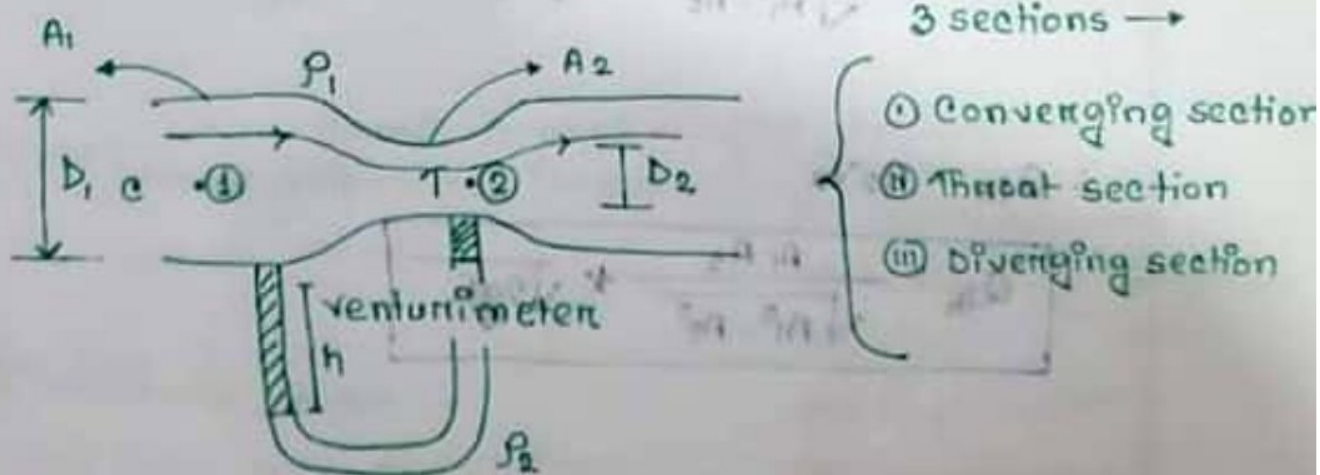
Exp no: 04

Exp. name: Determination of co. efficient of discharge for flow through venturimeter.

4.1 Theory:

venturimeter: venturimeter is the most widely used device to measure the discharge through the pipe.

A venturimeter is a converging-diverging nozzle of circular cross sectional area. The principle of venturimeter is that when a fluid flows through the venturimeter, it accelerates in the converging section and decelerates in diverging section resulting in a drop in the static pressure followed by a pressure recovery in the flow direction.



$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2$$

$$\Rightarrow \frac{P_1}{\gamma} - \frac{P_2}{\gamma} = \frac{V_2^2}{2g} - \frac{V_1^2}{2g} \quad \Rightarrow \quad h = \left( \frac{V_2^2}{2g} - \frac{V_1^2}{2g} \right)$$

$$Q = A_1 V_1 = A_2 V_2$$

$$\therefore V_1 = \frac{A_2 V_2}{A_1}$$

Putting the value of  $V_1$ ,

$$\therefore h = \left( \frac{V_2^2}{2g} - \left( \frac{A_2 V_2}{A_1} \right)^2 / 2g \right)$$

$$\Rightarrow h = \frac{V_2^2}{2g} - \frac{A_2^2 V_2^2}{A_1^2 2g}$$

$$\Rightarrow h = V_2^2 \left( \frac{1}{2g} - \frac{A_2^2}{A_1^2 2g} \right)$$

$$\Rightarrow V_2 = \sqrt{\frac{h}{\left( \frac{1}{2g} - \frac{A_2^2}{A_1^2 2g} \right)}}$$

$$\Rightarrow V_2 = \frac{A_1}{\sqrt{A_1^2 - A_2^2}} * \sqrt{2gh}$$

$\therefore Q_{th} = A_2 V_2$  → Area of throat.  
→ Area of converging section

$$Q_{th} = \frac{A_1 A_2}{\sqrt{A_1^2 - A_2^2}} * \sqrt{2gh}$$

→ Static pressure difference.



45 Observation sheet and sample calculation:

My group → Observation sheet:

Dia of converging section, $d_1$ (cm)	3.15
Area " " " $A_1$ (cm <sup>2</sup> )	7.79
Dia " throat " $d_2$ (cm)	1.55
Area " " " $A_2$ (cm <sup>2</sup> )	1.89
Area of tank, $A$ (cm <sup>2</sup> )	1372.5

measuring tank.

Group no.	Pressure Head at con. sec. $h_1$	Pressure Head at throat sec. $h_2$	Pressure head diff $h = h_1 - h_2$	Collection time $t$
01.	<del>65.5</del> 65.5	<del>62.5</del> 62.5	<del>0.25</del> 3	53

Calculation sheet:

Gip. no.	Pressure head at conv. $h_1$ (cm)	Pressure head at -th. $h_2$ (cm)	Pressure diff. $h = h_1 - h_2$ (cm)	Theoretical velocity. $Q_{th}$ (cm <sup>3</sup> /s)	Collection time $t$ (s)	Height in H <sub>2</sub> O tank. $H$ (cm)	Actual disch. $Q_a = \frac{AH}{t}$ (cm <sup>3</sup> /s)	Co-eff. disch. $C_d = \frac{Q_a}{Q_{th}}$
01.	<del>65.5</del> 65.5	<del>62.5</del> 62.5	3	<del>47.27</del> 149.47	53	5	129.48	<del>0.74</del> 0.87
02.								
03.								
04.								
05.								
06.								

$$\left. \begin{aligned} D_1 &= 3.15 \text{ cm} \\ D_2 &= 1.55 \text{ cm} \\ H_1 &= 655 \text{ mm} \\ H_2 &= 625 \text{ mm} \\ t &= 53 \text{ s} \end{aligned} \right\}$$

4.6 Result:4.7 Discussion:4.8 Assignment: